

# **Steel Pin and Hanger Assembly Replacement Options**

**Daniel G. Linzell, Ph.D., P.E., F.ASCE.**Voelte-Keegan Professor and Chair
Department of Civil Engineering
University of Nebraska-Lincoln

Chandana C. Balakrishna

Graduate Research Assistant Department of Civil Engineering University of Nebraska-Lincoln

# 2017

Nebraska Transportation Center 262 Prem S. Paul Research Center at Whittier School 2200 Vine Street Lincoln, NE 68583-0851 (402) 472-0141

"This report was funded in part through grant[s] from the Federal Highway Administration [and Federal Transit Administration], U.S. Department of Transportation.

The views and opinions of the authors [or agency] expressed herein do not necessarily state or reflect those of the U.S. Department of Transportation."

### **Steel Pin and Hanger Assembly Replacement Options**

Daniel G. Linzell, Ph.D., P.E., F.ASCE. Voelte-Keegan Professor and Chair Department of Civil Engineering University of Nebraska-Lincoln

Chandana C. Balakrishna Graduate Research Assistant Department of Civil Engineering University of Nebraska-Lincoln

A Research Report Sponsored by

Mid-America Transportation Center

University of Nebraska-Lincoln

Nebraska Department of Roads

January 2017

1. Report No. M042	2. Government Accession No.	3. Recipient's Catalog No.			
4. Title and Subtitle		5. Report Date January 2017			
Steel Pin and Hanger Assembly	Replacement Options	6. Performing Organization Code			
7. Author(s) Daniel G. Linzell and Chandana	C. Balakrishna	8. Performing Organization Report No. 26-1121-4031-001			
9. Performing Organization Nan Mid-America Transportation Ce 2200 Vine St.		10. Work Unit No. (TRAIS)			
PO Box 830851 Lincoln, NE 68583-0851		11. Contract or Grant No.			
12. Sponsoring Agency Name and Address Nebraska Department of Roads 1500 Hwy. 2 Lincoln, NE 68502		13. Type of Report and Period Covered July 2015- January 2017			
		14. Sponsoring Agency Code			
15. Supplementary Notes					

#### 16. Abstract

A number of steel beam bridges exist in the United States that contain pin and hanger assemblies. Pin and hanger assemblies are fracture critical members whose failure would result in collapse of the bridge or render it unable to perform its expected functions. As these bridges continue to age, many assemblies have deteriorated to a point where retrofit or replacement has to be considered and performed to maintain intended safety and performance. States have taken various approaches to address the pin and hanger assembly retrofit and replacement options. However, there is no single report that summarizes these approaches. This report documents steel pin and hanger assembly retrofit and replacement options via a literature review and synthesis that explores options that have been studied and implemented in the United States. In conjunction with the literature review, a survey was developed in conjunction with the Bureau of Sociological Research (BOSR) at the University of Nebraska-Lincoln to assist with identifying implemented strategies and evaluate best practices. Information was solicited from 50 states and was used in conjunction with the literature review to develop flowcharts that would assist NDOR personnel with assessing various options and their consequences when pin and hanger assembly retrofit or replacement options are being considered for bridges in the state.

17. Key Words	18. Distribution Statement			
Pin and Hanger; Steel; Bridge; Retrofit; Replacement				
19. Security Classif. (of this report)	20. Security Classif	(of this page)	21. No. of Pages	22. Price
Unclassified Uncla		ssified	193	

# **Table of Contents**

Chapter 1 Introduction	1
1.1 Background	1
1.2 Objectives and Scope	3
Chapter 2 Literature Review	4
2.1 Introduction	4
2.2 Literature	4
2.3 State and Federal DOT Provisions	9
2.4 Summary	12
Chapter 3 U.S. State Departments of Transportation Survey	14
3.1 Survey Objectives	14
3.2 Survey History and Timeline	15
3.3 Findings of the Survey	15
3.4 Follow-Up Contact	34
3.5 Summary	36
Chapter 4 Flowcharts Summarizing Retrofit and/or Replacement Options	38
4.1 Introduction	38
4.2 Retrofit and/or Replacement Options Process Summaries	39
4.2.1 Replace with Bolted Splices	40
4.2.2 Link Slab	42
4.2.3 Catcher Beam System	45
4.2.4 Replace with Ship Lap Joint.	48
4.2.5 Replace with Pin and Hanger Assembly.	53
4.3 Summary	55
Chapter 5 Recommendations for Future Research	56
References	57
Appendix A	61
Survey	61
Appendix B	65
Response to Survey of DOTs	65

Additional Comments	69
Appendix C	71
List of Abbreviations	71
Appendix D	74
Table A.1 Summary	74
Appendix D1	75

# **List of Tables**

Table 3.1 Types of bridges which has pin and hanger assembly	20
Table 3.2 Other types of steel bridges with pin and hanger assemblies.	21
Table 3.3 Implemented and programmed retrofit and/or replacement options	25
Table 3.4 Other implemented and programmed retrofit and/or replacement options	26
Table 3.5 Design Specifications.	30
Table 3.6 Developed own criteria & procedures.	30
Table 3.7 Reasons for pin and hanger assembly non-action.	33
Table 3.8 Summary of follow-up contacts	35
Table A.1 Summary	74

# **List of Figures**

Figure 2.1 Mianus River Bridge collapse.	5
Figure 3.1 Geographic representation of states that responded to the survey.	. 16
Figure 3.2 Visual representation of responses to question 1.	. 17
Figure 3.3 Geographic representation of state responses to question 1	. 18
Figure 3.4 Visual representation of state response to question 1(a).	. 19
Figure 3.5 Visual representation of state response to question 2	. 22
Figure 3.6 Geographical representation of states responded to question 2	. 23
Figure 3.7 Visual representation of state response to question 2 (a)	. 24
Figure 3.8 Geographical representation of federal design Specification usage	. 27
Figure 3.9 Visual representation of state responses to question 3.	. 28
Figure 3.10 Visual representation of states response to question 4.	. 29
Figure 3.11 Geographical representation of states have developed own criteria and procedures	. 29
Figure 3.12 Visual representation of states response to question 5.	. 31
Figure 3.13 Geographical representation of states need or not need for further action	. 32
Figure 3.14 Geographical representation of states contacted for additional details.	. 36
Figure 4.1 Flowchart demonstrates decision – making process.	. 39
Figure 4.2 Bolted splice design process.	. 41
Figure 4.3 Link slab detail.	. 43
Figure 4.4 Link slab design process.	. 44
Figure 4.5 Catcher beam system.	. 46
Figure 4.6 Catcher beam system representative detail	. 46
Figure 4.7 Catcher beam design process.	. 47

Figure 4.8 Ship lap joint at bearing at joint locations.	49
Figure 4.9 Ship lap joint detail.	50
Figure 4.10 Ship lap joint design process.	51
Figure 4.11 New pin and hanger assembly design process.	54

#### **Abstract**

A number of steel beam bridges exist in the United States that contain pin and hanger assemblies. Pin and hanger assemblies are fracture critical members whose failure would result in collapse of the bridge or render it unable to perform its expected functions. As these bridges continue to age, many assemblies have deteriorated to a point where retrofit or replacement has to be considered and performed to maintain intended safety and performance. States have taken various approaches to address the pin and hanger assembly retrofit and replacement options. However, there is no single report that summarizes these approaches. This report documents steel pin and hanger assembly retrofit and replacement options via a literature review and synthesis that explores options that have been studied and implemented in the United States. In conjunction with the literature review, a survey was developed in conjunction with the Bureau of Sociological Research (BOSR) at the University of Nebraska-Lincoln to assist with identifying implemented strategies and evaluate best practices. Information was solicited from 50 states and was used in conjunction with the literature review to develop flowcharts that would assist NDOR personnel with assessing various options and their consequences when pin and hanger assembly retrofit or replacement options are being considered for bridges in the state.

#### **Chapter 1 Introduction**

# 1.1 Background

Pin and hanger assemblies are structural components that have been used in many steel bridge systems around the United States (Mosavi et al. 2011). These assemblies are often used in steel girder systems and were traditionally implemented to reduce analysis, design, and construction complexity. The primary function of the pin and hanger assemblies is to mimic the rotational freedom provided by an idealized hinge in a continuous structural system, thereby reducing levels of indeterminacy and facilitating construction. The additional rotational degrees of freedom provided by the assemblies also help accommodate thermal movements of the bridge superstructure (Graybeal et al. 2000). As bridges continue to age, water, deicing chemicals, and debris that fall through the deck joint above the pin and hangers can accumulate on these assemblies and accelerate their degradation, possibly adversely affecting their performance and leading to a need for retrofit or replacement (Graybeal et al. 2000).

Pin and hanger assemblies are considered fracture critical members (FCMs), meaning they are non-redundant and their failure could cause partial or complete collapse. Non-redundant systems have traditionally contributed to major steel bridge collapses. The collapse of the Mianus River Bridge in Connecticut in 1983 is an example of a pin and hanger bridge that suffered a catastrophic failure (Connor et al. 2005).

The American Association of State Highway and Transportation Officials, Load and Resistance Factor Design Specifications (AASHTO LRFD) defines redundancy as "the quality of a bridge that enables it to perform its design function in a damaged state," and redundant member

as "a member whose failure does not cause failure of the bridge" (AASHTO LRFD, 2014). Different ways to enhance bridge redundancy include:

- Increasing the number of main supporting elements between points of structural support;
- Providing load redistribution mechanisms or providing continuity for main elements over interior supports elements; or
- Properly detailing structural elements using built-up cross sections, which provide division
  of elements to restrict increasing fracture propagation across the entire cross section.

States have taken various approaches to address the pin and hanger assembly retrofit and replacement, but there is no single report summarizing these approaches. This report documents a literature review that explores steel pin and hanger assembly replacement and retrofit options that have been studied and implemented in the United States. In addition to the literature review, a survey was developed in conjunction with the Bureau of Sociological Research at the University of Nebraska-Lincoln (BOSR) to assist with determining implemented strategies and evaluate best practices. In this survey, information was solicited from 50 states on current engineering practices related to addressing the steel pin and hanger assembly replacement options. Of these 50 solicitations, 38 (76%) were returned. Literature review and survey information was used to design an organized decision-making tool in the form of flowcharts that would assist NDOR personnel with assessing various options and their consequences when the pin and hanger assembly replacement and retrofit are being considered.

### 1.2 Objectives and Scope

The objectives of this project were to review and summarize research related to pin and hanger assembly behavior, repair and replacement while also determining and summarizing retrofit and replacement options being used by states in the U.S. The ultimate goal was the development of decision-making tools that would assist NDOR when considering pin and hanger assembly repair or replacement options in the future. These objectives were accomplished via the following steps:

- 1. Review relevant literature related to the pin and hanger assembly replacement options that have been studied and implemented in the United States;
- 2. Review relevant literature related to the design of steel web and flange splices one of the possible replacement options;
- 3. Survey U.S. State Departments of Transportation (DOTs) to investigate current practices for addressing pin and hanger assembly retrofit and replacement;
- 4. Synthesize and summarize information from Steps 1-3 to provide an initial summary of retrofit and replacement options;
- 5. Develop and present flowcharts that would assist engineers with assessing various options and their consequences when the pin and hanger assembly retrofit and replacements are being considered in the future.

### **Chapter 2 Literature Review**

### 2.1 Introduction

A major element of this study consisted of an in-depth literature review. The purpose of this review was to collect and summarize information related to pin and hanger assembly retrofit and replacement options. The literature review also provides information successfully implemented options in different parts of the United States and served as a resource for other portions of this study.

In this chapter, Section 2.2 *Literature*, summarizes the review of literature related to pin and hanger assembly retrofit and replacement options. Section 2.3 *State and Federal DOT Provisions*, describes available state DOT design provisions and protocols for various retrofit and replacement options.

### 2.2 Literature

In 1983, the I-95 Mianus River Bridge in Greenwich, Connecticut collapsed (Figure 2.1). The collapse was determined to occur when one of the pin and hanger assemblies fractured. This assembly was subjected to excessive corrosion due to water leaking through the deck joints and from drainage modifications (NTSB, 1984).



Figure 2.1 Mianus River Bridge collapse (Connor et al. 2005).

As a result of the Mianus River Bridge collapse, the Pennsylvania Department of Transportation (PennDOT) instructed its districts to identify and establish the current condition of pin and hanger assemblies on all bridges in Pennsylvania (Britt, 1990). A subsequent condition inspection of twin structures carrying I-80 over the Susquehanna River at Mifflinville, Pennsylvania discovered multiple fractured lower pin retainer bolts in its pin and hanger assemblies (Christie & Kulicki, 1991). Further investigation determined that the major cause of the fractures was significant build-up of corrosion on the pin and hangers. PennDOT had identified additional problems in similar bridges, such as pin cracking on the Wysox Bridge in the northeastern part of the state. As a result of this discovery and in an attempt to ensure future safety of similar bridges in the state, Modjeski and Masters (M&M) developed and proposed cost-effective methods to provide a higher level of redundancy for these bridges. M&M proposed the following pin and hanger assembly retrofit and replacement options:

- Providing continuity by removing the pin and hanger assembly and splicing the flange and web at that location;
- Providing a secondary system under the floor beams at the pin and hanger assembly; or
- Providing a secondary system under girders at the pin and hanger assembly.

PennDOT engineers, after several major studies (Christie & Kulicki, 1991), decided that providing continuity was the most advantageous solution from both aesthetic and safety points of view. However, preliminary study shows that this approach would only be economical when re-decking was programmed. Continuity would be established by designing splices into the girders following provisions established in the *AASHTO Standard Specifications for Highway Bridges*.

In 1989, the Loma Prieta earthquake in California demonstrated that bridges designed following pre-1983 AASHTO seismic criteria were sensitive to strong earthquakes (Shirole & Malik, 1993). As a result of these findings it was determined that a considerable retrofitting program was needed to address this issue. The program included improving the strength of the existing bridges whenever practical to improve their seismic resistance and global efficiency. Pin and hanger assemblies were deemed to be seismically sensitive components and global structural efficiency would be improved via their removal, which would provide continuity and enhance the redundancy of the structure.

In response to work in California, the New York State Department of Transportation (NYSDOT) initiated part of study on seismically sensitive bridges in New York to evaluate their resiliency and to provide a cost data for various seismic retrofits (Shirole & Malik, 1993). The project included a case study of five-span, continuous, steel, multi-girder bridge having pin and hanger assemblies that produced drop-in spans. The study recommended removal of the pin and hanger assembly replacing it with top flange, bottom flange and web splices following *AASHTO* 

Standard Specifications for Highway Bridges guidelines. It was also recommended that cumulative dead and live load stresses be checked in the vicinity of the replaced pin and hanger assembly locations.

Another possible retrofit option, termed a "link slab", has also been discussed in the research (Caner & Zia, 1998). In this method, expansion joints are removed at the pin and hangers, the deck is debonded from the girders for a minimum of 5 % of the span length on each side of the splice, and the joint is replaced with link slab, which renders the deck continuous while maintaining some level of rotational freedom for the girders beneath the link slab. Reducing the number of expansion joints via the placement of link slabs (Caner & Zia, 1998) would minimize or eliminate corrosion damage due to water leaking through the deck joints. Further discussion of this retrofit option can be found in *Section 4.2.2*.

A national effort to identify and synthesize inspections and repairs appropriate for FCMs was conducted in association with the National Cooperative Highway Research Program (NCHRP). The subsequent report provided a comprehensive investigation of bridges with fracture critical details and focused on inspection and maintenance of FCMs. One of the outcomes was identifying and briefly discussing prevailing pin and hanger assembly retrofit and replacement options in the U.S. The final report summarized two common techniques for the replacement and retrofit of pin and hanger assemblies (Connor et al. 2005):

• Complete removal of the pin and hanger assembly. In this method, the pin and hanger assembly is completely removed and replaced with a new section of the girder having bolted splices. The girders are made continuous for live load and a proportion of dead load given that these splices would be placed after the large part of the deck has been cast.

Continuity would be established by designing splices into the girders following *AASHTO LRFD Bridge Design Specifications*; and

 Placement of a catcher beam system. These systems are added below the location of the pin and hanger assembly to catch the suspended girder when the existing pin and hanger assembly fails.

In 2010, PennDOT further investigated pin and hanger assembly rehabilitation via a preservation program associated with the I-579 Crosstown Boulevard Bridge in Pittsburgh (Sirianni & Tricini, 2010). The program included complete replacement of pin and hanger assemblies with new stainless pins and high strength hangers. By replacing the existing assemblies with new, more durable components, the assemblies would be strengthened and maintenance requirements for the fracture critical bridges could be reduced.

In 2014, the Manitoba Infrastructure and Transportation Department conducted a detailed structural survey of the Pinawa Bridge, a bridge that contained pin and hanger assemblies. The study identified that steel girders near the existing pin and hanger assemblies had severe corrosion and deterioration due to deck expansion joint leakage (Banthia et al. 2014), which, subsequently, caused corrosion at the pin and hanger assembly that could possibly lead to catastrophic failure of the assembly. A number of possible failure mechanisms were identified, including:

- Reduction of pin cross section that could lead to crack initiation;
- Locking of the pin, which could produce considerable amount of torsional stresses on a
  reduced cross-section, stresses that, when combined with direct shear stresses, could
  provide an area for development and increases of cracks which leads to pin failure (Banthia
  et al. 2014); and

Corrosion and packrust formation of hanger plates that could cause the pin to move out of
the assembly and result in failure of the structure at the location of the assembly.

The study did not directly observe any cracks or loss in pin cross-sectional area or prevention of rotation. Despite these observations, it was recommended to replace all pin and hanger assemblies with bolted splices following guidelines provided in the AASHTO Standard Specifications for Highway Bridges and Manual for Bridge Evaluation.

#### 2.3 State and Federal DOT Provisions

The Nebraska Department of Roads (NDOR) has implemented certain retrofit and replacement options for the pin and hanger assemblies on specific bridges. These options included implementing;

- Catcher beam systems;
- Bolted splices; and
- Replacement with new pin and hanger assembly.

Design drawings for the implemented assembly options are found in Appendix D1.

NDOR was interested in identifying other State and Federal agencies who have implemented retrofit and replacement options and developed design specifications and supporting documents. Identified DOTs and their implemented options and documentation are summarized below.

The 2002 edition of the Montana Department of Transportation's "Montana Structural Manual" provides rehabilitation alternatives for pin and hanger assemblies (MDT, 2002). It was stated that pin and hangers are sensitive to corrosion because of leaking deck joints and subsequent

accumulation of debris on the assembly. This could result in the pin misplacements due to unseating of hangers and frozen pins and in initiation of fatigue cracks in the hangers. They recommended the following pin and hanger rehabilitation techniques (MDT, 2002):

- Unlocking the frozen pin and hanger assembly. Provide alternative support beam system
  to the suspended girder and remove the pin and hanger assembly. The elements of the
  assembly could be replaced or cleaned of corrosion before re-assembling the elements;
- Complete elimination of pin and hanger assembly. In this method, pin and hanger assemblies should be completely replaced with bolted splices. This approach requires a structural analysis of the continuous girder to show that revised load paths do not exceed the resistance of the superstructure. Continuity would be established by designing splices into girders following appropriate AASHTO Standard Specifications for Highway Bridges; and
- Providing a catcher beam system. In a catcher beam system, a supplemental support beam
  system is provided to catch the suspended girder ends if the pin and hanger assembly fails.
  Similar structural system could also be provided temporarily when frozen pin and hanger
  assemblies are slated to be unlocked.

PennDOT further investigated pin and hanger assembly rehabilitation in 2010 and recommended installation of a catcher beam system when pin and hanger assembly failure is a concern so that bridge integrity and safety is maintained (PennDOT, 2010). They stated that the catcher beam system should be designed to be active only if the pin and hanger fails and must accommodate anticipated thermal movements. The gap between the girder and the catcher beam system must be kept as small as possible to limit impact loading if failure occurs. They

recommended use of auxiliary neoprene bearings on the catcher beam system to reduce any impact effects (PennDOT, 2010).

In 2011, the Illinois Department of Transportation published a report that recommended that steel girders with pin and hanger assemblies be examined for assembly elimination and to make the superstructure system continuous whenever feasible and economical (IDOT, 2011). Continuity would be established by designing splices into the girders following the *AASHTO Standard Specifications for Highway Bridges*.

In 2012, the Federal Highway Administration stated that pin and hanger assembly failure is caused by formation of corrosion between the hanger and the girder web due to deck expansion joint leakage. As steel corrodes, it can occupy up to 10 times its original volume and cause unwanted forces in a limited space (FHWA-BIRM, 2012), which results in packrust and possible failure of the assembly. Additional pin and hanger assembly defects that were identified in the report were corrosion, fatigue cracking and coating failures. Various retrofit and replacement options were discussed as summarized below:

- Catcher beam system. The catcher beam system is added to the structure to carry a load if
  the pin and hanger assembly fails. The gap between the girder and the catcher beam should
  be kept as small as possible to reduce impact. Auxiliary neoprene bearings on the catcher
  beam system could be provided to reduce impact effects should failure occur;
- Removal and replacement of pin and hanger assembly with bolted splices. This approach requires a structural analysis to determine if other members can support continuous girders instead of cantilevered and drop-in spans. Analyses should investigate both positive and negative moment regions in the superstructure; and

 Replacing the pin and hanger assembly with a structural grade stainless steel pin and hanger, which results in reduction in corrosion mitigation.

In 2014, the Minnesota Department of Transportation published a study on a rehabilitation of the Kennedy Bridge over the Red River. This study focused on rehabilitation alternatives and showed that its pin and hanger assemblies had sufficient load carrying capacity. However, failure of multiple hangers could result in failure of the structure (MnDOT, 2014). Part of this study focused on increasing reliability of a bridge containing a pin and hanger assembly. It was reported that pin and hanger assembly retrofit and replacement options can include removing existing pins and hangers, re-machining pin holes to accommodate new pins as required to remove corrosion and pitting and the installation of new, higher strength pins and reinforced hangers. It was stated that each girder must be temporary supported while work is occurring and that temporary supports must be able to accommodate hanger fit up.

#### 2.4 Summary

This chapter has documented the results of a literature search that focused on current practices implemented in the United States and research related to retrofit and replacement of pin and hanger assemblies. A summary of finding from the literature review are provided below.

Retrofit options:

Bolted Splices -

Provide continuity by removing the existing pin and hanger assembly and splicing the flange and web at that location following appropriate AASHTO Specifications (AASHTO Standard Specifications for Highway Bridges, and AASHTO LRFD Bridge Design Specifications) and/or relevant state specifications. Providing continuity was the most advantageous solution from both

aesthetic and safety points of view but would be economical only when re-decking was programmed.

Rehabilitation options:

Link Slab -

Providing a link slab is a rehabilitation option that would remove expansion joints by linking two adjacent girder sections together using a continuous slab design. This approach would render the deck continuous while maintaining some level of rotational freedom for the girders.

Catcher Beam System -

A secondary catcher beam system could be added below the location of the pin and hanger assembly. This system should provided to carry live loads if the existing pin and hanger fails. The use of auxiliary neoprene bearings on the catcher beam system was recommended to use, reduce any impact effects should failure occur.

Removal and replacement option:

New Pin and Hanger Assembly -

In this option existing pins and hangers are removed and replaced with new, higher strength pins and reinforced hangers. It was recommended to use stainless steel pins and hangers according to *AASHTO LRFD Bridge Design Specifications* (Article 6.4.7), this could results in reduction in corrosion failure. While work is under construction each girder must be temporary supported and that temporary supports must be modifiable to accommodate hanger fit up.

### **Chapter 3 U.S. State Departments of Transportation Survey**

#### 3.1 Survey Objectives

In December 2015 a survey was sent to 50 State Departments of Transportation (DOTs). The objective of the survey was to assemble additional information on variety of topics related to pin and hanger retrofit and replacement options. These topics included: a) types of steel bridges that contain pin and hanger assemblies; b) pin and hanger assemblies that need retrofitted and/or replacements; and c) designs, procedures, or criteria for retrofit and/or replacements. Of the 50 surveys, 38 were received as of March 2016. Results from these surveys were examined to: a) document current practices and level of success concerning pin and hanger assembly retrofit and replacement options; b) identify practical application of retrofit and replacement options documented in the literature; and c) identify new or innovative retrofit and replacement options that have not yet been recorded in the literature.

The survey was divided into three sections. Section 1 (General) collected general information related to types of steel bridges that contain pin and hanger assemblies. Section 2 (Options) intended to identify various options, criteria and procedures related to retrofit and replacement of pin and hanger assemblies in each of the states. In addition, data related to retrofit and replacement options that have been implemented and programmed for future was requested. Section 3 (Future Contact) requested that additional information related to pin and hanger assemblies be provided, information that included: to share the respective state DOTs that have developed their own criteria and procedures for retrofits and /or replacements. A copy of the survey is included in Appendix A and responses are provided in Appendix B.

#### 3.2 Survey History and Timeline

The questionnaire was designed by BOSR with technical input being provided by UNL Civil Engineering personnel assigned to the project and NDOR. Prior to the initial mailing, NDOR notified and encouraged State Bridge Engineers to complete the survey. The initial mailing occurred in mid-December 2015. Non-responders were mailed survey packets a second time in early January 2016. Completed surveys were collected by BOSR through early March with findings summarized and provided to UNL Civil personnel.

## 3.3 Findings of the Survey

Surveys that were completed and returned were initially examined by BOSR, who performed data analysis, processing and filtering. BOSR's used Statistical Package for the Social Sciences (SPSS) software for processing and documenting the dataset. BOSR personnel assigned to the project, in turn, analyzed each survey question in detail and prepared a report. As stated earlier, of the 50 State Bridge Engineers who were sent the survey, 38 were completed and returned (Figure 3.1), a 76% response rate based on the American Association for Public Opinion Research's (AAPOR) standard definition for Response Rate 2 (RR2), which counts partial interviews as respondents (AAPOR, 2015). The following sections summarize survey responses to each question.

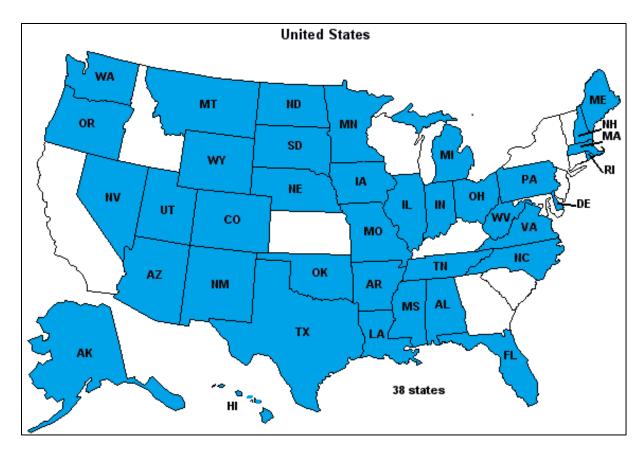
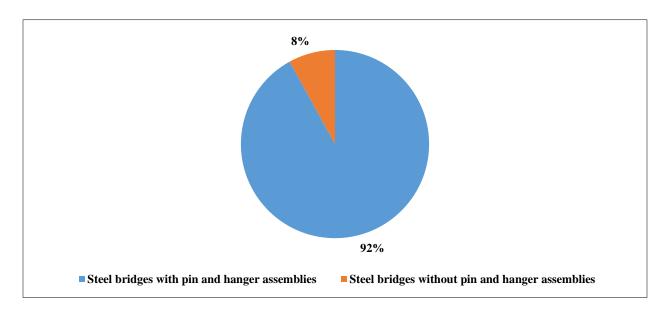


Figure 3.1 Geographic representation of states that responded to the survey.

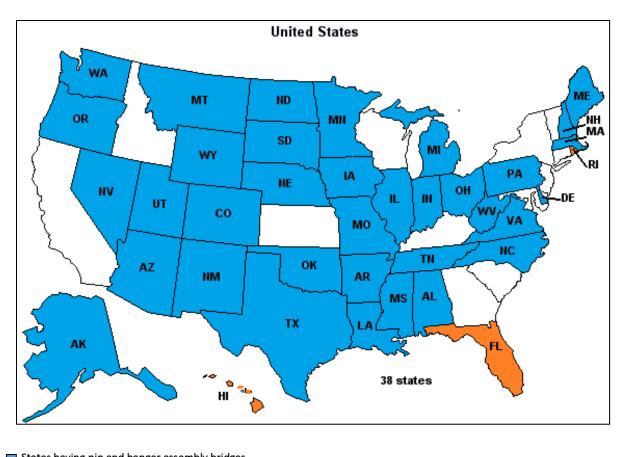
### 3.3.1 Question 1

Do you have steel bridges that contain pin and hanger assemblies?

Figure 3.2 and Figure 3.3 show that, of the 38 states who answered the question, 35 have steel bridges that contain pin and hanger assemblies and 3 states have steel bridges without pin and hanger assemblies.



**Figure 3.2** Visual representation of responses to question 1.



States having pin and hanger assembly bridges
 States don't have steel pin and hanger assembly bridges

**Figure 3.3** Geographic representation of state responses to question 1.

#### Question 1 (a)

If yes, please provide the number of steel bridge types for each category that have pin and hanger assemblies.

Figure 3.4 reports on the superstructure types that contain pin and hanger assemblies in their states. Eighteen states (67%) reported having two or three girder bridges with pin and hanger assemblies, 25 (86%) have at least one bridge with four or more girders having a pin and hanger assemblies, and 19 states (68%) contain at least one truss bridge with a pin and hanger assembly (Figure 3.4). Additional bridges reported as having pin and hanger assemblies included tied

through arches, suspension bridges, and pinned arches. Additional details are found in Table 3.1, Table 3.2 and Appendix B.

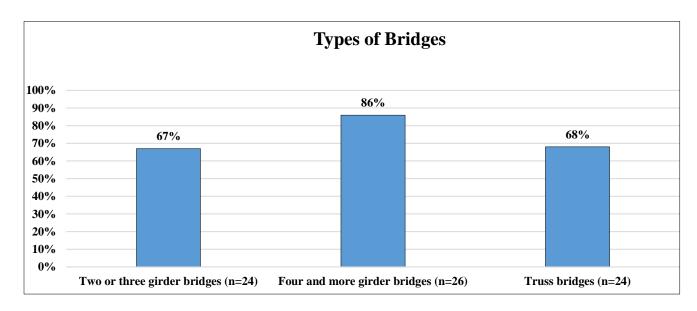


Figure 3.4 Visual representation of state response to question 1(a).

 Table 3.1 Types of bridges which has pin and hanger assembly.

DOTs	Two or three girder bridges	Four or more girder bridges	Truss bridges
Alabama DOT	1	5	2
Alaska DOT & PF	0	6	2
Arizona DOT	12	157	84
Arkansas State Highway and Transportation Department			6
Delaware DOT	0	3	1
Illinois DOT	1	92	14
Indiana NDOT	0	0	0
Iowa DOT	0	2	0
Maine DOT	0	6	3
Massachusetts DOT	1	11	1
Minnesota DOT	4	29	7
Mississippi DOT		24	2
Missouri DOT	26	750	10
Montana DT	4	150	0
New Hampshire DOT		74	
New Mexico DOT	0	17	0
North Carolina DOT	1	1	0
North Dakota DOT	0	14	1
Ohio DOT	9	13	
Oklahoma DOT	0	2	0
Oregon DOT	5	73	12
Pennsylvania DOT	45	15	12
South Dakota DOT	0	0	
Tennesseem DOT	2	0	2
Utah DOT	2	33	0
Virginia DOT	1	18	3
Washington State DOT	51	306	488
West Virginia DOT	6	26	5
Wyoming DOT	12	90	4

<sup>\*</sup>Acronym definitions in Appendix C.

 Table 3.2 Other types of steel bridges with pin and hanger assemblies.

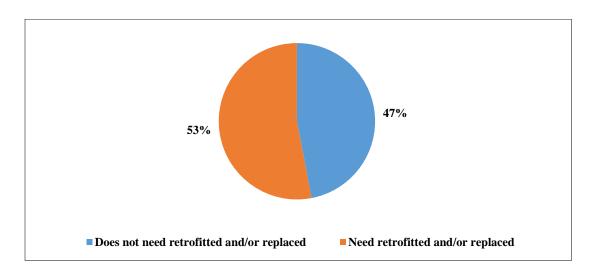
Other, Specify					
DOTs	Other types of bridges	Number of P & H assemblies			
Alaska Department of Transportation and Public Facilities	Box girders				
Arkansas State Highway and Transportation Department	Arch deck	2			
Colorado DOT	Tie down				
Illinois DOT	Truss with eye bars & pins	1			
Iowa DOT	Secondary highway steel girders Secondary highway truss				
Michigan DOT	All girder bridges	1099			
Minnesota DOT	Arch Suspension	1 1			
Ohio DOT	Riveted steel arches	2			
Oregon DOT	RGDG	9			
Utah DOT	Pinned arches Suspension arches	7 1			
Washington State DOT	Concrete box (2) Steel box(3)	132 90			
West Virginia DOT	Tied thru arch Suspension Bridge	1 1			

<sup>\*</sup>Acronym definitions in Appendix C.

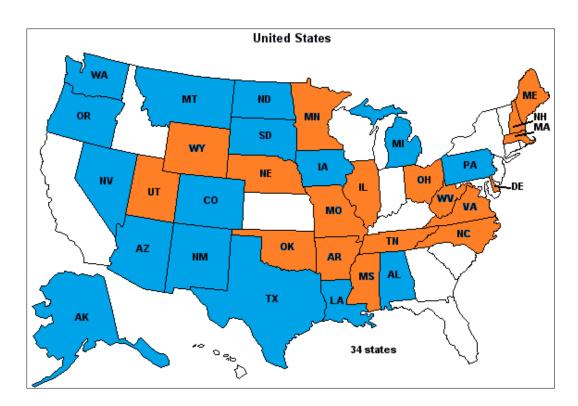
### *3.3.2 Question 2*

Does your agency view the pin and hanger assemblies as components that need to be retrofitted and/or replaced?

Figure 3.5 and Figure 3.6 shows state agencies were nearly evenly split between viewing pin and hanger assemblies as components that need to be retrofit and/or replaced and feeling that these assemblies do not need retrofitted and/or replaced. A complete list of reasons for non-action can be found in Appendix B.



**Figure 3.5** Visual representation of state response to question 2



**Figure 3.6** Geographical representation of states responded to question 2

Does not need retrofitted and/or replaced
 Need retrofitted and/or replaced

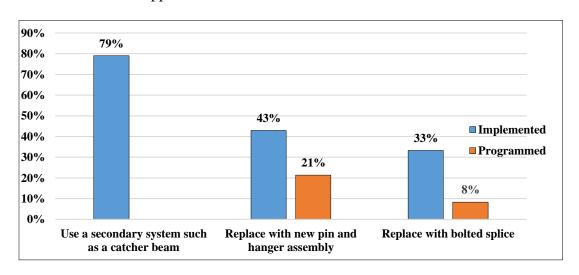
#### *Question 2(a)*

If yes, please provide the number of retrofit and/or replacement options that you have implemented or programmed for each category below. If you have implemented or scheduled retrofit and/or replacement options other than those listed below, please describe and provide the number for each option in the additional table rows.

Figure 3.7 shows that, for those that view retrofitting and/or replacement as necessary, most states have implemented a secondary system, such as a catcher beam (79%). Few responses indicated that replacements had taken place using new pin and hanger assemblies (43%) or bolted splices (33%). Despite fewer states implementing replacement using new pin and hanger

assemblies or bolted splices, nearly one-quarter of states who responded to the question have new pin and hanger replacement projects planned for the future (21%), while 8% have replacements with bolted splice repairs planned. Details are found in Table 3.3.

Other retrofit and/or replacement options implemented or planned by survey respondents included: (a) replacing the bridge or entire superstructure with concrete girders; (b) supporting the assembly using an "under-running bearing beam," which is akin to a catcher beam; and replacing the assembly with a "ship lap joint". Complete detail on these retrofit and replacement options can be found in Table 3.4 and Appendix B.



**Figure 3.7** Visual representation of state response to question 2 (a)

 Table 3.3 Implemented and programmed retrofit and/or replacement options.

Retrofit/replacement options						
DOTs		Catcher beam Replace with Replace w system P & H assembly bolted spli		_		
DOIS	Number implemented	Number programmed	Number implemented	Number programmed	Number implemented	Number programmed
Arkansas State Highway and Transportation Department	1					
Delaware DOT	1					
Illinois DOT	0	0	92	92	0	0
Indiana DOT	1	0	0	0	0	0
Maine DOT	4	0	0	0	1	0
Massachusetts DOT	2	0	0	0	0	0
Minnesota DOT	1	0	5	0	2	0
Mississippi DOT			1	1		
Missouri DOT	20	0	30	4	0	0
New Hampshire DOT			0		8	
North Carolina DOT	1	0	0	0	0	0
Oklahoma DOT	1	0	0	0	0	0
Tennessee DOT	1	0	0	0		
Utah DOT	0		5		2	3
West Virginia DOT	3	0	0	0	0	0
Wyoming DOT	0	0	1	0	0	0

<sup>\*</sup>Acronym definitions in Appendix C

 Table 3.4 Other implemented and programmed retrofit and/or replacement options.

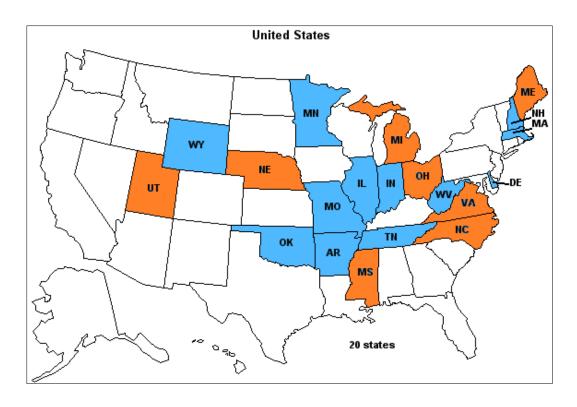
Other, Specify						
DOTs	Other options	Numbe r imple me nte d	Number programmed			
Maine DOT	Superstructure replace	1	1			
Massachusetts DOT	Ship lap joint. Replace P & H assembly with under running beam	0	1 0			
Mississippi DOT	Replace bridge	1	3			
Nebraska Department of Roads	Replace bridge or superstructure		50/102			
North Carolina DOT	Replace with concrete girder	0	1			
Virginia DOT	Replace bridge					
Wyoming YDOT	Suspension hanger/seismic	1	0			

<sup>\*</sup>Acronym definitions in Appendix C.

#### 3.3.3 Question 3

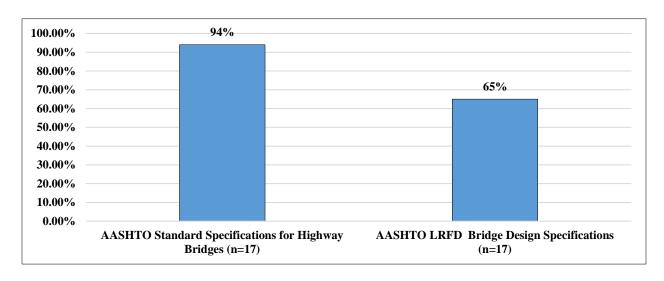
For the retrofits and /or replacements you indicated above as implemented or programmed, did you follow any of the designs, procedures, or criteria below?

The survey indicated that multiple designs, procedures, and/or criteria are used to complete pin and hanger assembly retrofit or replacement. Nearly all state bridge engineers who answered the inventory question reported using AASHTO Standard Specifications for Highway Bridges criteria and procedures, while some states use AASHTO LRFD Bridge Design Specifications criteria and procedures as shown in Figure 3.8 Figure 3.9. Five states reported using their own developed criteria and procedures.



States uses AASHTO Standard Specifications for Highway Bridges
 States uses either of one design Specifications

Figure 3.8 Geographical representation of federal design Specification usage.

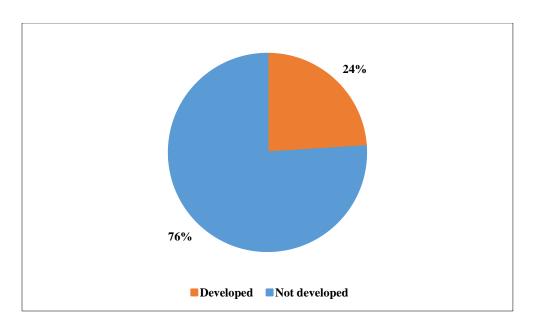


**Figure 3.9** Visual representation of state responses to question 3.

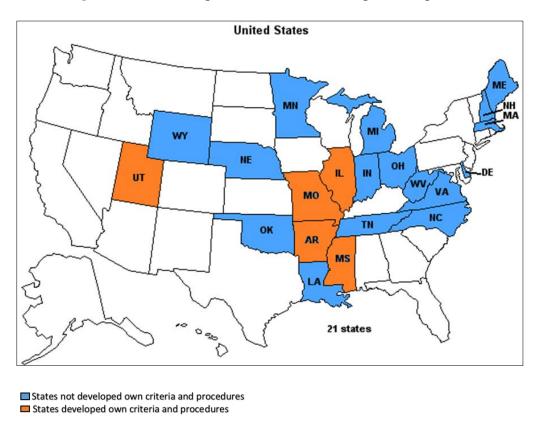
#### *3.3.4 Question 4*

Have you developed your own criteria and procedures for retrofits and/or replacements?

One-quarter of states in the (24%) reported developing their own criteria and procedures for retrofits and /or replacements (Figure 3.10 and Figure 3.11). More states use their own procedures in conjunction with the *AASHTO Standard Specifications for Highway Bridges*. Additional details are found in Table 3.5, Table 3.6 and Appendix B.



**Figure 3.10** Visual representation of states response to question 4.



**Figure 3.11** Geographical representation of states that have developed own criteria and procedures.

 Table 3.5 Design Specifications.

Design Specfications	Total number of States	
AASHTO LRFD criteria and procedures	11	
AASHTO Standard Specfication criteria and procedures	16	
Developed own criteria and procedures	5	

 Table 3.6 Developed own criteria & procedures.

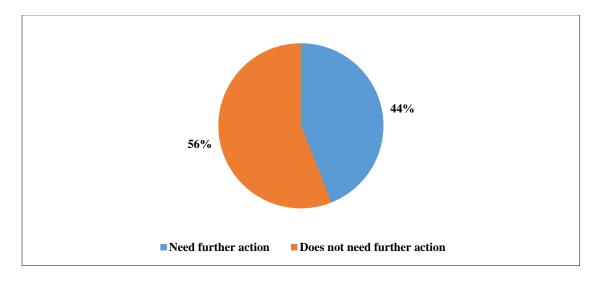
Developed own criteria & procedures for retrofits/replacements			
DOTs	Comments		
Arkansas State Highway and Transportation Department	Internally developed.		
Illinois DOT	It is part of our structural services manual. Bureau of Bridges and Structures.		
Mississippi DOT	Our bridge replacement program prioritizes bridges with pins & hanger high enough to systematically replacethe bridge with another (usually concrete) bridges.		
Missouri DOT	No set criteria. Details are case-by-case.		
Utah DOT	Is not documented.		

<sup>\*</sup>Acronym definitions in Appendix C.

#### *3.3.5 Question 5*

Does your agency view the pin and hanger assemblies as components that need no further action at this time?

Of the 32 state bridge engineers who answered the question, half reported that their agency views pin and hanger assemblies as not needing further action at this time as shown in Figure 3.12 and Figure 3.13. Reasons for non-action included: a) bridges being in good condition and functioning properly; b) routine inspections and adequate maintenance; and c) a lack of concern about these assemblies. A complete list of reasons for non-action can be found in Table 3.7 and Appendix B.



**Figure 3.12** Visual representation of states response to question 5.

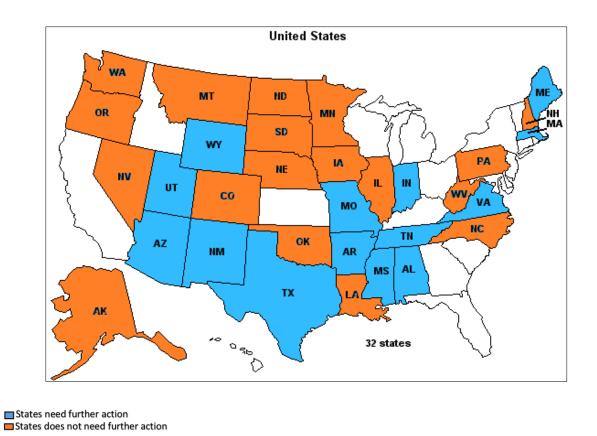


Figure 3.13 Geographical representation of states need or not need for further action.

 Table 3.7 Reasons for pin and hanger assembly non-action.

Agency view P & H assemblies that need no further action at this time			
DOTs	Comments		
Alaska DOT & PF	Pin & hangers are functioning properly.  No pack rust present.		
Colorado DOT	No section loss due to corrosion & no crack on hanger.		
Delaware DOT	We are not as concerned with pin & hanger assemblies for multi-beam bridges.  Pin & hanger assemblies on truss bridges are treated as a fracture critical member and are scrutinized more.		
Iowa DOT	Proper inspection should identify deficiencies in time to address them without impacts to public safety.		
Louisiana DOT	Bridges are in good condition.		
Montana DT	Pins and hangers are usually inspected every 2 years and UT inspected every 4 years. With our relatively dry climate and large temperature swings the p & h assemblies usually stay moving as designed with little rust impact.		
Minnesota DOT	We will include repairs or improvements to pin and hanger elements as conditions warrant. We have not developed projects solely on pin and hanger detail unless condition justifies.		
North Carolina DOT	Inspection reports indicate the condition of the pin and hang is "good".		
Nebraska Department of Transportation	All bridges are inspected by certified inspectors at least every 2 years and all bridges that this agency manages directly have redundant secondary systems should failure occur.		
Nevada DOT	We haven't identified problems with the hangers, aside from minor corrosion.		
Ohio DOT	We retrofit when they are deteriorated.		
Oklahoma DOT	We used ultrasonic inspection on our pins. No problems were found.		
Oregon DOT	We inspect & monitor p & h's and only r & r or provide supplemental support when their condition indicates a need.		
Pennsylvania DOT	We have retrofitted the inventory of 2 girder and truss bridges with suspended assemblies.		
South Dakota DOT	These assemblies are part of annual NBIS inspections and the pins get a periodic NDT inspection as well.		
Virginia DOT	We evaluate each one individually.		
Washington State DOT	Routine inspections and painting when needed.		
West Virginia DOT	We monitor during routine inspections and provide action as needed		

<sup>\*</sup>Acronym definitions in Appendix C.

#### 3.3.6 Question 6

If you developed your own criteria and procedures for retrofit and/or replacements, would you be willing to share those with us?

Of the 30 state bridge engineers who answered the question, 10 states were willing to share their criteria and procedures electronically.

#### *3.3.7 Question 7*

Would you like to receive results of this study?

Of the 38 states bridge engineers who answered the question, 33 states would like to receive the results from this study.

#### 3.4 Follow-Up Contact

States that indicated they would provide additional information in response to question 6, based on the response to question 6, follow up for the fourteen states (Figure 3.14). The plans, drawings and photos are found in Appendix D1. Additional details of the retrofit and/or replacement options are discussed in Chapter 4. Summary of contact information found in Table 3.8.

 Table 3.8 Summary of follow-up contacts

DOTs	Contacted for the information
Arkansas State Highway and Transportation Department	Not responded
Colorado DOT	Not responded
Georgia DOT	Not responded
Illinois DOT	Provided repair drawings found in Appendix D1
Indiana DOT	Not responded
MassDOT	Provided information on ship lap joints with plan and pictures found in Appendix D1
Michigan DOT	Provided pin and hanger assembly drawings found in Appendix D1
North Dakota DOT	Not responded
New Hampshire DOT	Not responded
Oklahoma DOT	Provided catcher beam system drawing found in Appendix D1
Pennsylvania DOT	Provided catcher beam system drawing found in Appendix D1
South Carolina DOT	Not responded
Texas DOT	Not reponded
Utah DOT	Not responded

<sup>\*</sup>Acronym definitions in Appendix C.

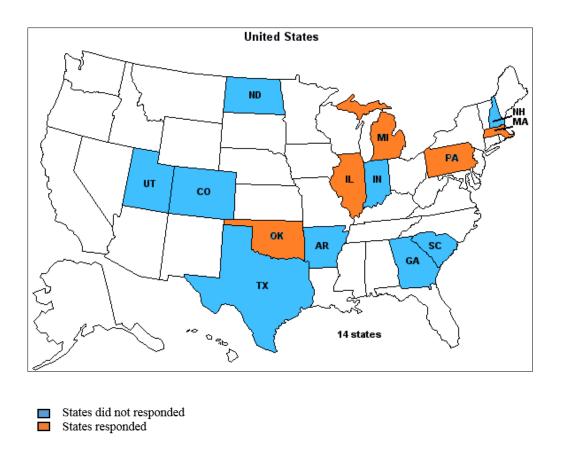


Figure 3.14 Geographical representation of states contacted for additional details.

## 3.5 Summary

The State DOT survey produced the following information:

- States who responded were roughly split between seeing such retrofits and replacements as necessary and unnecessary;
- Pin and hanger assemblies are most commonly found bridges having four and more girders (86%);
- Implementing a secondary system, such as a catcher beam (79%), is a more widely used retrofit and/or replacement option than replacing with either a new pin or hanger assembly

- (43%) or with bolted splices (33%), although at the time of the inventory study no future secondary system retrofits were programmed;
- Nearly all of the states utilize AASHTO Standard Specifications for Highway Bridges (94%), while fewer states use the AASHTO LRFD Bridge Design Specifications (65%), and some states developed their own criteria and procedures; and
- Additional retrofit and/or replacement options that were revealed by the survey included replacing with a "ship lap joint," providing an "under-running bearing beam," and, as expected, replacing the entire bridge or superstructure.

# Chapter 4 Flowcharts Summarizing Retrofit and/or Replacement Options

## 4.1 Introduction

The objectives of this chapter are to provide flowcharts that describe steps associated with completing feasible options associated with addressing pin and hanger assembly retrofit and/or replacement. Approaches for which flowcharts are provided are categorized as retrofit, rehabilitation, or removal and replacement options as shown in Figure 4.1. The intention is that these flowcharts will provide an organized decision-making tool that would assist NDOR personnel with assessing options and their consequences when pin and hanger assembly retrofit and/or replacement are being considered. As appropriate, each cell in the flowcharts refers to corresponding articles in appropriate state and federal design specifications. These include the AASHTO Standard Specifications for Highway Bridges, the AASHTO LRFD Bridge Design Specifications and NDOR's Bridge Office Policies and Procedures (BOPP) manual.

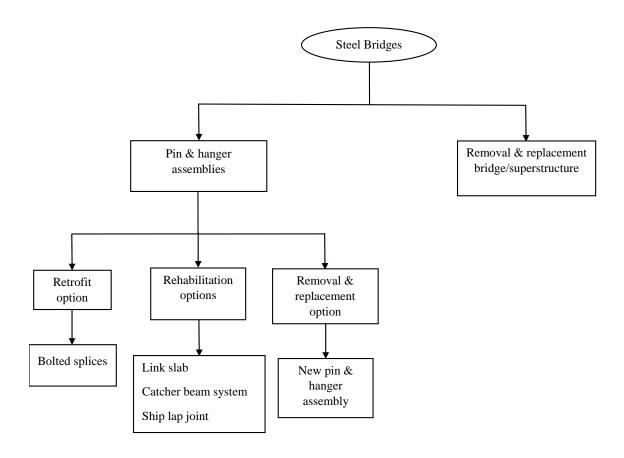


Figure 4.1 Flowchart demonstrates decision – making process.

## 4.2 Retrofit and/or Replacement Options Process Summaries

This section summaries retrofit, rehabilitation and, removal and replacement options based on the literature review and survey of DOTs and provided along with pros and cons of each respective options. Each section organized into brief summary followed with pros, cons and flowcharts with description.

#### *4.2.1 Replace with Bolted Splices*

This section summarizes the option that involves removing pin and hanger assemblies and replacing them with bolted splices. Items that are discussed and presented in the corresponding flowchart incorporate relevant information from the literature search, DOT survey and appropriate federal and state specifications.

When a major retrofit of a bridge structure is programmed, pin and hanger assemblies should be examined for elimination. The pin and hanger assembly would be replaced with continuity web and flange splices and existing deck expansion joints at the hinges would be removed and replaced to make these locations continuous. By making the drop-in section spans locations to continuity support the demand of the girder changes, so demand should be recalculated. While the pin and hanger assembly is being replaced with bolted splices, the girders should be temporarily supported from below or above the deck.

The state DOT survey produced a comment related to replacing pin and hanger assemblies with bolted splices. For drop-in section spans, the method implemented to eliminate the assemblies completely and replace with bolted splices involved installation of counterweights at the ends of the span. A flow-chart detailing general steps involved in the process is located in Figure 4.2.

#### Pros:

- Pin and hanger assembly is removed and continuity is provided through splices, possibly eliminating non-redundancy and making the structure more efficient; and
- Expansion joints eliminated to reduce and mitigate superstructure corrosion.

#### Cons:

- Changing the structural system from containing a drop-in span to being completely continuous necessitates a re-evaluation of superstructure behavior and capacity; and
- Higher construction cost.

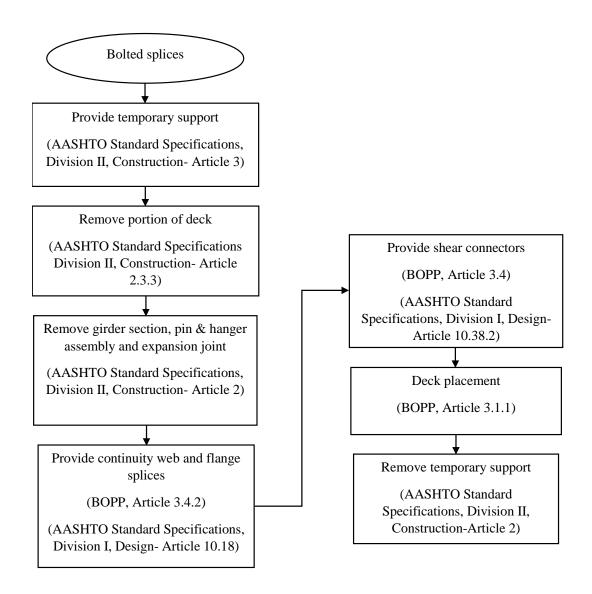


Figure 4.2 Bolted splice design process.

As shown in Figure 4.2, when considering replacing the assemblies with bolted splices, the process starts with following steps. While replacing the pin and hanger assemblies with bolted splices, the girder should be supported by temporary support beam and this support should be provided according to Standard Specifications, Division II-Construction (Article 3). The portion of the deck along the expansion joints are removed as per the design dimensions of the splices according to Standard Specifications, Division II-Construction (Article 2.3.3). The portion of the girder section near the pin and hanger location, pin and hanger assembly, and the expansion joints are removed according to Standard Specifications, Division II-Construction (Article 2). The dropin span is completely converted into continuity support which is provided through bolted splices connection according to Standard Specifications, Division I-Design (Article 10.18) and BOPP Specifications (Article 3.4.2). Here demand of the girder changes, so demand should be recalculated. Provide shear connectors along the newly constructed girder, shear connectors are designed to provide a composite action between the slab and the girders according to Standard Specifications, Division I-Design (Article 10.38.2) and BOPP Specifications (Article 3.4). Place the deck according to BOPP Specifications (Article 3.1.1). Finally, after construction temporary support should be removed according to Standard Specifications, Division II-Construction (Article 2).

#### 4.2.2 Link Slab

This section summarizes the option that involves removing expansion joints and replacing them with link slab. Items that are discussed and presented in the corresponding flowchart incorporate relevant information from the literature search.

The deck expansion joint is one of the significant component in the functioning of bridge structures (Chang & Lee, 2002). Deck expansion joints accompany the pin and hanger assemblies. The elimination or reduction of expansion joints reduces costs. One identified option that would help eliminate deck joints is via providing "link slabs" at joint locations. Figure 4.3 referred from (Caner & Zia, 1998). A flow-chart detailing general steps involved in the process is located in Figure 4.4.

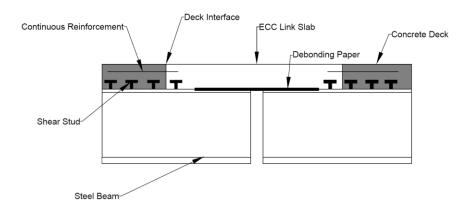


Figure 4.3 Link slab detail.

#### Pros:

 Reduced construction and maintenance of bridge via reduction of joints, moisture intrusion and subsequent corrosion control.

#### Cons:

- Continuity achieved by providing link slab influences shrinkage, creep and thermal stress which causes structural damages; and
- Continuous slab has high stresses developed due to repeated load will lead to fracture and cracking of the structures along the slab.

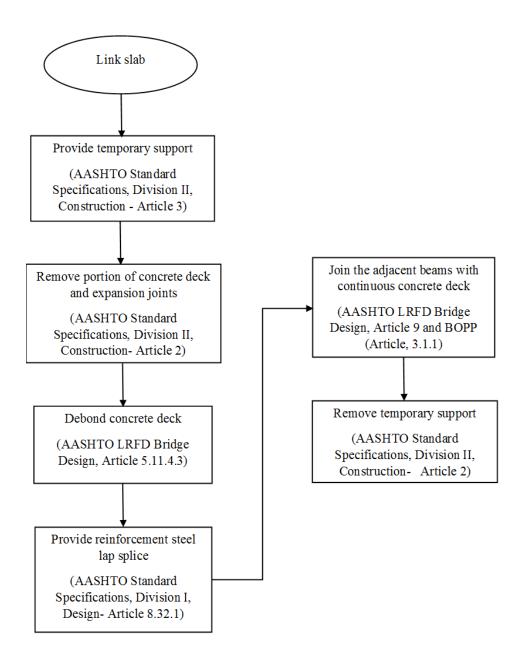


Figure 4.4 Link slab design process.

As shown in Figure 4.4, when considering rehabilitation with link slab, the process starts with following steps according to (Caner & Zia, 1998). While replacing the pin and hanger assembly with a link slab, the girder should be supported by temporary support beam and this support should be provided according to Standard Specifications, Division II-Construction (Article

3). Expansion joints and a portion of the concrete deck along the expansion joints are removed according to Standard Specifications, Division II-Construction (Article 2). Debond the concrete deck on each side of the beam at least 5% of the span length according to AASHTO LRFD Specifications, (Article 5.11.4.3) along the debonded region, the shear connectors are removed to prevent composite action. Further, the top flange of the girder is provided with debonding mechanism in the form of standard roofing tar paper which acts as a water proofing material. Provide reinforcement steel lap splice for continuity of deck reinforcement according to Standard Specifications, Division I-Design (Article 8.32.1). Join the adjacent beams with a continuous concrete deck according to AASHTO LRFD Specifications (Article 9) and BOPP Specifications (3.1.1). Finally, after construction temporary support should be removed according to Standard Specifications, Division II -Construction (Article 2).

#### 4.2.3 Catcher Beam System

This section summarizes the option that involves rehabilitation of pin and hanger assemblies with catcher beam system. Items that are discussed and presented in the corresponding flowchart incorporate relevant information from the literature search, DOT survey and appropriate federal and state specifications. A Secondary catcher beam system is provided to carry live loads across the expansion joint when the existing pin and hanger fails at the location of the pin and hanger assembly. The retrofit should be detailed to resist applied live load and the gap between the girder and the catcher beam must be kept as small as possible to the limit impact loading. To reduce impact, the use of auxiliary neoprene bearings on the catcher beam is also recommended (PennDOT, 2010). A flow-chart detailing general steps involved in the process is located in Figure 4.7.

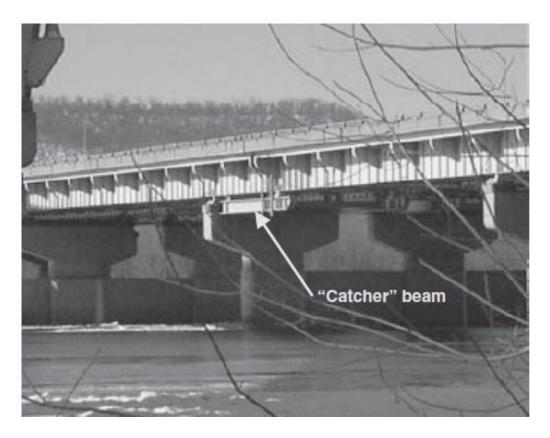


Figure 4.5 Catcher beam system. (Connor et al. 2005)

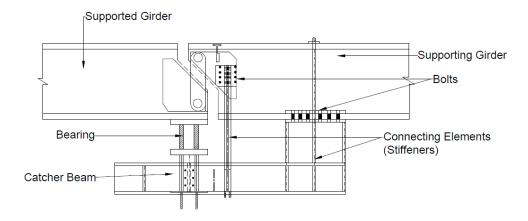


Figure 4.6 Catcher beam system representative detail.

#### Pros:

When pin and hanger assembly fails to carry the live load then catcher beam system should
be installed to carry the live load, which is an immediate option to replace and control the
sudden bridge collapse.

#### Cons:

• This is a temporary system, which works for very less number of years due to fatigue related problems in catcher beam system, and replacement needs to be considered.

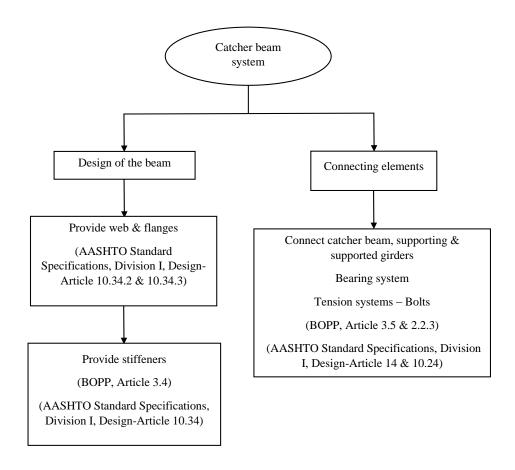


Figure 4.7 Catcher beam design process.

As shown in Figure 4.7, when considering retrofit of pin and hanger assemblies with catcher beam, the design process is explained below. Catcher beam system design consists of two components: design of the beam and connecting elements.

- Design of beam: The web and flanges of the beam is designed according to Standard Specifications, Division I-Design (Article 10.34.2 & 10.34.3). Stiffeners are designed according to Standard Specifications, Division I-Design (Article 10.34) and BOPP Specifications (Article 3.4).
- Connecting elements: For connecting the catcher beam and the supported girder, bearing systems are used and this bearing system is designed according to Standard Specifications, Division I-Design (Article 14). For connecting the catcher beam and the supporting girder, bearing systems and tension systems like bolts are designed according to Standard Specifications, Division I-Design (Article 14 & 10.24) and BOPP Specifications (Article 3.5 & 2.2.3).

#### 4.2.4 Replace with Ship Lap Joint.

This section summarizes the option that involves rehabilitation of pin and hanger assemblies with ship lap joint. Items that are discussed and presented in the corresponding flowchart incorporate relevant information from the DOT survey and state specifications.

The Massachusetts DOT has utilized a different type of pin and hanger replacement option they refer to as a "ship lap joint." In this option, which performs in similar fashion to the original pin and hanger assembly, bearings are used to carry loads at the joint location, with girder sections being modified to act as short "cantilevers" that transfer loads across the joint in shear and bending. This detail is depicted for a specific project, the I-91 viaduct in Springfield, Massachusetts, in

Figure 4.8, Figure 4.9 and in Appendix D1. A flow-chart detailing general steps involved in the process is located in Figure 4.10.



Figure 4.8 Ship lap joint at bearing at joint locations (Mass DOT, 2014).

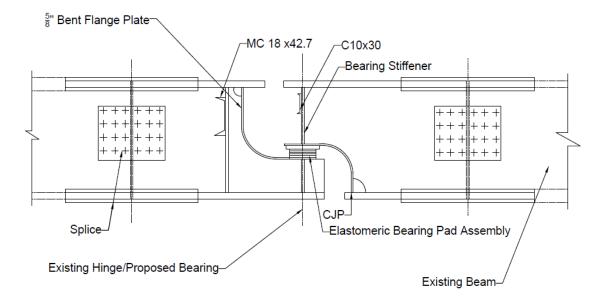


Figure 4.9 Ship lap joint detail (Mass DOT, 2014).

#### Pros:

• In the ship lap joint, support beam is carried by bearings, which improves rotational degree of freedom.

#### Cons:

- Still need to maintain joint which results in accumulation of debris and moisture and causes corrosion;
- Design and retrofit required for ship lap joint appears tedious compared to pin and hanger assemblies; and
- Fabrication and construction cost are more compare to pin and hanger assemblies.

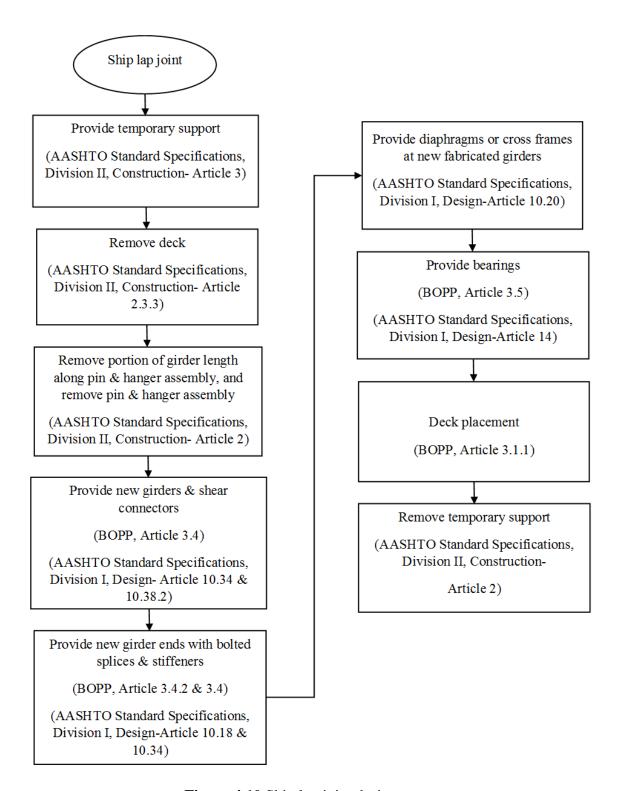


Figure 4.10 Ship lap joint design process.

As shown in Figure 4.10, when considering replacing the assemblies with ship lap joint, the process starts with following steps. While replacing the pin and hanger assemblies with a ship lap joint, the girder should be supported by a temporary support beam and this support should be provided according to Standard Specifications, Division II-Construction (Article 3). Then remove the deck according to Standard Specifications, Division II-Construction (Article 2.3.3). The portion of the girder length and the pin and hanger assembly are removed according to Standard Specifications, Division II-Construction (Article 2). Then provide new girders and shear connectors according to Standard Specifications, Division I-Design Standard Specifications (Article 10.34 & 10.38.2) and BOPP Specifications (Article 3.4). Then provide the new girder ends with bolted splices connection and stiffeners according to Standard Specifications, Division I-Design (Article 10.18 & 10.34) and BOPP Specifications (Article 3.4.2 & 3.4). Provide diaphragms or cross frames at new fabricated girders according to Standard Specifications, Division I-Design (Article 10.20). The support beam is carried by bearings which carries the loads at the joint locations and bearing systems are designed according to Standard Specifications, Division I-Design (Article 14) and BOPP Specifications (Article 3.5) which improves rotational degree of freedom. Further, place the deck according to BOPP Specifications (Article 3.1.1). Finally, after construction, temporary support beam should be removed according to Standard Specifications, Division II-Construction (Article 2).

#### 4.2.5 Replace with Pin and Hanger Assembly.

This section summarizes the option that involves removing pin and hanger assemblies and replacing them with new similar pin and hanger assembly. Items that are discussed and presented in the corresponding flowchart incorporate relevant information from the literature search, DOT survey and appropriate federal and state specifications.

When pin and hanger assembly is found to be frozen, they should be considered for examination and should be replaced with new pin and hanger assembly. The hanger plates and pins should be designed according to AASHTO Standard Specifications for Highway Bridges. While replacing the new pin and hanger assembly, the suspended span should be temporarily supported from below or above the deck. FHWA recommended to use new stainless steel pins and hangers according to AASHTO LRFD Bridge Design Specifications (Article 6.4.7), which reduces corrosion damage. Higher strength pins and larger hanger cross sections are also recommended to use so that by replacing existing assemblies with new, more durable components the assembly would be strengthened and maintenance requirements could be reduced. (Sirianni & Tricini, 2010).

From the DOTs survey, the approach of replacing new pins and hangers is programmed in more states than any other approaches. A flow-chart detailing general steps involved in the process is located in Figure 4.11.

#### Pros:

- Replacement with similar design can be cost efficient and cause minimal disruption to traffic; and
- By using stainless pins and hangers, corrosion could be controlled.

#### Cons:

- Still provides non-redundant system; and
- Pin and hanger assembly needs regular ultrasonic inspection every two years. So there is a higher inspection and maintenance cost.

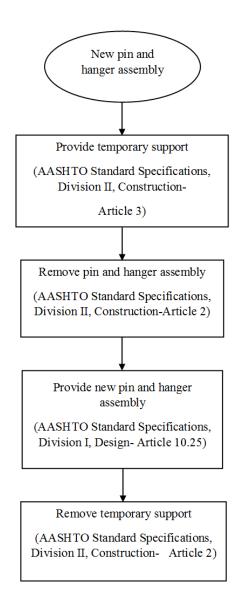


Figure 4.11 New pin and hanger assembly design process.

As shown in Figure 4.11, when considering replacing the assemblies with new assemblies, the process starts with following steps. When replacing the pin and hanger assemblies with new similar design section, the girder should be temporary supported and this support should be provided according to Standard Specifications, Division II-Construction (Article 3). Removal of the pin and hanger assembly is carried out according to Standard Specifications, Division II-Construction (Article 2). Then provide a new pin and new hanger according to Standard Specifications, Division I-Design (Article 10.25). Providing stainless steel pins and hangers are recommended to use and these are designed according to AASHTO LRFD Specifications (Article 6.4.7), which reduces corrosion damage. Finally, after construction, temporary support beam should be removed according to Standard Specifications, Division II-Construction (Article 2).

## 4.3 Summary

This chapter summarized and provided flowcharts that describes steps associated with completing feasible options associated with addressing pin and hanger assembly retrofit and/or replacement. The intention was that the described flowcharts will provide an organized decision-making tool that would assist NDOR personnel with assessing options and their consequences when pin and hanger assembly retrofit and/or replacement are being considered. The respective flowcharts in this chapter are designed based on the relevant information from the literature search, DOT survey and appropriate federal and state Specifications. These included the AASHTO Standard Specifications for Highway Bridges, the AASHTO LRFD Bridge Design Specifications and NDOR's Bridge Office Policies and Procedures (BOPP) manual.

## **Chapter 5 Recommendations for Future Research**

- In the present study, research work was related to the synthesis part of finding the different types of pin and hanger assembly retrofit and replacement options.
- The future research should focus on the analysis part of the different types of pin and hanger assembly retrofit and replacement options.
- The analysis part includes finding the behavior of the various retrofit and /or replacement option of steel pin and hanger assembly, and its effects on the behavior of the bridge with different retrofit and/or replacement options.
- The research mainly focuses on retrofit and replacement options and their effect on bridges due to distortion induced fatigue cracking at the connections between the girders, one of the severe problem of steel bridges. Fatigue analysis should be carried out by modelling and analyzing using finite element analysis.
- The development of a finite element models and analysis are planned for the bridges located in the Nebraska State.

#### References

- AASHTO Standard Specifications for Highway Bridges, 16th edition. (1996). American Association of State Highway and Transportation Officials , Washington D.C.
- AASHTO Bridge Construction Specifications, 3th edition. (2010). American Association of State Highway and Transportation Officials, Washington D.C.
- AASHTO LRFD Bridge Design Specifications, 7th edition. (2014). American Association of State Highway and Transportation Officials, Washington D.C.
- American Association for Public Opinion Research. (2015). "Standard Definitions", Final Dispositions of Case Codes and Outcomes Rate for Surveys.
- Banthia, V., Hengen, T., & Phillips, B. (2014). "Rehabilitation Works for Pinawa Bridge Over Winnipeg River,". In Transportation 2014: Past, Present, Future-2014 Conference and Exhibition of Transportation of Canada//Transport 2014.
- Bridge Condtion Report Procedures and Practices. (2011). Bureau of Bridges and Structures

  Division of Highways, Illinois Department of Transportation.
- Bridge Inspector's Reference Manual (BIRM). (2012). Volume 1, Federal Highway Administration, Publication No. FHWA NHI 12- 049.
- Bridge Office Policies and Procedures (BOPP). (2014). Nebraska Department of Roads, Bridge Division.
- Bridge Safety Inspection Manual 2nd Edition. (2010). Publication 238 Part IE:Evaluation Specifications, Pennsylvania Department of Transportation.
- Britt, M. F. (1990). "The Pennsylvania Department of Transportation's Auxiliary Support System Retrofit for Bridges with Nonredundant Pin and Hanger Details". *In Second Workshop on Bridge Engineering Research in Progress, Proceedings*.

- AASHTO Standard Specifications for Highway Bridges, 16th edition. (1996). American Association of State Highway and Transportation Officials , Washington D.C.
- AASHTO Bridge Construction Specifications, 3th edition. (2010). American Association of State Highway and Transportation Officials, Washington D.C.
- AASHTO LRFD Bridge Design Specifications, 6th edition. (2012). American Association of State Highway and Transportation Officials, Washington D.C.
- American Association for Public Opinion Research. (2015). "Standard Definitions", Final Dispositions of Case Codes and Outcomes Rate for Surveys.
- Banthia, V., Hengen, T., & Phillips, B. (2014). "Rehabilitation Works for Pinawa Bridge Over Winnipeg River,". In Transportation 2014: Past, Present, Future-2014 Conference and Exhibition of Transportation of Canada//Transport 2014.
- Bridge Condtion Report Procedures and Practices. (2011). Bureau of Bridges and Structures Division of Highways, Illinois Department of Transportation.
- Bridge Inspector's Reference Manual (BIRM). (2012). Volume 1, Federal Highway Administration, Publication No. FHWA NHI 12- 049.
- Bridge Office Policies and Procedures (BOPP). (2014). Nebraska Department of Roads, Bridge Division.
- Bridge Safety Inspection Manual 2nd Edition. (2010). Publication 238 Part IE:Evaluation Specifications, Pennsylvania Department of Transportation.
- Britt, M. F. (1990). "The Pennsylvania Department of Transportation's Auxiliary Support System Retrofit for Bridges with Nonredundant Pin and Hanger Details". *In Second Workshop on Bridge Engineering Research in Progress, Proceedings*.

- Caner, A., & Zia, P. (1998). "Behavior and Design of Link Slabs for Jointless Bridge Decks". *PCI Journal*, 43(1998):68-81.
- Chang, L. M., & Lee, Y. J. (2002). "Evaluation of Performance of Bridge Deck Expansion Joints".

  \*\*Journal of Performance of Constructed Facilities, 16(1),3-9.
- Christie, S., & Kulicki, J. M. (1991). "New Support for Pin-Hanger Bridges,". *Civil Engineering-ASCE*, 61(2).
- Connor, R. J., Dexter, R., & Mahmoud, H. (2005). "Inspection and Management of Bridges with Fracture-Critical Details". (No.Project 20-5(Topic 53-08)).
- Graybeal, B., Walther, R., & Washer, G. (2000). "Ultrasonic Inspection of Bridge Hanger Pins".

  \*Transportation Research Record: Journal of the Transportation Research Board,

  (1697),19-23.
- Kennedy Bridge Planning Study. (2014). Technical Memorandum, Bridge Rehabilitaion Alternatives, Minnesota Department of Transportation.
- Montana Structures manual- Part II. (2002). Chapter 22, Bridge Rehabilitation, Reference number: SS-10 Pin and Hanger Rehabilitation, Montana Department of Transportation.
- Mosavi, A. A., Sedarat, H., Emami-Naeini, & Lynch, J. (2011). "Finite Element Driven Damage Detection of a Skewed Highway Bridge with Pin and Hanger Assemblies".
- National Transportation Safety Board (NTSB). (1984). "Highway Accident Report Collapse of a Suspended Span of Interstate Route 95 Highway Bridge Over the Mianus River, Greenwich, Connecticut, June 28,1983," Report No. NTSB/HAR-84/03, NTSB, Washington D.C.
- New York State Route 5 Buffalo Skyway management Study Report. (2008). City of Buffalo, Erie County, New York Department of Transportation.

- Shirole, A. M., & Malik, A. H. (1993). "Seismic Retrofitting of Bridges in New York State,". *In Symposium on Practical Solutions for Bridge Strengthening and Rehabilitation*.
- Sirianni, C. M., & Tricini, J. (2010). "I- 579 Crosstown Boulevard Bridge Preservation Project".

  \*\*American Society of Highway Engineers.\*\*
- Structural Services Manual. (2015). Bureau of Bridges and Structures Division of Highways, Illinois Department of Transportation., Springfiled Illinois.

## **Appendix A**

## Survey

## Steel Pin and Hanger Assembly Replacement Options Inventory Survey

A number of steel beam bridges exist in the United States that contain steel pin and hanger assemblies. These assemblies were used to facilitate construction and to reduce the level of indeterminacy along a given beam line when the bridges were originally built. As the bridges continue to age, these assemblies have collected debris and moisture and, in certain instances, have deteriorated to a point where their retrofit or removal has been completed or is being considered. We are facilitating this survey on behalf of the Nebraska Department of Roads (NDOR) to explore how other agencies address pin and hanger assemblies that are aging and becoming deteriorated. Results from the survey can be provided to you upon request.

Section 1. General
<ol> <li>Do you have steel bridges that contain pin and hanger assemblies?              ○ Yes             ○ No → Go to Question 7 on page 3      </li> <li>If yes, please provide the number of steel bridge types for each category below that have pin and hanger assemblies. If you do not have a pin and hanger assembly for the steel bridge type, please write in '0'.</li> </ol>
Number of pin and hanger
Type of bridge assemblies
a. Two or three girder bridges
b. Four and more girder bridges
c. Truss bridges
d. Other, specify:
e. Other, specify:

Sect	tion 2.	Optic	ons					
	Does yo	d? Yes	ency view the pion		mblies as componen	ts that nee	d retro	fitted and/or
	2a. If yes, please provide the number of retrofit and/or replacement options that you have implemented or programmed for each category below. If you have implemented or scheduled retrofit and/or replacement options other than those listed below, please describe and provide the number for each option in the additional table rows. If you have not implemented or programmed the retrofit and/or replacement option listed, please write in '0'.							
						Numbe		Number
			ofit option			implemer	nted	programmed
		a.	Use a secondar	y system such as a	"catcher beam"			
		b.	Replace with ne	w pin and hanger	assembly			
		c.	Replace with bo	olted splice				
		d.	Other, specify:					
		e.	Other, specify:					
3. For the retrofits and/or replacements you indicated above as implemented or programmed, did you follow any of the designs, procedures, or criteria below?								
	а Δ	ASHT	O LRFD criteria a	nd procedures		Yes	No O	
				fication criteria and	d procedures	$\tilde{}$	~	
	J. 7.		o standard specif	nederon enteria an	a procedures	0	0	
4.	√°	Yes No	eloped your owi  → Go to questio	n 5 on page 3	edures for retrofits a	and/or repl	acemei	nts?

<ul> <li>5. Does your agency view the pin and hanger assemblies as components that need <u>no further action</u> at this time?</li></ul>	
Section 3. Future Contact	
<ul> <li>6. If you developed your own criteria and procedures for retrofits and replacements, would you be willing to share those with us?  Yes  No → Go to Question 10  Not applicable  6a. If yes, which format would you prefer to share those in?  Electronically  Hard copy</li> </ul>	
7. Would you like to receive the results of this study?  O Yes O No	
8. If you answered yes to Question 6 or 7, please provide your information below for us to contact you to either request your criteria and procedures, or to provide you the results of this study.  Name    First   Last	

9. Please use the space below to provide any additional comments.	
Thank you!	
That completes our questions. We greatly appreciate the time you have taken to complete this	
inventory survey. For your convenience, please use the postage-paid return envelope included in your questionnaire to the Bureau of Sociological Research.	our
Questions or requests from this survey can be directed to:	
Bureau of Sociological Research	
University of Nebraska-Lincoln PO Box 886102	
Lincoln, NE 68588-6102 Phone: 1-800-480-4549 (toll free)	
E-mail: bosr@unl.edu	

## **Appendix B**

## Response to Survey of DOTs

### **Question 1**

Other types of steel bridges that have pin and hanger assemblies other than listed are:

- Arizona DOT: Arch Bridge (85).
- Arkansas State Highway and Transportation Department: Arch deck (2).
- Alaska Department of Transportation and Public Facilities: Box girders (1).
- Colorado DOT: Tie down.
- Illinois DOT: Truss with eye bars & pins (1).
- Iowa DOT: Secondary highway steel girders, secondary highway truss.
- Michigan DOT: All girder bridges (1099).
- Minnesota DOT: Arch (1), Suspension (1).
- Ohio DOT: Riveted steel arch (2).
- Oregon DOT: RGDG (9).
- Utah DOT: Pinned arches (7), Suspension arch (1).
- Washington State DOT: Concrete box -2 (132).
- West Virginia DOT: Tied thru arch (1), Suspension bridge (1).

### **Question 2**

- Maine DOT: Superstructure replace (number implemented-1, number programmed -1).
- Massachusetts DOT: Ship lap joint (number programmed -1), replace p & h assembly with under running bearing beam (number implemented-1).
- Michigan DOT: Replace bridge (number implemented-1, number programmed -3).

- North Carolina DOT: Replace w/ concrete girder (number programmed -1).
- Nebraska Department of Roads: replace bridge or superstructure- (of the 102 pin and hanger bridges on the state system 50 are scheduled for replacement of either the entire bridge or the entire superstructure).
- Virginia DOT: replace Bridge.
- Wyoming DOT: suspension hanger/seismic (number implemented-1).

### **Question 4**

- Arkansas State Highway and Transportation Department: Internally developed.
- Illinois DOT: It is part of our structural services manual. Bureau of bridges and structures
   IDOT.
- Michigan MDOT: Our bridge replacement program prioritizes bridges with pins & hanger high enough to systematically replace the bridge with another (usually concrete) bridge.
- Missouri DOT: No set criteria. Details are case-by-case.
- Utah DOT: Is not documented.

### **Question 5**

- Alaska Department of Transportation and Public Facilities: Pin & hangers are functioning properly. No pack rust present.
- Colorado DOT: No section loss due to corrosion & no crack on hanger.
- Delaware DOT: We are not as concerned with pin & hanger assemblies for multi-beam bridges. Pin & hanger assemblies on truss bridges are treated as a fracture critical member and are scrutinized more.

- Iowa DOT: Proper inspection should identify deficiencies in time to address them without impacts to public safety.
- Louisiana Department of Transportation and Development: Bridges are in good condition.
- Montana DOT: Pins and hangers are usually inspected every 2 years and UT inspected every 4 years. With our relatively dry climate and large temperature swings the p & h assemblies usually stay moving as designed with little rust impact.
- Minnesota DOT: We will include repairs or improvements to pin and hanger elements as conditions warrant. We have not developed projects solely on pin and hanger detail unless condition justifies.
- North Carolina DOT: Inspection reports indicate the condition of the pin and hanger is "good".
- Nebraska Department of Roads: All bridges are inspected by certified inspectors at least every 2 years and all bridges that this agency manages directly have redundant secondary systems should failure occur.
- Nevada DOT: We haven't identified problems with the hangers, aside from minor corrosion.
- New Hampshire DOT: Framing plan varies from 10 to 7 girder lines, condition is satisfactory.
- Ohio DOT: We retrofit when they are deteriorated.
- Oklahoma DOT: We used ultrasonic inspection on our pins. No problems were found.
- Oregon DOT: We inspect & monitor p & h's and only r & r or provide supplemental support
  when their condition indicates a need.

- Pennsylvania DOT: We have retrofitted the inventory of 2 girder and truss bridges with suspended assemblies.
- South Dakota DOT: These assemblies are part of annual NBIS inspections and the pins get a periodic NDT inspection as well.
- Virginia DOT: We evaluate each one individually.
- Washington State DOT: Routine inspections and painting when needed.
- West Virginia DOT: We monitor during routine inspections and provide action as needed

## **Question 6**

• 10 states willing to share their own criteria and procedures for retrofit and or/replacements are:

	States willing to share their o	wn criteria and procedures for retorfit and or/replacen	nents
Name	Email	DOT	Preference for sharing
Michael Hill	mike.hill@ahtd.ar.go	Arkansas State Highway and Transportation Department	Electronically
Behrooz Far	behrooz.far@state.co.us	Colorado Department of Transportation	Electronically
Victor Veliz	victor.veliz@illinois.gov	Illinois Department of Transportation	Electronically
Anne Rearick	arearick@indot.in.gov	Indiana Department of Transportation	Electronically
Dave Powelson	dpowelson@dot.state.nh.us	New Hampshire Department of Transportation	Electronically
Tim Schwaglor	tschwaglor@nd.gov	North Dakota Department of Transportation	Electronically
Walter Peters	wpeters@odot.org	Oklahoma Department of Transportation	Electronically
Tom Macioce	tmacioce@pa.gov	Pennsylvania Department of Transportation	Electronically
Graham Bettis	graham.bettis@txdot.gov	Texas Department of Transportation	Electronically
Joshua Sletten	jsletten@utah.gov	Utah Department of Transportation	Electronically

## **Additional Comments**

- Arkansas State Highway and Transportation Department: We usually have 1 or 2 bridges a year that have pin/hanger issues. Our fix is normally to replace pin and hanger. Sometimes we keep the hanger and just flip it around. When we have wear we will bore and replace with bigger pins.
- Illinois DOT: As a result of a fractured pin is one of our structures in the mid 1990's the Illinois Department of Transportation developed an aggressive program for the replacement of pins and link assemblies. Between 1995 and 1997 over 90 structures on our primary system were retrofitted. Over 2000 pins and corresponding links or plate assemblies were replaced throughout the state. In general the retrofit replaced the old style "shoulder" pin (with no bushings) with a constant diameter solid pin made of a stronger material (Nitronic 60) using Teflon bushings. The intent was to provide a better pin assembly as well as one that was easier to inspect in the future.
- Iowa DOT: We have replaced bushings in pin & hanger assemblies due to corrosion/wear.
- Massachusetts DOT :For the replacement of the p & h assembly with the under running bearing beam, the detail looks just like a catcher beam except that the suspended span sits on a bearing on that beam and the p & h assembly was removed in its entirely.
- Michigan DOT: MDOT does not automatically view pin & hangers as needing replacement. We replace them on a case-by case basis based on condition and load capacity. Although pin & hangers are not utilized on new bridges, we do not have any focused efforts to remove them from our inventory.

- Mississippi DOT: We have replace pins & links on our large scale MS River crossing bridges in Watchez, MS. It is the only bridge we intend to remain in service with these details. The replacements were very large scale. These are long span truss bridges.
- Montana DOT: Our pin and hanger assemblies tend to work well. We have replaced pins
  over the years due to wear and also a few assemblies when they were ruined by impacts to
  girders from overweight loads.
- Minnesota DOT: MnDOT stopped building bridges w/ pin and hanger details in 1960's.
  We have not rehabilitated that many as the bridge width is typically too narrow therefore we have done mostly bridge replacements for those vintage. It has been over 10 years since last pin and hanger rehab and that one was caused by no cotter pin on pin and there was a condition concern the hanger may come off of pin. Call w/ questions.
- Missouri DOT: We only replace or repair them after they deteriorate. We don't have a
  program to do so.
- New Mexico DOT: Performs ultrasonic testing on all pins every 60 months. We have found and replaced compromised/broken pins.
- Ohio DOT: Number of retrofits performed you did not give a time frame for this work.
   This makes it difficult to answer. This type of work has gone on for many years. We do not track this work so there is no way to answer that question beyond the memory of current group.
- Utah DOT: Please contact me for additional details on the bridge retrofit projects we have completed or programmed. I would like a copy of the results.
- Wyoming DOT: The pin & hanger we replaced was due to damage from gunshot.

## **Appendix C**

## List of Abbreviations

Alabama Department of Transportation (ALDOT)

Alaska Department of Transportation and Public Facilities (Alaska DOT & PF)

American Association for Public Opinion Research (AAPOR)

American Association of State Highway and Transportation Officials, Load and Resistance

Factor Design (AASHTO LRFD)

Arizona Department of Transportation (ADOT)

Arkansas State Highway and Transportation Department (AHTD)

Average Daily Truck Traffic (ADTT)

Bridge Office Policies and Procedures (BOPP)

Bureau of Sociological Research (BOSR)

Colorado Department of Transportation (CDOT)

Delaware Department of Transportation (DelDOT)

Federal Highway Administration (FHWA)

Florida Department of Transportation (FDOT)

Fracture Critical Members (FCMs)

Georgia Department of Transportation (GDOT)

Hawaii Department of Transportation (Hawaii DOT)

Illinois Department of Transportation (IDOT)

Indiana Department of Transportation (INDOT)

Iowa Department of Transportation (IOWADOT)

Louisiana Department of Transportation and Development (LADOTD)

Maine Department of Transportation (Maine DOT)

Massachusetts Department of Transportation (Mass DOT)

Michigan Department of Transportation (MDOT)

Minnesota Department of Transportation (MnDOT)

Mississippi Department of Transportation (Mississippi DOT)

Missouri Department of Transportation (MoDOT)

Montana Department of Transportation (MDT)

National Bridge Inspection Standards (NBIS)

National Cooperative Highway Research Program (NCHRP)

National Transportation Safety Board (NTSB)

Nebraska Department of Roads (NDOR)

Nevada Department of Transportation (NDOT)

New Hampshire Department of Transportation (NHDOT)

New Mexico Department of Transportation (NMDOT)

New York State Department of Transportation (NYSDOT)

Non-destructive Testing (NDT)

North Carolina Department of Transportation (NCDOT)

North Dakota Department of Transportation (NDDOT)

Ohio Department of Transportation (ODOT)

Oklahoma Department of Transportation (OklahomaDOT)

Oregon Department of Transportation (OregonDOT)

Pennsylvania Department of Transportation (PennDOT)

Rhode Island Department of Transportation (RIDOT)

South Dakota Department of Transportation (SDDOT)

South Carolina Department of Transportation (SCDOT)

Tennessee Department of Transportation (TDOT)

Texas Department of Transportation (TxDOT)

Transportation Research Board (TRB)

Utah Department of Transportation (UDOT)

Virginia Department of Transportation, Central Office (VDOT)

Washington State Department of Transportation (WSDOT)

West Virginia Department of Transportation (WVDOT)

Wyoming Department of Transportation (WYDOT)

## Appendix D

## Table A.1 Summary

Summary of various retrofit and replacement options are briefly presented in the Table A1.

## **Table A 1: Summary of DOT Options**

Retrofit/replacement options	Pros	Cons	States that uses retrofit/replacement options	States that have drawings
<b>Bolted splices</b>	Eliminates non-redundant system, make structure more efficient.  Reduces and mitigate superstructure corrosion.	Need to re-evaluate superstructure behavior and capacity. Higher construction cost.	MaineDOT, MnDOT, NHDOT, UDOT.	
Link slab	Reduction of joints controls corrosion and moisture intrusion.	Structural damages-(thermal stress, shrinkage & creep).  Higher stress lead to fracture & cracking along the slab.		
Catcher beam system	Immediate option, controls sudden failure of bridge.	Temporary system.  Fatigue related problem replacement need to be considered.	AHTD, DelDOT, INDOT, MaineDOT, MassDOT, MnDOT, MoDOT, NCDOT, Oklahoma DOT, TDOT, WVDOT.	OklahomaDOT, PennDOT
Ship lap joint	Support beam carried by bearings, improves rotational degree of freedom.	Need to maintain joints.  Higher maintenance and initial construction cost.  Design, retrofit required are tedious compare to pin and hanger assembly.	MassDOT.	MassDOT
New pin and hanger assembly	Similar design can be cost-effective and minimal traffic disruption.	Regular ultrasonic inspection. Still provides non-redundant system.	IDOT, MnDOT, Mississippi DOT, MoDOt, UDOT, WYDOT.	IDOT, MichiganDOT

## Appendix D1

## Nebraska Department of Roads Design Plans

- S07507234 Bridge built in 1957, repaired and overlaid in 1982-1983 and re-decked in 2010. The re-deck plan eliminated the deck expansion joints and provided with bolted splices.
- S02611926 Bridge built in 1939, widened, re-decked and overlaid with asphalt in 1975, repaired and deck overlaid with concrete in 2009. The 2009 plan replaced some existing pins with new pins. Girder supported using temporary system during pin replacement
- 3. S01118443 Pin and hanger assembly bridge, built in 1945, and overlaid in 1983.
- 4. S05703867 Pin and hanger assembly bridge, built in 1934, and widened in 1962.
- 5. S07301232 Pin and hanger assembly bridge, built in 1933, widened and re-decked in 1973.

# (R<sub>2</sub>) 28 Janurary 2009

PROJECT NUMBER (R1) 8 August 2008

75-2(1064) 16

C.N. 22342

STRUCTURE NUMBER S075 07234



BRIDGE ENGINEER

DIVISION

BRIDGE SK R INDEX - BRIDGE

A GIRD R GIRD R REC

ROADS ROLLED' NO PO GENERAL

LOAD H-20 GENER
THE CHECKED BY VIK
- DEPARTMENT (

'-0" **LOAD** 

NEBRASKA

PLATTSMOUTH NORTH BRI

The existing structure was built under project 475(2)-1, dated 1957. Plans are available from the Bridge Division upon request.

The concrete bridge deck is designed by the empirical design method in accordance with AASHTO LRFD fourth edition.

The contractor may substitute any one of the alternate designs shown on the plans for the original design. All quantities are based on the original design and no additions or deductions will be allowed for the use of an alternate design.

All structural steel for stiffeners and all spilce material shall conform to the requirements of ASTM A709/A709M, Grade 50W weathering steel.

Nuts, boits and washers used in the assembly of weathering steel shall be Type 3.

All fasteners shall be 76" high strength bolts, ASTM A325.

Field tack welding of form hangers or miscellaneous hardware to any part of the

The girders for this bridge are not designed to resist any torsional or lateral forces due to temporary construction loads. The contractor must provide any temporary bracing necessary to support the dirder web and flanges against all torsional forces resulting from construction loads.

Concrete for slab, approach slabs and rails shall be class "478D", with a minimum 28-day strength of 4000 Psl.

All reinforcing steel shall be epoxy coated and conform to the requirements of ASTM A615/A615M, Grade 60 steel.

The minimum clearance, measured from the face of the concrete to the surface of any reinforcing bar, shall be 3", except where otherwise noted.

All dimensions shown are in horizontal plane only. No allowance have been made for vertical curve or roadway cross slope.

Girder shims that will be provided to the contractor account for dead load deflection due to the weight of the slab and rall only. The contractor is responsible for making the necessary adjustments for the particular forming system used to achieve the slab grades and elevations shown on the plans.

Required Construction as follows:

New Slab, Turndown and Ralis, New Appraoch Slabs and Grade Beams New Bearings at Abutments

Concrete Repair at Abutments if necessary
Add stiffeners (3x3x %angle where shown Spilce Top and Bottom Flanges at Pin and Hanger Systems

PREPARATION OF BRIDGE AT STA. 859+67.50 I EACH ABUTMENT NO. 1 EXCAVATION \_\_\_\_\_ 1 LUMP SUM ABUTMENT NO. 2 EXCAVATION .... I LUMP SUM CLASS 47BD-4000 CONCRETE FOR BRIDGES 216.1 CU. YD. 175.4 CU. YD. SLAB \_\_\_\_ HAUNCH \_ 1.3 CU. YD. 39.4 CU. YD. CONCRETE RAILS \_\_\_\_\_ STRUCTURAL STEEL FOR SUPERSTRUCTURE \_\_\_\_\_ 4110 LBS. EPOXY COATED REINFORCING STEEL .... 38520 LBS. SI AR 8595 LBS. CONCRETE RAILS \_\_ 10 EACH EXPANSION BEARING, TFE TYPE \_\_\_\_ 10 EACH BEARING DEVICE REPLACEMENT \_\_ GRANULAR BACKFILL \_\_ 85 CU. YD. SUBSURFACE DRAINAGE MATTING \_\_\_\_ 79 SQ. YDS. BROKEN CONCRETE RIPRAP \_ 500 TONS CONCRETE FOR PAVEMENT APPROACHES 216.5 CU, YD. CLASS 47BD-4000 \_ 152.3 CU. YD. SLAB 22.2 CU. YD. CONCRETE RAILS \_\_\_\_\_ 42.0 CU. YD. GRADE BEAM \_\_ EPOXY COATED REINFORCING STEEL FOR PAVEMENT APPROACHES 36775 LBS. 26435 LBS. SI AR 5805 LBS. CONCRETE RAILS \_\_ GRADE BEAM \_\_ 4535 LBS. PRECOMPRESSED POLYURETHANE FOAM JOINT, TYPE B \_ 95.5 LIN. FT. 261 LIN. FT.  $(R_2)$   $1\frac{1}{2}$ " CONDUIT IN BRIDGE.

OCHEGAL MOTER OLIMITITIES & THREY

GENERAL NOTES , QUANTITIES & INDEX	. 1
GENERAL PLAN & ELEVATION	2
PHASING PLAN	3
PLAN & ELEVATION OF ABUTMENT NO. 1	4
PLAN & ELEVATION OF ABUTMENT NO. 2	5
GRADE BEAM BILL OF BARS	6
GIRDER LAYOUT & FIELD SPLICE DETAILS	7
CROSS SECTION OF ROADWAY	8
PLAN VIEW OF SLAB AND TURNDOWN	9
SLAB BILL OF BARS	10
APPROACH SLAB	1.1
APPROACH SLAB SECTION AND DETAILS	12
RAIL ON APPROACH SLAB	13
BILL OF BARS - APPROACH SLAB	14

PROJECT NUMBER 75-2(1064) 16A

c.n. 22342 STRUCTURE NUMBER S075 07234

NO.

BRIDGE ENGINEER

4-0" 3-SPĀN AM GIRDER BRIDGE EN & REDECK LROAD NOTES

ROLLED BE/ WIDE

6

LOCATION PLATTSMOUTH NORTH
SKEW 42°30'
ROADWAY 32'-0"
DISIGN LIVE LOAD H-20
DISTAILED BY 13H
CHECKED BY VIX

DUNITY CASS
WY. NO. US-75
ER. POST. 72+34
FA. 859+67.50
ESTONED BY BN

Minimum Construction Clearance (\* 12'-0") Minimum Construction Clearance (\* 12'-0")

MINIMUM CONSTRUCTION CLEARANCES

(Normal to Railroad)

No Construction Activities or other Obstructions may be placed within these Limits.

\* Add 1.5 Inches per Degree of Track Curvature to the Horizontal Clearance Distance.

## RAILROAD NOTES

THE PROPOSED GRADE SEPARATION PROJECT SHALL NOT INCREASE THE QUANTITY AND/OR CHARACTERISTICS OF THE FLOW IN THE RAILROAD'S DITCHES AND/OR DRAINAGE STRUCTURES.

THE ELEVATION OF THE EXISTING TOP-OF-RAIL PROFILE SHALL BE VERIFIED BEFORE BEGINNING CONSTRUCTION. ALL DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE RAILROAD PRIOR TO CONSTRUCTION.

THE CONTRACTOR MUST SUBMIT A PROPOSED METHOD OF EROSION AND SEDIMENT CONTROL AND HAVE THE METHOD APPROVED BY THE RAILROAD.

ALL SHORING SYSTEMS THAT IMPACT THE RAILROAD'S OPERATIONS AND/OR SUPPORTS THE RAILROAD'S EMBANKMENT SHALL BE DESIGNED AND CONSTRUCTED PER CURRENT RAILROAD GUIDELINES FOR TEMPORARY SHORING.

ALL DEMOLITIONS WITHIN THE RAILROAD'S RIGHT-OF-WAY AND/OR DEMOLITION THAT MAY IMPACT THE RAILROAD'S TRACKS OR OPERATIONS SHALL BE IN COMPLIANCE WITH THE RAILROAD'S

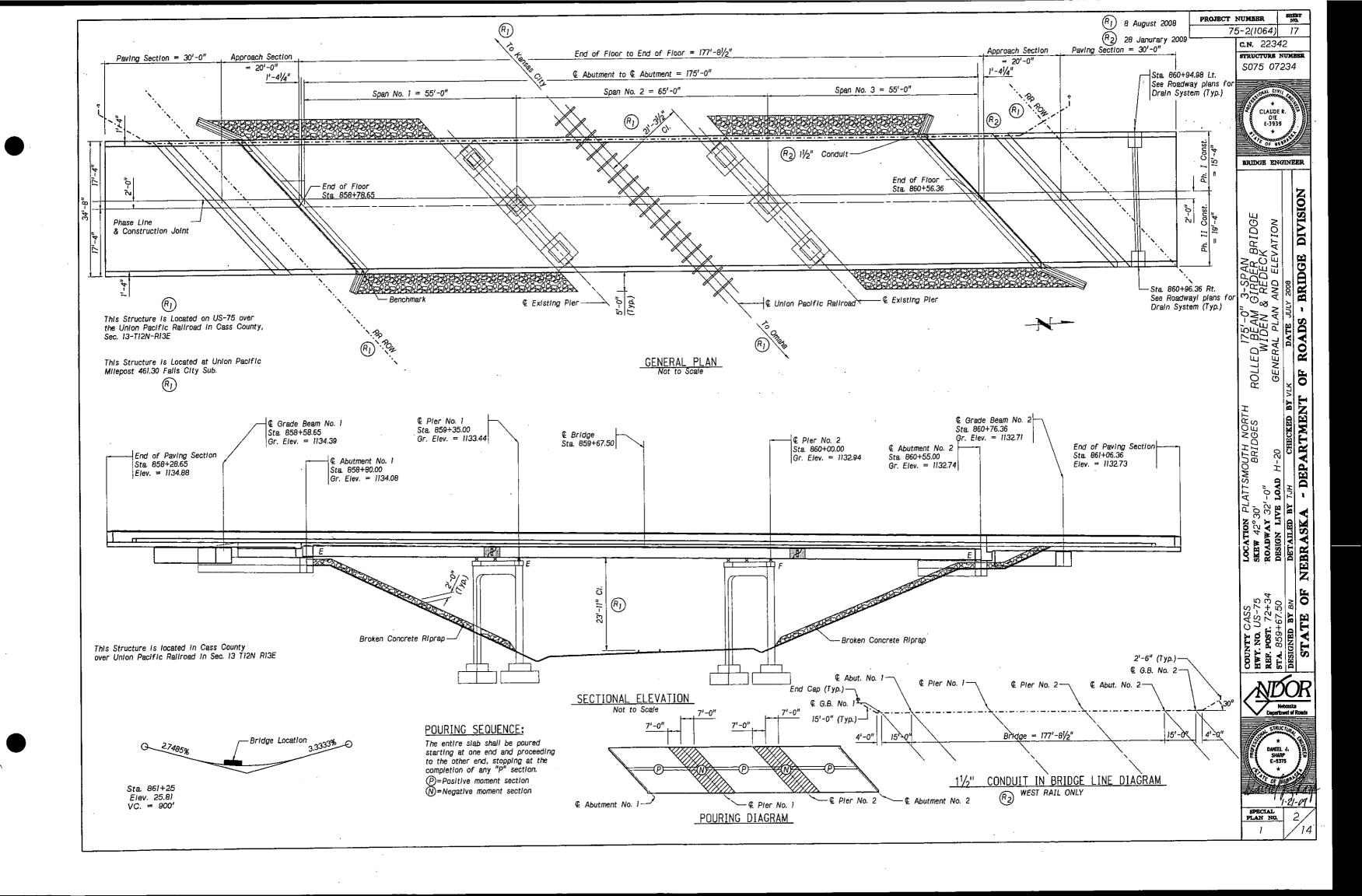
ERECTION OVER THE RAILROAD'S RIGHT-OF-WAY SHALL BE DESIGNED TO CAUSE NO INTERRUPTION TO THE RAILROADS OPERATION, ENABLING THE TRACK(S) TO REMAIN OPEN TO TRAFFIC PER THE RAILROAD'S REQUIREMENTS.

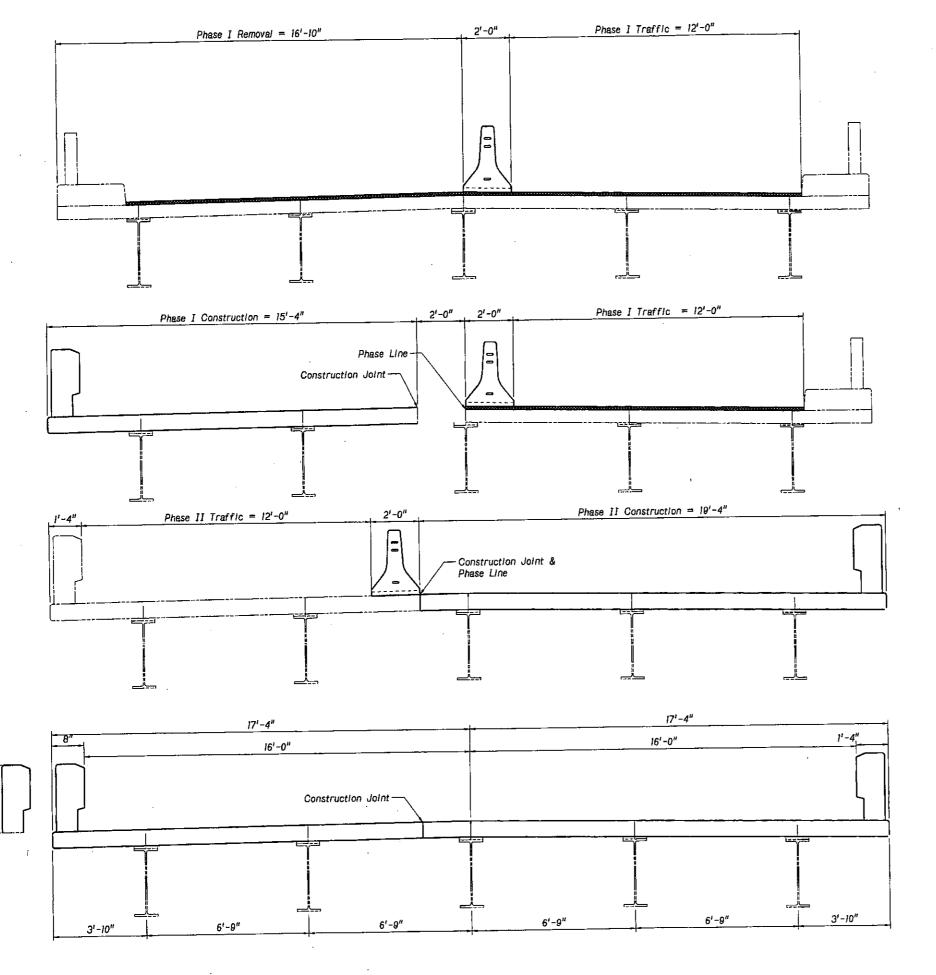
RAILROAD REQUIREMENTS DO NOT ALLOW WORK WITHIN 50 FEET OF TRACK CENTERLINE WHEN A TRAIN PASSES THE WORK SITE AND ALL PERSONNEL MUST CLEAR THE AREA WITH IN 25 FEET OF THE TRACK CENTERLINE AND SECURE ALL EQUIPMENT.

FALSE-WORK CLEARANCES SHALL COMPLY WITH MINIMUM CONSTRUCTION CLEARANCES.

ALL PERMANENT CLEARANCES SHALL BE VERIFIED BEFORE PROJECT CLOSING.

FOR RAILROAD COORDINATION PLEASE REFER TO THE RAILROAD MINIMUM REQUIREMENTS AS PART OF SPECIAL PROVISIONS.





Notes:

Concrete Protection Barriors will be anchored to the slab as per Special Plan 3C.
The barriers will be placed next to the break line and construction line, as shown. Due to low traffic speed the 1'-0" min. ledge is not required.

BRIDGE ENGINEER DIVISION 175'-0" 3-SPAN ROLLED BEAM GIRDER BRIDGE WIDEN & REDECK PHASING PLAN ROADS - BRIDGE LOCATION PLATTSMOUTH NORTH
SKEW 42°30'
ROADWAY 32'-0"
DESIGN LIVE LOAD H-20
DETAILED BY 7JH CHECKED BY VLK
F NEBRASKA - DEPARTMENT OF R BR. NO. US-75
BR. POST. 72+34
CA. 859+67.50
ESTGNED BY BN 6-27-08

SPECIAL PLAN NO.

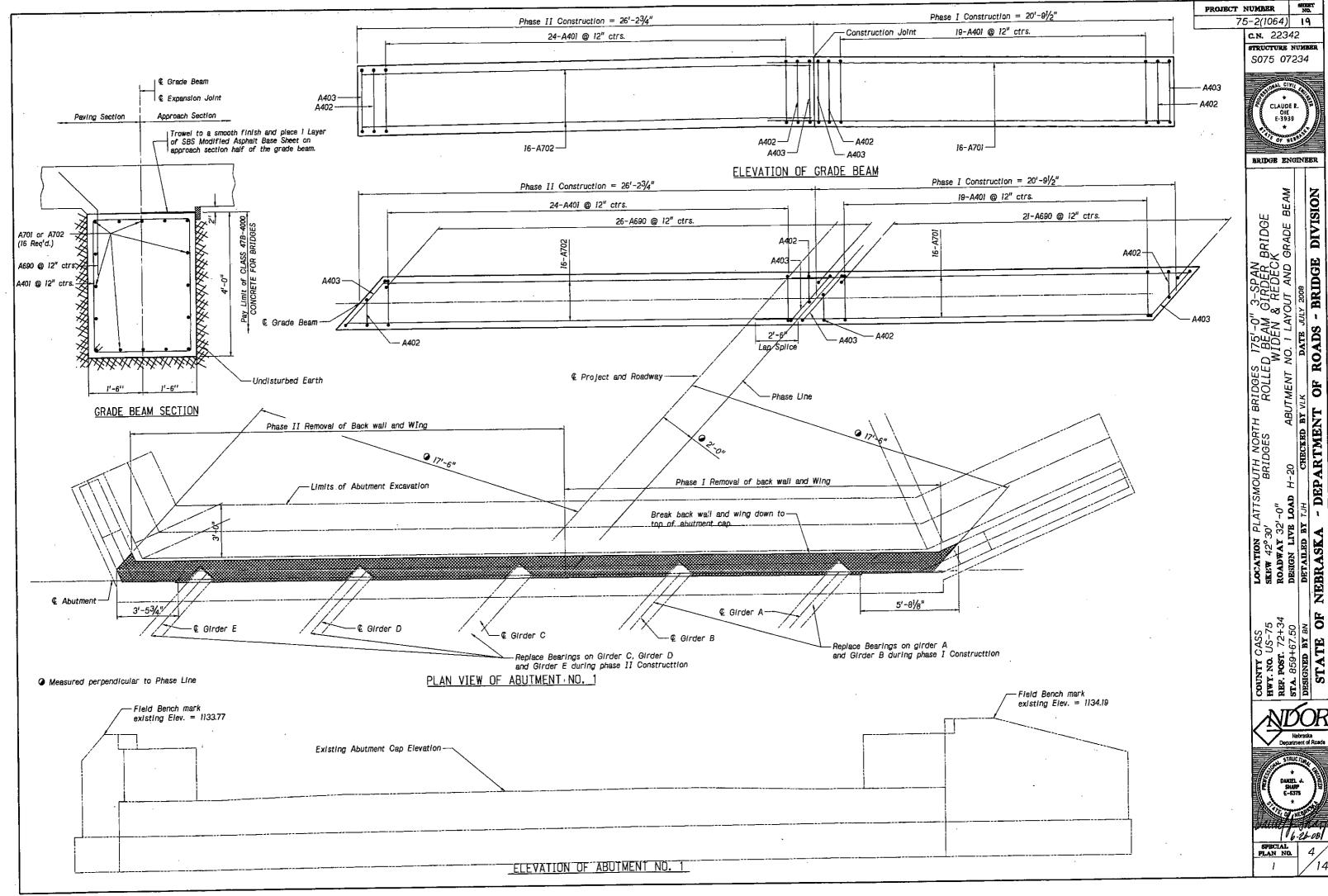
MA 11 20 0 00000 9

PROJECT NUMBER

75-2(1064) 18 C.N. 22342 STRUCTURE NUMBER S075 07234

SHEBT NO.

PHASING PLAN



M9 85:81:9 8005/85/9 8:15/10h (1779)01999

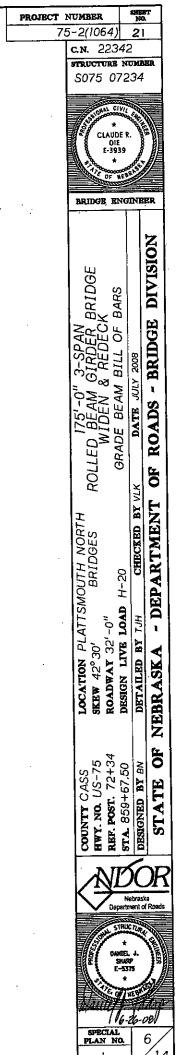
AARK	NUMBER	OF BARS I								T			WEDGIT.
		AL RUINA	LENCTH	TYPE	"A"	"B"	"C"	"D"	"E"	"F"	PIN	HOOK	WEIGHT
_	PHASE I	PHASE 2	LENGTH	TIPE	A					<u> </u>			LBS
										<del> </del>	.		749
47 <i>01</i>	16		22'-11"	STR.					<del> </del>	<u> </u>			842
4702	·	16	25'-9"	STR.						<del> </del>		<del> </del>	042
		<del>   </del>		1	01 011	11 511	11 011					<del> -</del>	241
4690	21	26	3'-5"	105	2"-0"	1-0	1-0		<del></del>	<del> </del>	-+-	<del>                                     </del>	
4 - 0 -			rai oli	107	21_611	21-611			<del>                                     </del>	-	2"	41/2"	366
		<del>/ +</del>								<del> </del>	2"	41/2"	28
		<del></del>									2"	41/2"	39
4403	- 2		14 -1	107	3 0	3.0			<del>                                     </del>				
	<del> </del>	<del>                                     </del>		<del> </del>									
	<del>                                     </del>	<del> </del>		<del>  -</del>					ļ				<u> </u>
											SUBTOT	AL =	2266 LE
									<u> </u>	<u> </u>		<u> </u>	740
A701	16		22'-11"	STR.					ļ	ļļ		<del>  -</del>	749 842
A702		16	25'-9"	STR.			<u> </u>	ļ	ļ <u></u>			<del> </del>	842
	<u> </u>								<u> </u>	<del> </del>			241
A690	21	26	3'-5"	105	2'-0"	1'-5"	1'-0"		<del> </del> -	<del> </del>		<del> </del> -	241
				107	ol oll	Ol Cit	ļ		├	<del>  </del>	2"	41/5"	366
				_			<u> </u>	<del> </del>	<del> </del>	<del> </del>		41/5"	28
									<del> </del>	<del>                                     </del>	2"	41/2"	39
A403	1 2	2		107	3 -0	3.3			<del>                                     </del>	<del>    -</del>	<del></del>	<del>  '`-</del>	<u> </u>
<u> </u>	<del> </del>			<del> </del> -		<del> </del>	<b>-</b>	i -		<del>  </del>		<u> </u>	
	A401 A402 A403 A403 A701 A702	A401 19 A402 2 A403 2 A701 16 A702 2 A401 19 A402 2	A401 19 24 A403 2 2 2 A403 2 2 2 A403 2 2 A701 16 A702 16 A690 21 26 A401 19 24 A402 2 2	A401 19 24 12'-9" A403 2 2 14'-7" A701 16 22'-11" A702 16 25'-9" A401 19 24 12'-9" A402 2 2 10'-7"	A401 19 24 12'-9" 107 A403 2 2 10'-7" 107 A701 16 22'-11" STR. A702 16 25'-9" STR. A401 19 24 12'-9" 107 A403 2 2 10'-7" 105	A401 19 24 12'-9" 107 3'-6"  A403 2 2 14'-7" STR.  A690 21 26 3'-5" 105 2'-0"  A401 19 24 12'-9" 5TR.  A690 21 26 3'-5" 105 2'-0"  A401 19 24 12'-9" 107 3'-6"  A402 2 2 10'-7" 107 3'-6"	A401 19 24 12'-9" 107 3'-6" 1'-5"  A701 16 22'-11" STR.  A702 16 25'-9" STR.  A401 19 24 12'-9" 107 3'-6" 1'-5"  A702 16 25'-9" STR.  A403 2 2 10'-7" 107 3'-6" 1'-5"  A702 16 25'-9" STR.  A401 19 24 12'-9" 107 3'-6" 1'-5"  A402 2 2 10'-7" 107 3'-6" 1'-5"  A403 2 2 14'-7" 107 3'-6" 1'-5"	A401 19 24 12'-9" 107 3'-6" 1'-5" 1'-0"  A701 16 22'-11" STR.  A702 16 25'-9" STR.  A690 21 26 3'-5" 105 2'-0" 1'-5" 1'-0"  A401 19 24 12'-9" 107 3'-6" 2'-6"  A402 2 2 10'-7" 107 3'-6" 3'-5"  A702 16 25'-9" STR.  A690 21 26 3'-5" 105 2'-0" 1'-5" 1'-0"  A401 19 24 12'-9" 107 3'-6" 2'-6"  A402 2 2 10'-7" 107 3'-6" 1'-5"  A403 2 2 14'-7" 107 3'-6" 3'-5"	A401 19 24 12'-9" 107 3'-6" 1'-5" 1'-0"  A403 2 2 14'-7" 107 3'-6" 3'-5"  A409 21 26 3'-5" 105 2'-0" 1'-5"  A409 21 26 3'-5" 105 2'-0" 1'-5" 1'-0"  A409 21 26 3'-5" 105 2'-0" 1'-5" 1'-0"  A401 19 24 12'-9" 107 3'-6" 2'-6"  A402 2 2 10'-7" 107 3'-6" 2'-6"  A403 2 2 14'-7" 107 3'-6" 1'-5"  A403 2 2 14'-7" 107 3'-6" 3'-5"	A401 19 24 12'-9" 107 3'-6" 1'-5" 1'-0"  A403 2 2 14'-7" 105 2'-0" 1'-5"  A702 16 25'-9" STR.  A401 19 24 12'-9" 107 3'-6" 2'-6"  A403 2 10'-7" 107 3'-6" 1'-5"  A40401 19 24 12'-9" 107 3'-6" 2'-6"  A405 2 2 14'-7" 107 3'-6" 2'-6"  A406 2 2 10'-7" 107 3'-6" 2'-6"  A407 2 2 14'-7" 107 3'-6" 2'-6"  A408 2 2 14'-7" 107 3'-6" 1'-5"  A409 2 2 14'-7" 107 3'-6" 1'-5"	A401 19 24 12'-9" 107 3'-6" 2'-0" 1'-5" 1'-0"  A403 2 2 14'-7" 107 3'-6" 3'-5"  A702 16 25'-9" STR.  A690 21 26 3'-5" 105 2'-0" 1'-5" 1'-0"  A401 19 24 12'-9" 107 3'-6" 2'-6"  A402 2 2 10'-7" 107 3'-6" 1'-5"  A403 2 2 14'-7" 107 3'-6" 1'-5"  A400 19 24 12'-9" 107 3'-6" 2'-6"  A402 2 2 10'-7" 107 3'-6" 1'-5"  A403 2 2 14'-7" 107 3'-6" 1'-5"	A401   19   24   12'-9"   107   3'-6"   2'-6"   2"   2"   2"   2"   2"   2"   2"	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

Granular Backfill

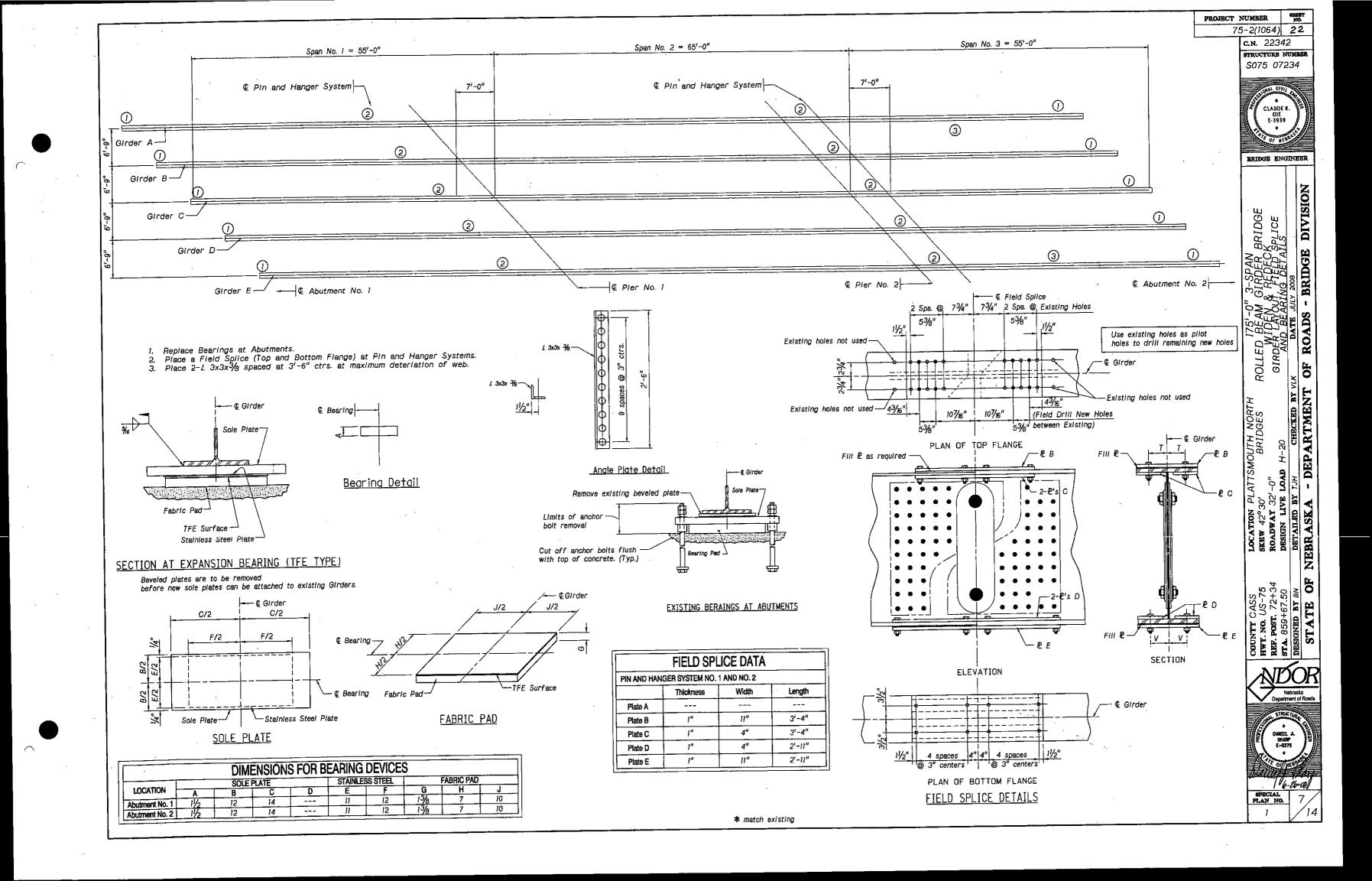
Oranular Backfill

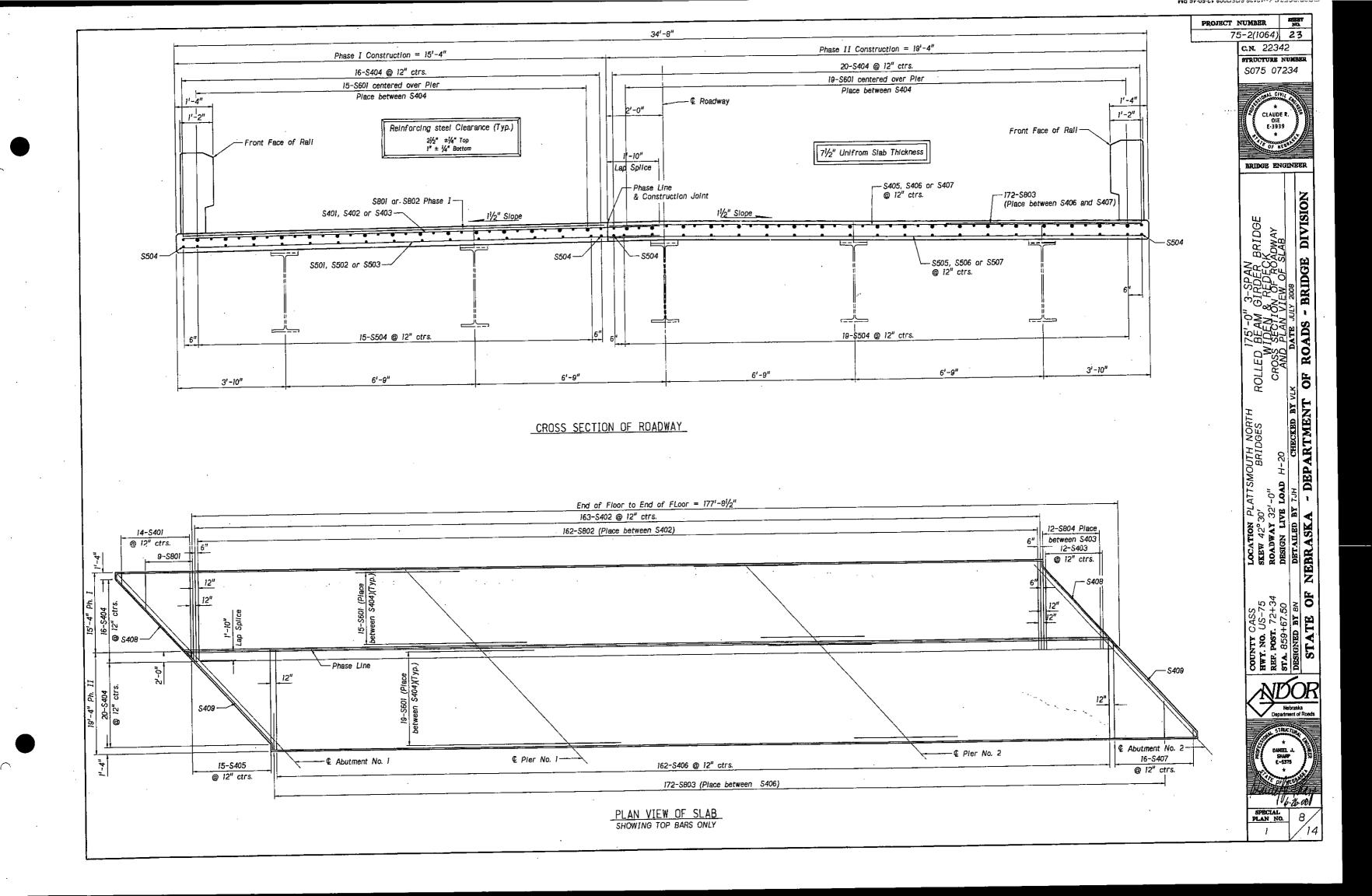
Place fabric side of subsurface drainage matting toward backfill.

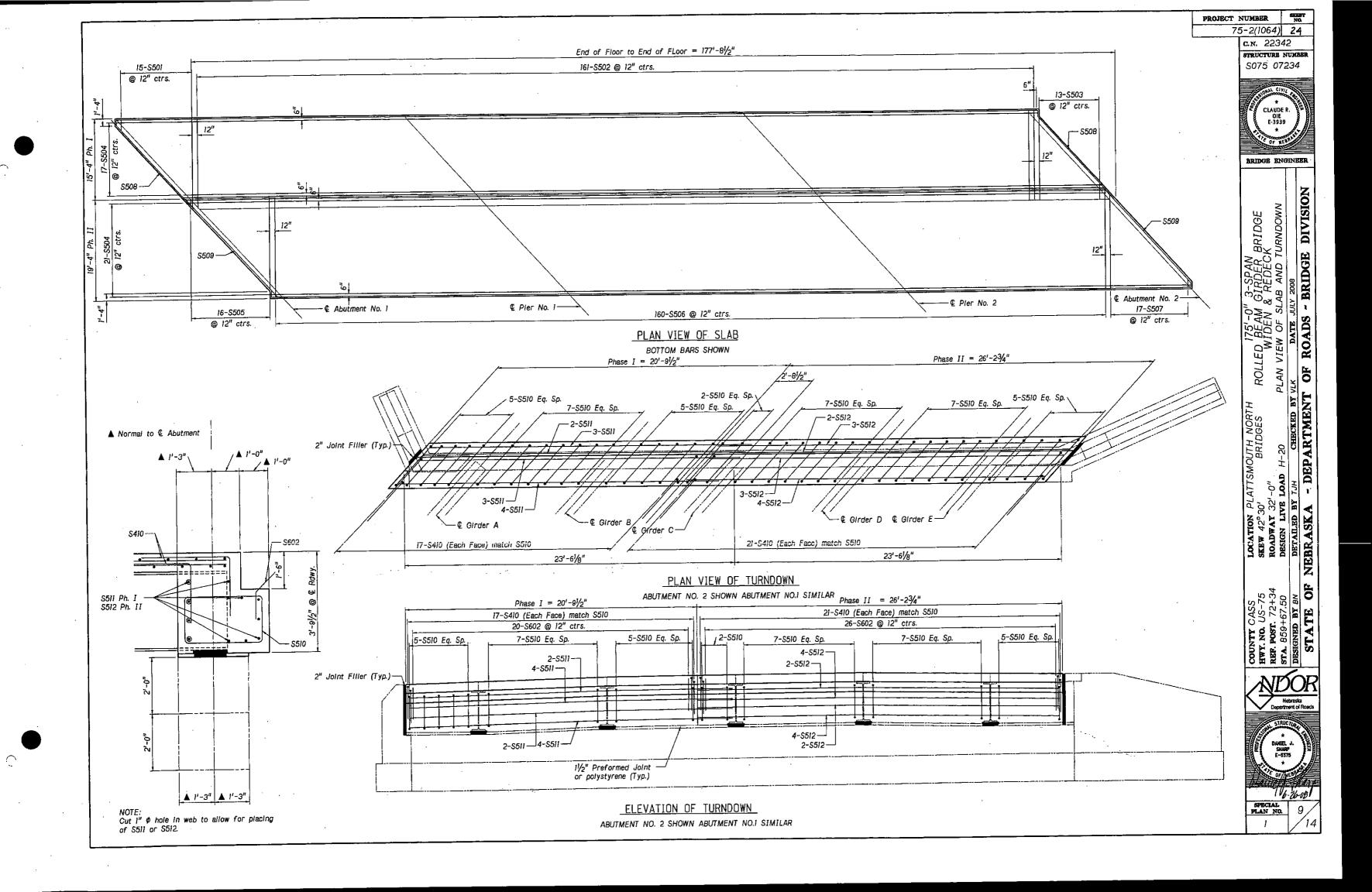
DRAINAGE DETAIL AND GRANULAR BACKFILL



Sheet F







								D 4				<del> </del>	·		
		· -	<del> </del>	B 1	L L	. '	0 F	B A	R S			1	1		WEIGHT
	MARK	NUMBER Phase 1		LENGTH	TYPE	"Å"	"B"	"C"	"0"	"E"	"F"	_	PIN	HOOK	LBS
ŀ	S80I	9	I IIRSE E	Avg. 9'-9"	STR.										234
ŀ	· S802	162		14'-10"	STR.	-	<u> </u>								6416
H	S803	102	172	6'-6"	STR.			T							2985
ŀ	S804	12	112	Avg. 9'-5"	STR.			···							302
ŀ	3004	12		71g, 0 0											
ŀ	S601	30	38	28'-0"	STR.		<del></del>	<del></del>				<u> </u>		_	2860
ł	S602	40	52	3'-0"	105	1'-6'	' 1'-6"	10"			-				4/5
ŀ	5602	40	32	3-0	100	, ,	<del>-                                     </del>	<del></del>		··· <del>··</del>	_	1	i- i		
ŀ	0501			Avg. 9'-4"	STR.		$+ \cdots$					1			146
ŀ	S501	15		16'-11"	STR.							<del>                                     </del>			2841
1	S502	161						<del></del>					-		134
ļ	S503	13		Avg. 9'-11"	STR.			<del> </del>	Includes	1 - 21-	6" lan	Sollos			7421
Ļ	S504	17	21	187'-3"	STR.		_		Triciages	4 - 2	6 Lap	Spirce	<del> </del>	<del></del>	157
Į	S505	ļ	16	Avg. 9'-5"	STR.						ļ	-	+		3185
	S506	<u> </u>	160	19'-1"	STR.	<u>:</u>					<del> </del>		<del> </del>		171
	S507		17	Avg. 9'-8"	STR.				<b>├</b> ──		<del> </del>		ļ	<del></del>	48
ſ	\$508	2		22'-11"	STR.		<u> </u>				<u> </u>		<del> </del>		54
, [	S509	L	2	25'-11"	STR.				ļ		<u> </u>		F1/	2!/	
۱	\$510	34	42	10'-9"	107	1'-6	" 3'-5		<u> </u>	ļ <u>.</u>	<u> </u>		51/2	2!/2	852
	S511	24		22'-11"	STR.				<u> </u>		<del> </del>	<b></b>	<del> </del>		574
İ	S512		24	25'-9"	STR.				<u> </u>	ļ	ļ <u> </u>		<del> </del> -	ļ	645
1												ļ·.	<del></del>		ļ
ļ	S401	14		Avg. 9'-2"	STR.								<del></del>		86
l	\$402	163		16'-11"	STR.										1842
	5403	12	i	Avg. 8'-11"	STR.										71
	\$404	16	20	185'-3"	STR.				Includes	4 - 2'	-0" Lap	Splice	1		4455
	\$405	<del>                                     </del>	15	Avg. 9'-5"	STR.								1		94
	\$406	<del> </del>	162	19'-1"	STR.										2065
	5407	<del>                                     </del>	16	Avg. 9'-8"	STR.										103
	\$408	2	- 70	22'-11"	STR.		_						Ţ		31
	S409	<del>-</del> -	2	25'-11"	STR.		$\neg$				T				35
	\$410	68	82	3'-0"	104	1'-6	" 1'-6	"	1					Į.	301
	3470	00	<u> </u>										CLIDIOT		8522 LB
		,	1			1	<del></del>		1			<del></del>	SUBTOTA	4L - 3	0022 LD
						-	21 2		<del> </del>		<del> </del>	<del> </del>	33/4"	-	2104
LIDOL	S591	178	178	5'-8"	104	2'-10			<del> </del>	<del> </del>	├	<del>  -</del>	33/4"		2228
<u> </u>	S592	178	178	6'-0"	104	3,-0	)" 3'-0	<u> </u>	Include	4 2	Cit I an	l colleg	374		3906
-	\$593	10	10.	187'-3"	STR	<u> </u>	<u> </u>		Include	5 4 - 2	_o ran	T Spince	<del> </del>	-	3300
)	<u> </u>	<u></u>	<u> </u>			_			<del> </del>	ļ	<del> </del>	+	11/.11	4"	257
5	\$391	89	89	5'-4"	107	1'-6	" 0'-10	<u>)"</u>	<del> </del>	ļ	1	<b>_</b>	11/2"	4	357
					<u> </u>	<u> </u>			<u> </u>	1	<del> </del>		+	<del></del>	-
1									<del> </del>	ļ	<b> </b>			ļ —	<del> </del>
2	<u> </u>							·	ļ		<u> </u>		<del> </del>	<b>↓</b>	-
		1								<u> </u>				1	<u> </u>
													SUBTOT.		595 LE
_		В	AR SE	TS					AR SET					AL = 4	7117, LE
	1100	MAX.	MIN.	NO.	BAI		MARK	MAX.	MIN.	NO.	_   _ 6	IARS			
N	MARK	LENGTH	LENGTH		PER		MARA -	LENGTH	LENGTH	OF SE	IS PE	R SET			
	801	14'-8"	4'-10"	1	9										
	804	15'-5"	3'-5"		12	2									
_	-														
9	5501	16'-8"	2'-0"	1	15	<del>,  </del>									
_	503	16'-11"	2'-11"		13	_						]			
_	505	17'-7"	1'-3"		16										
_	5507	17'-10"	1'-6"		17										
-	,507	,, ,,	<del>                                     </del>	<del></del>	† <del>''</del>	_+		<u> </u>	l						
-	5401	16'-3"	2'-1"	1	14	+									
_	403	14'-11"	2'-11"		12	$\overline{}$			1	<del>                                     </del>					
_					18	_		<del> </del>		<del> </del>	$\dashv$	$\overline{}$			
٠,	3405	17'-7"	l'-3"		10	$\overline{}$		<del></del>	<del></del>	+	+				
_	5407	17'-10"													

N:\brdge\ebasesheets\bilbar2.dgn

NOTE: FOR BENDING DIAGRAMS, HOOK LENGTHS & PIN DIAMETERS SEE SHEET 14 OF 14.

PROJECT NUMBER NO.

75-2(1064) 25

C.N. 22342

STRUCTURE NUMBER S075 07234



ROADS - BRIDGE DIVISION ROLLED BEAM GIRDER BRIDGE WIDEN & REDECK SLAB BILL OF BARS

 COUNTY CASS
 LOCATION PLATTSMOUTH NORTH

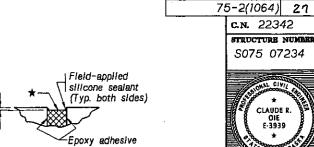
 HWY. NO. US-75
 SKEW 42°30′
 BRIDGES
 ROLL

 STA. 859+67.50
 DESIGNED BY BW
 DETAILED BY TUH
 CHECKED BY VK

 STATE OF NEBRASKA - DEPARTMENT OF



MA 60 ta 8 8005いている みとしたしっち ひてヨコバリタタタ



BRIDGE ENGINEES

Predicate the Contraction of the

C.N. 22342

STRUCTURE NUMBER S075 07234

PROJECT NUMBER

DIVISION

BRIDGE K GIRD & REL SLAB

ROADS

BRIDGE

P

- DEPARTMENT

NEBRASKA

P.O.

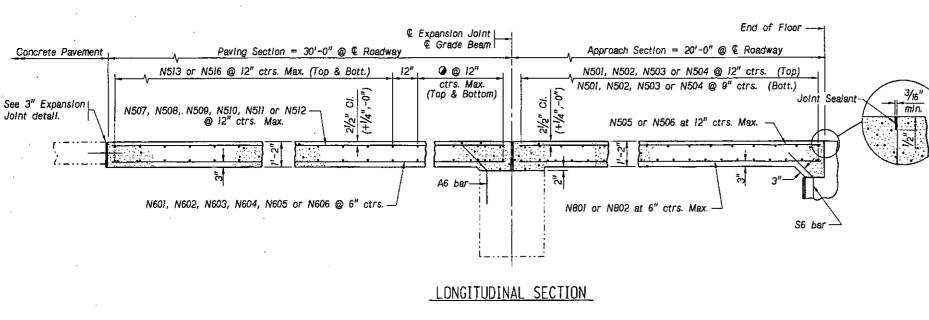
ROLLED

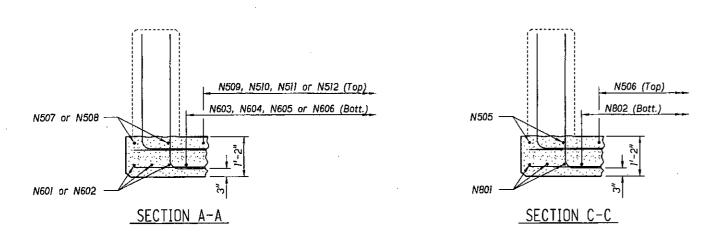
H-20 .-0,, **LOAD** 

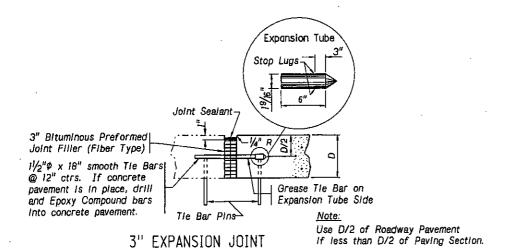
STATE



DETAIL "D' ★ Factory applied & cured silicone facing € Expansion Joint |\_ © Grade Beam Paving Section Approach Section X" Open Joint Precompressed Polyurethane Foam, Type B (See Detail "D") Polystyrene -Granular Backfill -Place 3" x 6" of Polystyrene on top of the Granular Backfill prior to pouring the concrete slab. Place 1 Layer of SBS Modified Asphalt Base Sheet on approach section half of the grade beam. SECTION B-B Measured at 50°F. Gap width shall be decreased /g" for every Y°F. Increase in temperature above 50°F. Gap width shall be increased /g" for every Y°F. decrease in temperature below 50°F. Y° = 11.4°F @ Grade Beam No. 1 Y° = 21.2°F @ Grade Beam No. 2 Concrete Rall Width = 1'-2". See sheet 13 of 14 for placement of rall reinforcement. See Standard Specifications for tining and finishing of approach slabs. SBS MODIFIED ASPHALT base sheets and all other miscellaneous items shall be considered







- End of Floor 8 ga. Galvanized plate — extend from edge to edge of deck, Rout and seal. Stabilized plate during Anchor

ALTERNATE JOINT DETAIL AT END OF FLOOR

To be used if approach slab is poured continuous with bridge deck.

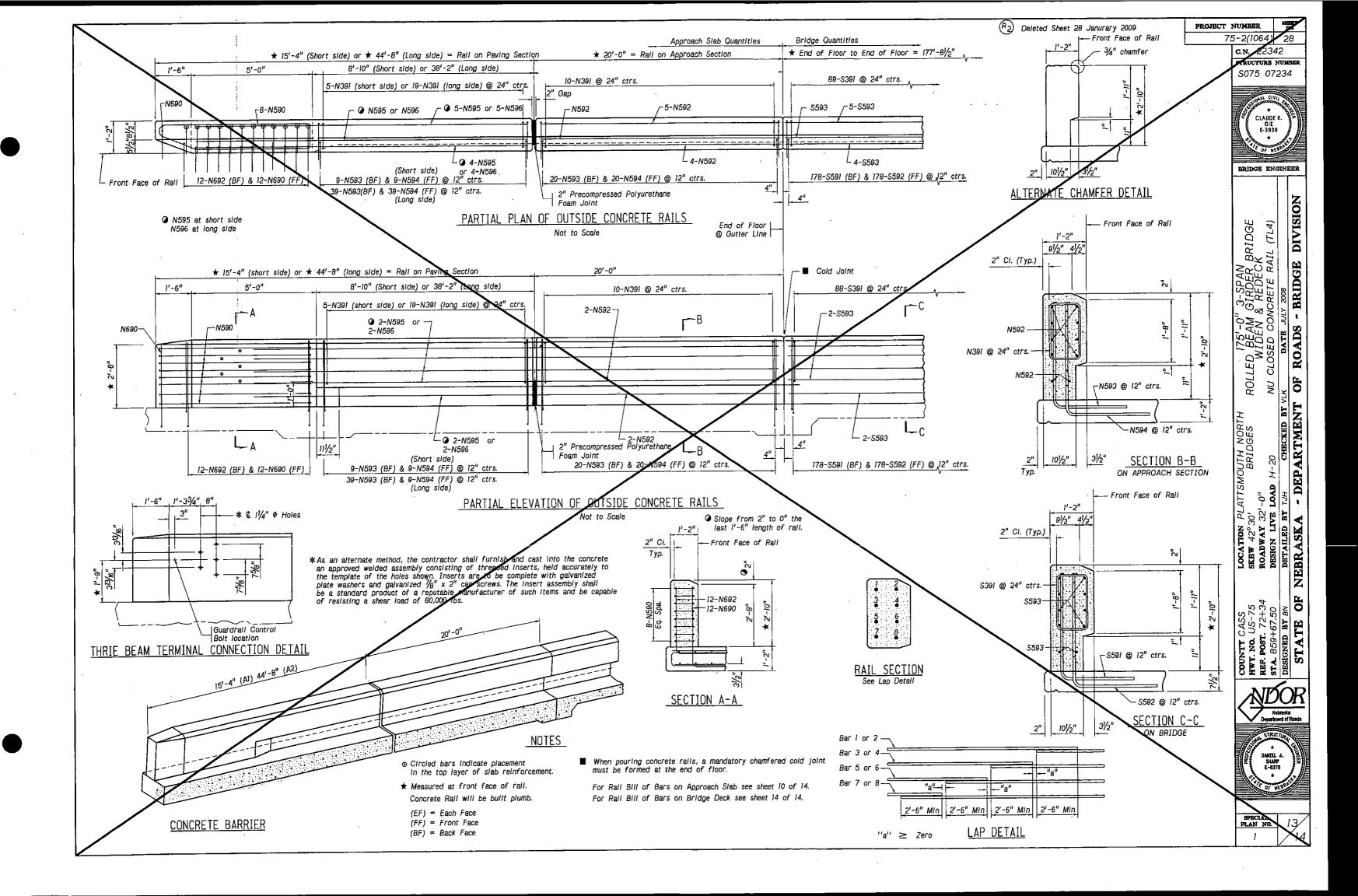
APPROACH SLAB NOTES:

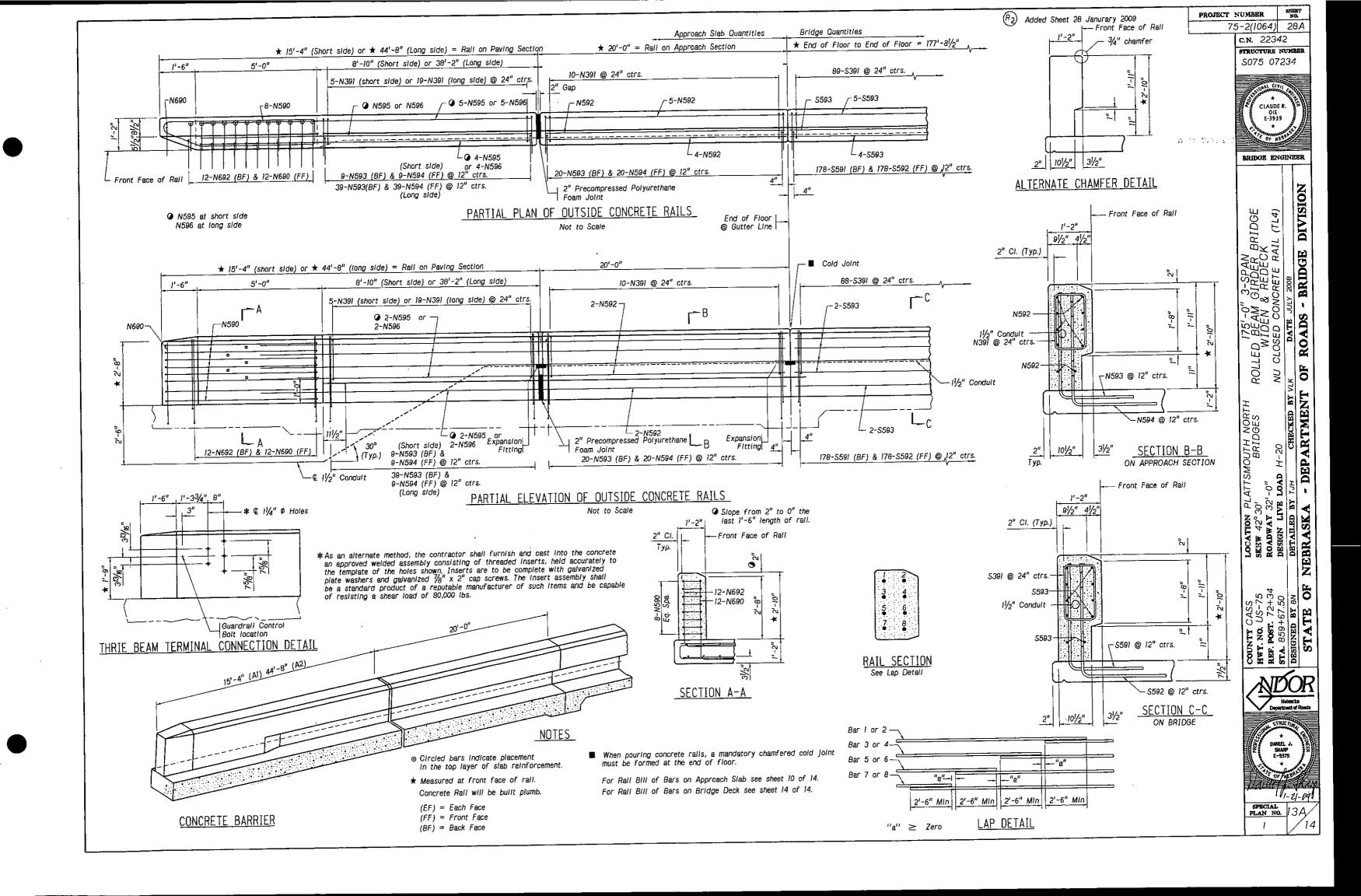
subsidiary to the pay item, CONCRETE FOR PAVEMENT APPROACHES CLASS 47BD-4000.

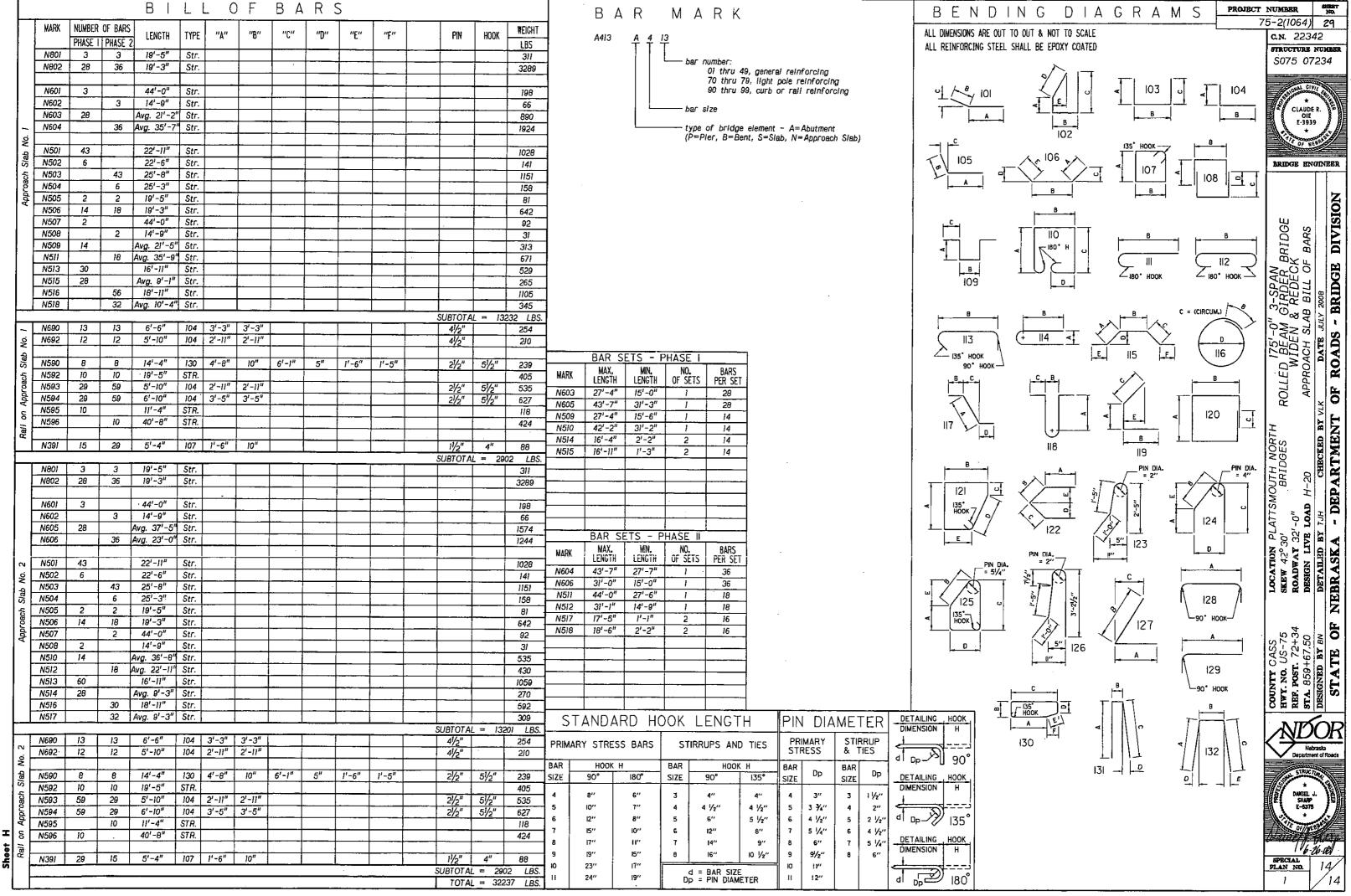
SBS MODIFIED ASPHALT base sheets shall be modified bitumen roofing material, with a minimum thickness of 0.000 inch and a minimum weight of 60 lbs. per 100 sq. feet.

The expansion gap between approach section and paving section shall be cleaned of all foreign matter before the installation of the expansion device or the filler material. **★** Working points are located at the intersection of the edge of clear roadway and **©** Grade Beam.

★ Dimensions measured at edge of clear roadway.



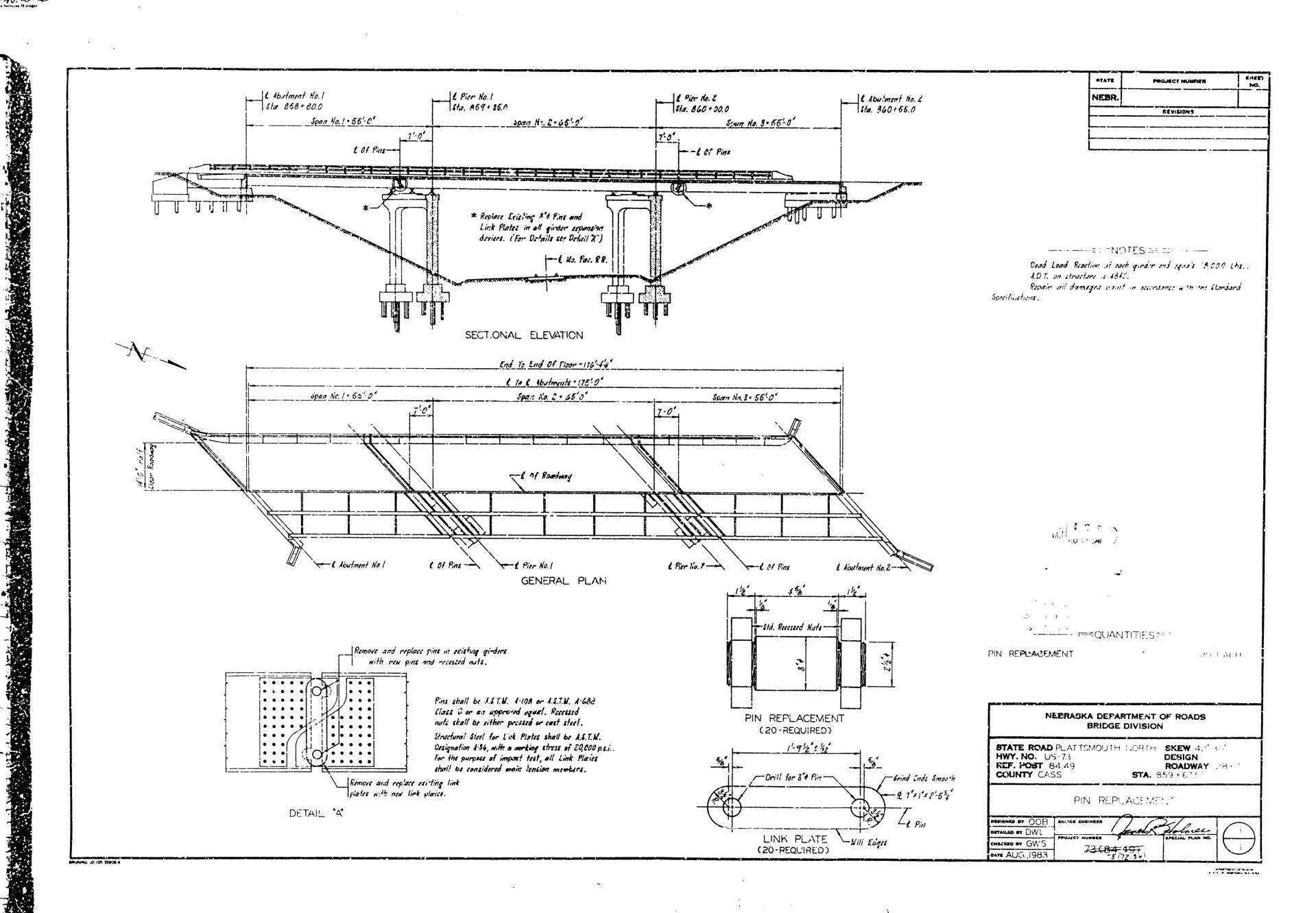




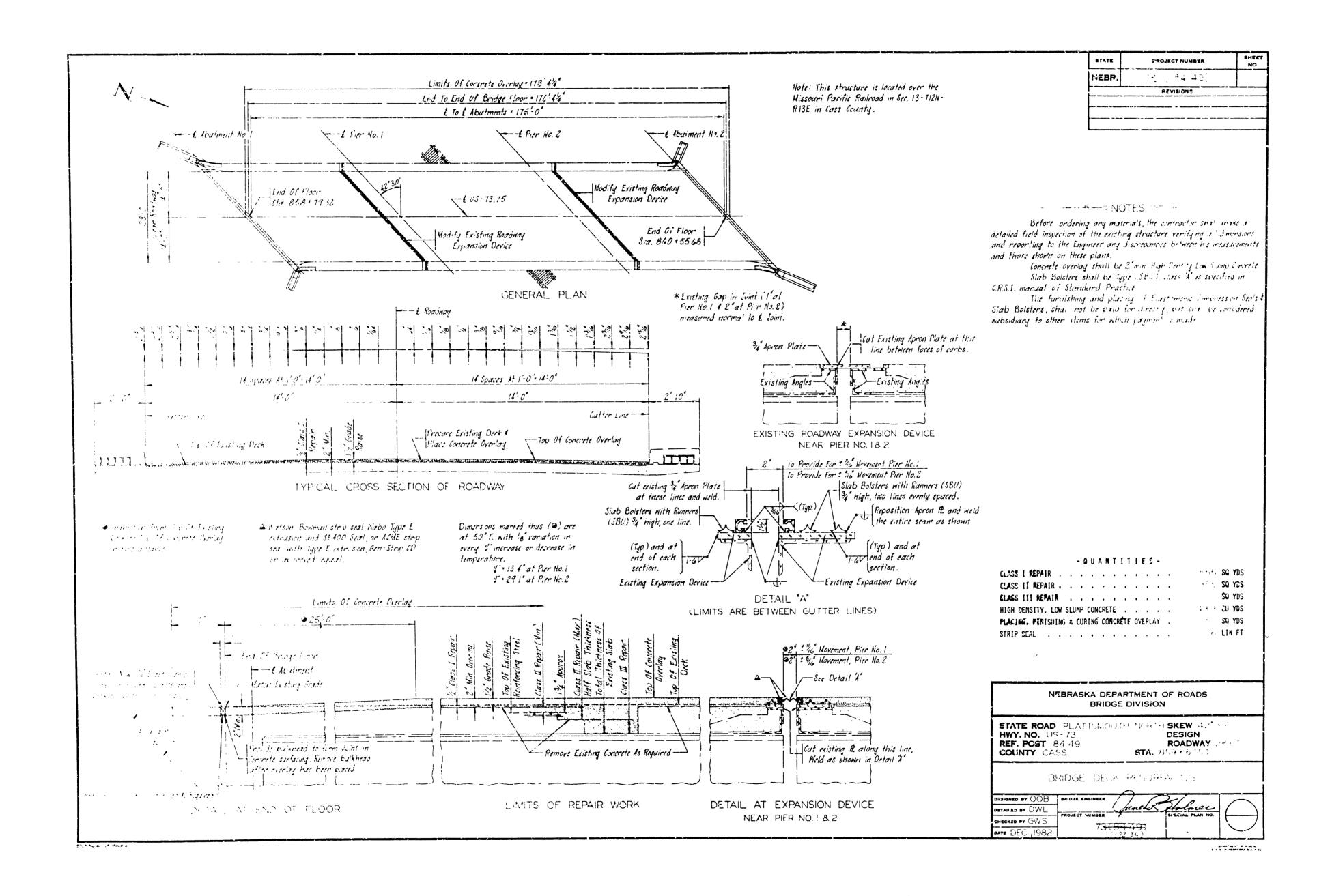
DEPARTMENT OF ROADS OFFICE SERVICES SECTION CERTIFICATE OF AUTHENT CITY

Date . "Wick 1986.

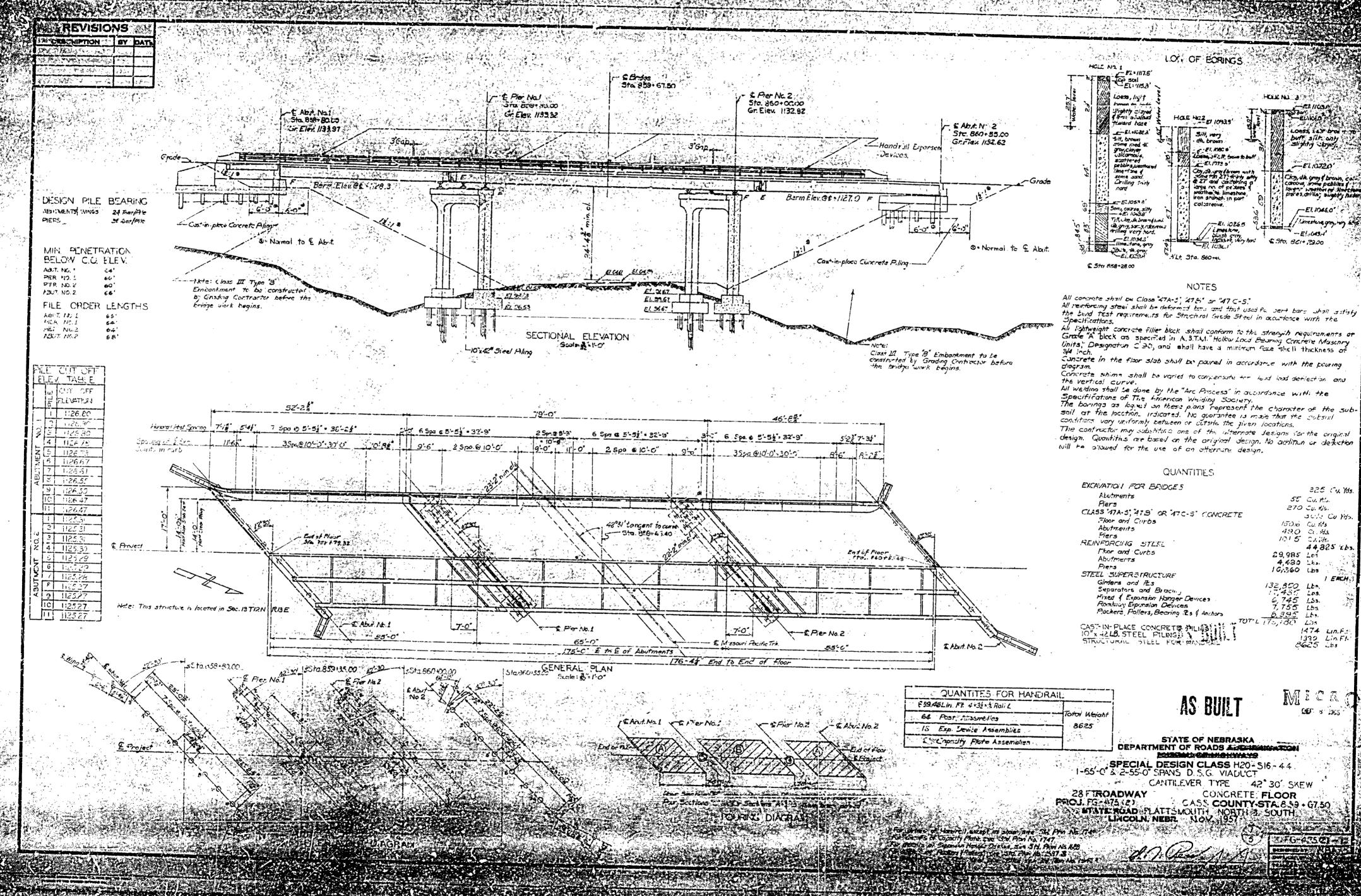
Swam Merchin morning weeks allen R. Eles

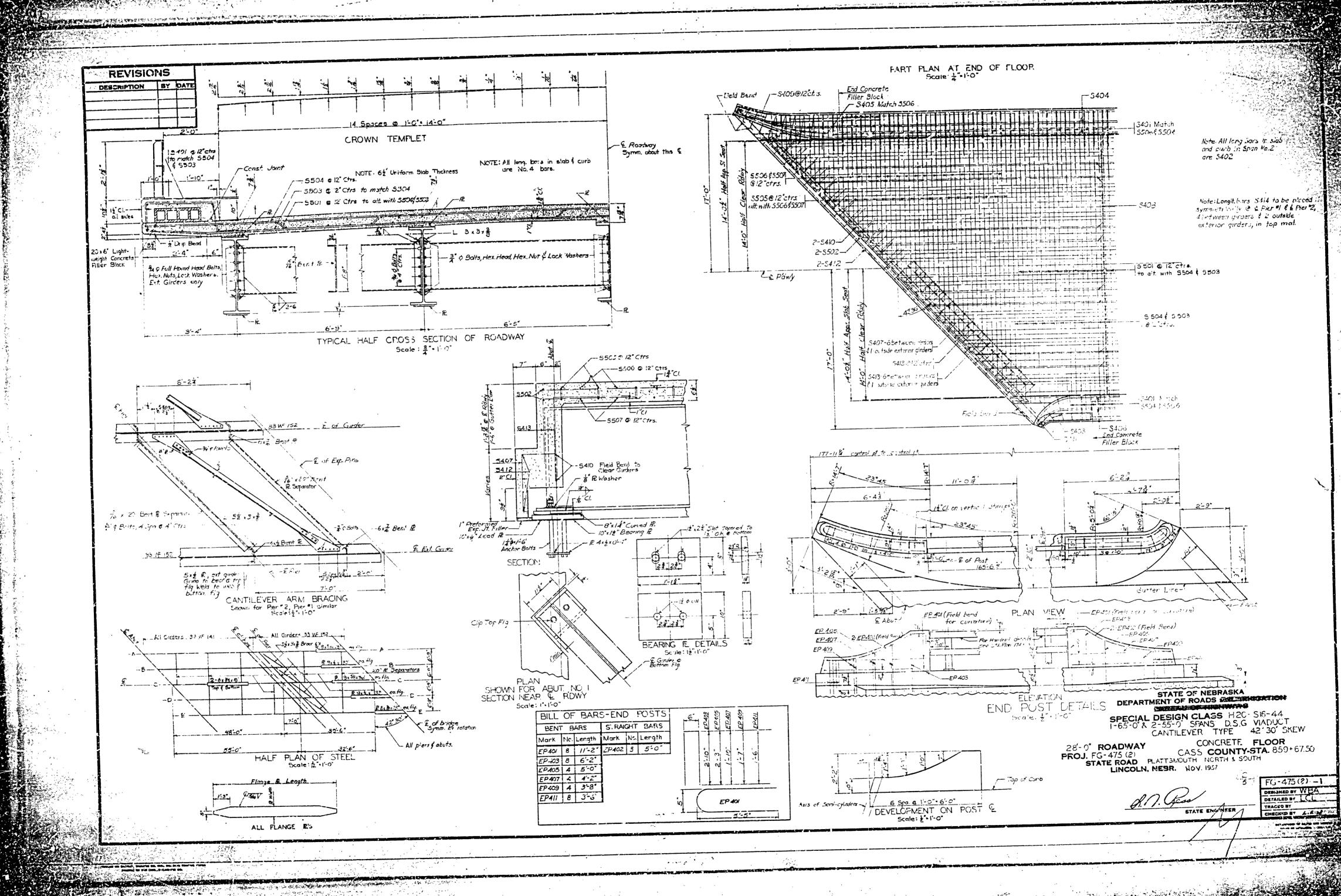


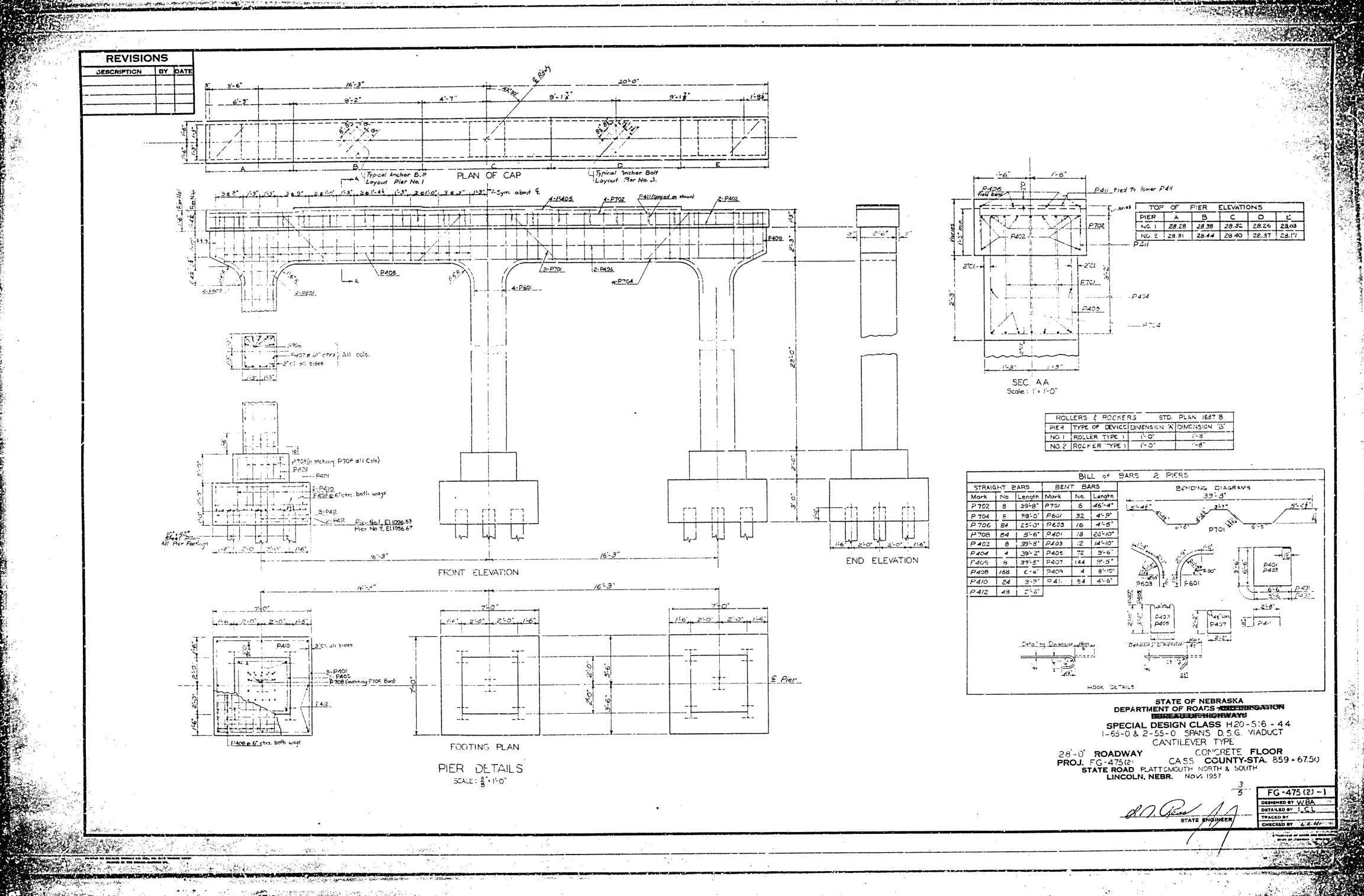
allen K. Evers

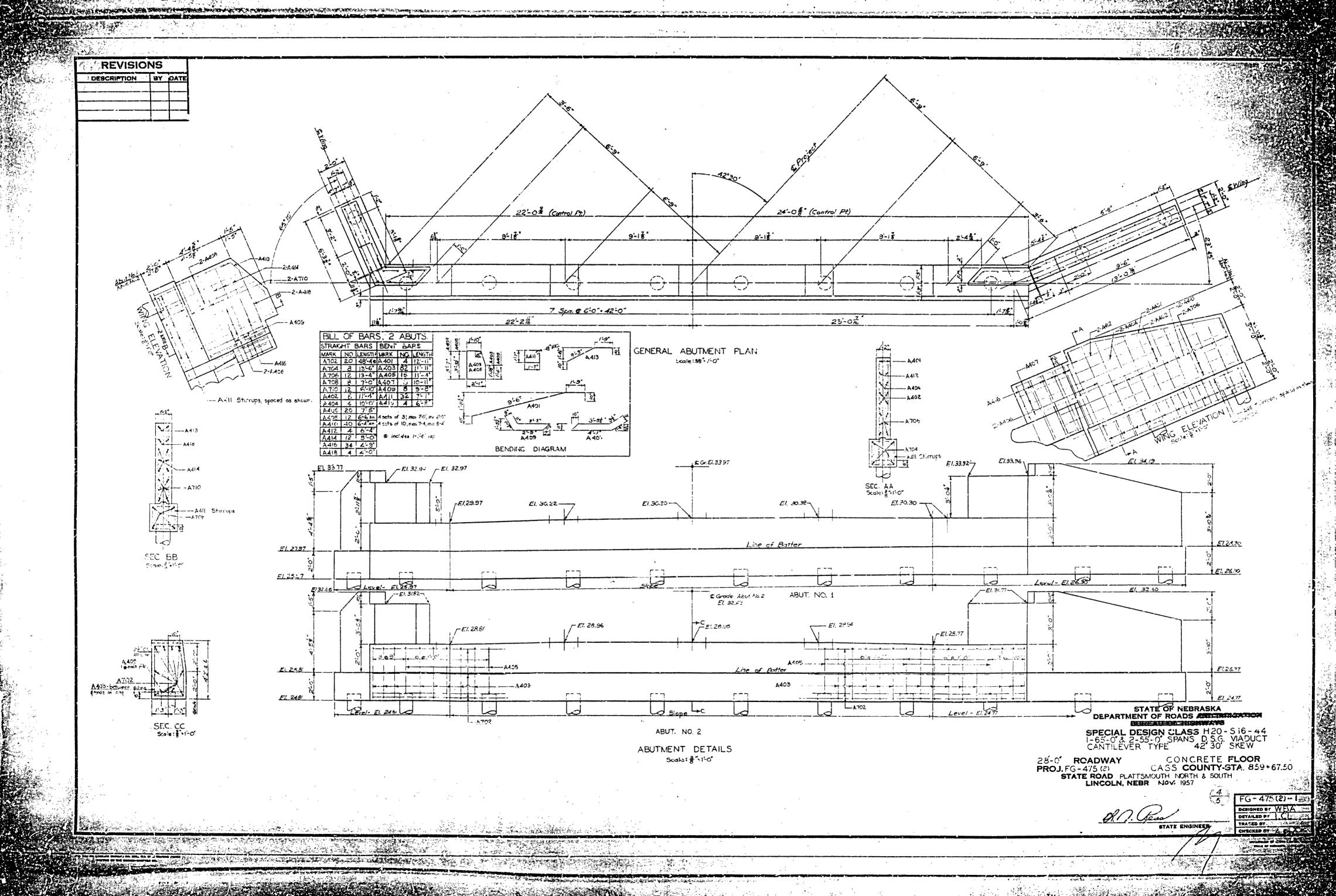


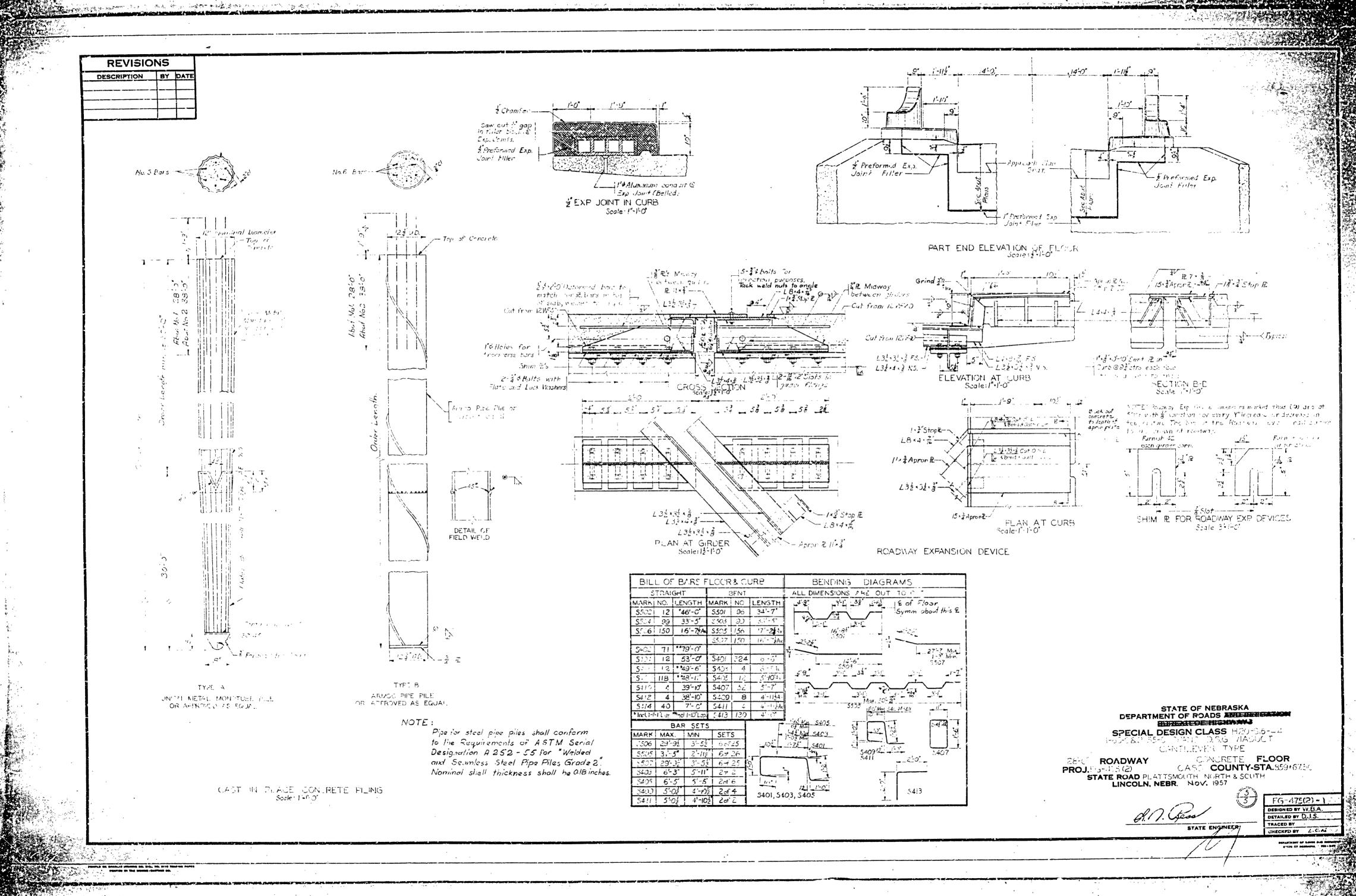
TA .











- INDEX -

DIVISION

DECK STEEL GIRDER BRIDGE (REHAB)
NOTES, QUANTITIES, & INDEX

NOTES, DATE JUNE 2009

NT OF ROADS - BRIDGE DIVISION

- DEPARTMENT

NEBRASKA

AS BUILT

JUL 1 4 201

SPECIAL PLAN NO.

- LEWELLEN SOUTHEAST

## - NOTES -

The existing structure was built under project 249-C(3)-1, dated 1939, and was widened under project 26(119.26) & 26 (119.54), dated 1973. Plans are available from the Bridge Division upon request.

The contractor may substitute any one of the alternate designs shown on the plans for the original design. All quantities are based on the original design and no additions or deductions will be allowed for the use of an alternate design.

All sructural steel for Superstructure shall conform to the regulrements of ASTM A709/A709M, Grade 36.

Field tack welding of form hangers or miscellaneous hardware to any part of the

Concrete for slab, approach slabs and rails shall be class "47BD", with a minimum 28-day strength of 4000 Psi.

All other cast-in-place concrete shall be Class "47B" concrete with a 28-day strength of 3,000 psi.

All reinforcing steel shall be epoxy coated and conform to the requirements of

The minimum clearance, measured from the face of the concrete to the surface of any reinforcing bar, shall be 3", except where otherwise noted.

All existing concrete coming in contact with the new work shall be thoroughly cleaned and roughened before placing new concrete. All reinforcing steel encountered in breaking back existing concrete shall be

thoroughly cleaned, straightened and extended into the new work a minimum of 24 in.

All dimensions shown are in horizontal plane only. No allowances have been made for vertical curve or roadway cross slope.

The girders for this bridge are not designed to resist any torsional or lateral forces due to temporary construction loads. The Contractor must provide any temporary bracing necessary to support the girder web and flanges against all torsional or lateral forces resulting from construction loads.

Before ordering any materials, the contractor shall make a detailed field inspection of the project site, verifying all dimensions and reporting to the Engineer any discrepancies between his measurements and those shown on the plans.

All materials removed shall become the property of the contractor and shall be removed

All preparations, materials, equipment, tools, labor and incidentals necessary to complete the work that are not paid for directly, shall be considered as subsidary to items for which

All concrete surfaces to be in contact with the new work shall be thoroughly cleaned before placing any new concrete.

Contractor will determine the locations of all Class II Repair, with the approval of the Engineer.

The contractor shall place a 1" deep saw cut at the limits of pavement removal to facilitate a clean, smooth line when breaking back existing concrete.

When breaking existing concrete, the use of a maximum 15 lb. hammer applied at a 45° angle is required.

## - QUANTITIES -- GROUP 6 -

PIN REPLACEMENT \_

- OROUR	0 -							
ABUTMENT NO. 1 EXCAVATION ABUTMENT NO. 2 EXCAVATION		LUMP SUN		NOTES. QUANTITIES. & INDEX				
PREPARATION OF BRIDGE AT STA 694+45.86 ABUTMENT REPAIR		I EACH <del>-30 SQ: FT:-</del>		CONSTRUCTION PHASING 3				
CLASS 47BD-4000 CONCRETE FOR BRIDGES SLAB HAUNCH CONCRETE RAIL	43.0 CU. YDS. .70 CU. YDS. 84.8 CU. YDS.	128.5 CU. YDS.		GRADE BEAM PLAN & ELEVATION				
CLASS 47B-3000 CONCRETE FOR BRIDGE ABUTMENTS		52.2 CU. YDS.		SLAB REINFORCING				
EPOXY COATED REINFORCING STEEL SLAB CONCRETE RAILS ABUTMENTS	6,350 LBS. 16,795 LBS. 13,365 LBS.	36,510 LBS.		56'-0" RAIL ON BRIDGE				
CONCRETE FOR PAVEMENT APPROACHES CLASS 47BD-4000 SLAB CONCRETE RAILS	<del>-181.9 - CU. YDS.</del>		194.0 CU. YDS.	SLAB BILL OF BARS				
EPOXY COATED REINFORCING STEEL FOR PAVEMENT APPROACHES SLAB CONCRETE RAILS	30,235 LBS. 4,295 LBS.	34,530 LBS.		APPROACH SLAB BILL OF BARS				
GRANULAR BACKFILLSTRUCTURE				CLASS II AND III REPAIR LOCATION AND SIZE LOCATED IN FALCON PROJECT\61440\DISTRICT\AS BUILT\BRIDGE\ A26-2(1023) lewellen se patch.				
PRECOMPRESSED POLYURETHANE FOAM JECLASS 4, COLD MILLLING								
CLASS I REPAIR		1915 SQ. YDS.	20.000.00 100					
CLASS III REPAIR			28.986 SQ. YDS. 0.600 SQ. YDS.	ELEVATION NORTHWEST ALUMINUM CAP IN BRIDGE RAIL 3305.044 ELEVATION SOUTHEAST ALUMINUM CAP IN BRIDGE RAIL 3305.049				
PLACING, FINISHING, AND CURING CONCRETE OVERLAY - SF CONCRETE FOR OVERLAY - SF			185.432 CU. YDS					
	<del></del>							

I EACH

The location of all aerial and underground utility facilities may not be indicated in these plans. Underground utilities, whether indicated or not will be located and flagged at the request of the contractor.

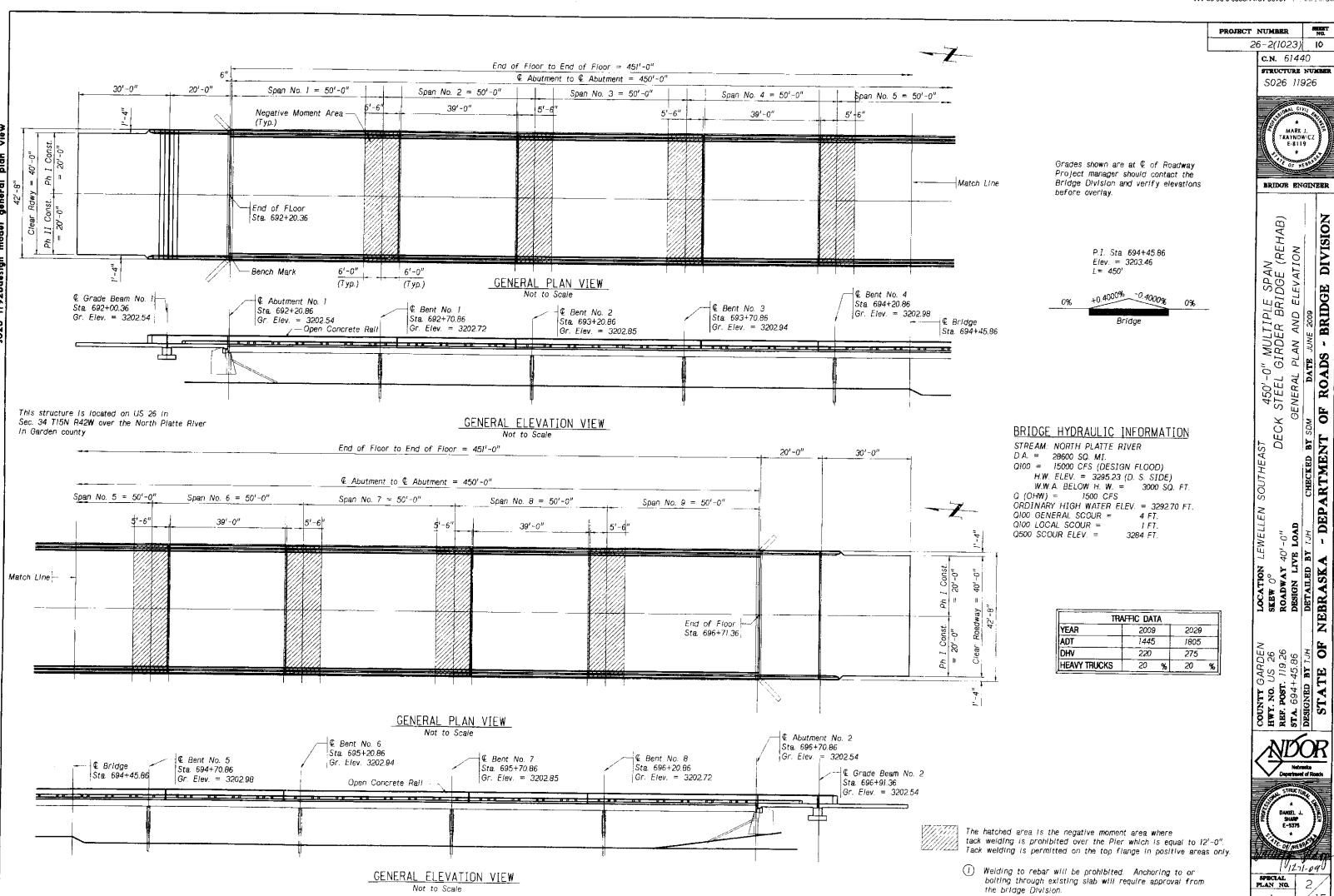
No excavation will be permitted in the area of underground utility facilities until all such facilities have been located and idetified to the satisfaction of all parties. The excavtion must be accomplished with extreme care in order to avoid any possibility of damage to the utility facility.

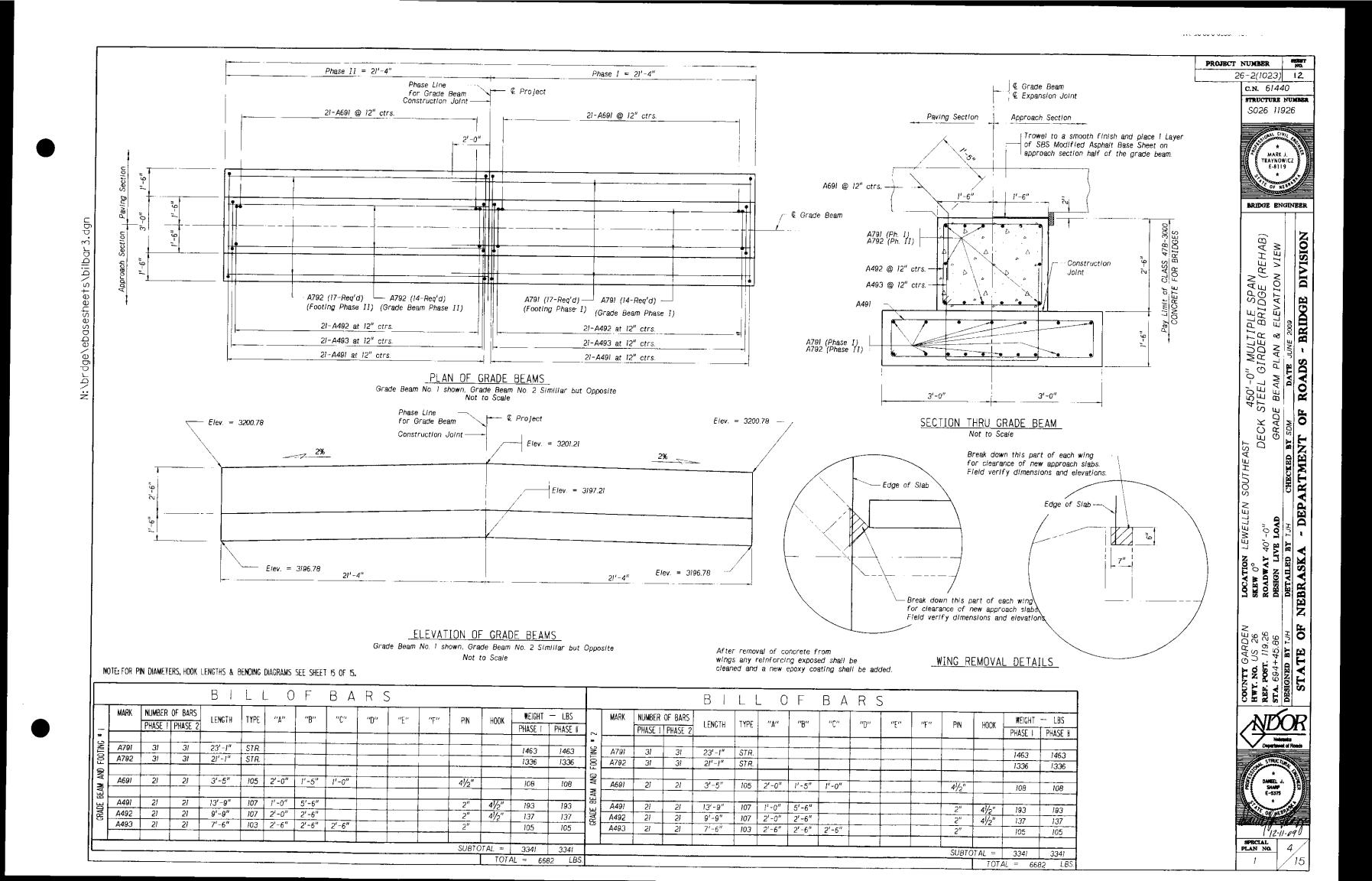
NO.

10

DIVISION

Q.





- End of Paving Section

¢ Grade Beam — -

├--- € Abutment

3'-6"-

<u>L2</u> = 13'-5"

PLAN OF GRANULAR BACKFILL

MO. PROJECT NUMBER 26-2(1023) 13

> C.N. 61440 STRUCTURE NUMBER S026 11926



BRIDGE ENGINEER

DIVISION

ROADS

P

450'-0" MULTIPLE SPAN
STEEL GIRDER BRIDGE (REHAB)
LAR BACKFILL & PIN REPLACEMENT
DATE JUNE 2009

RRIDGE

GRANULAR DECK DEPARTMENT

LEWELLEN LOCATION LEWELLE SKBW 0°
ROADWAY 40'-0"
DESIGN LIVE LOAD
DETAILED BY 13H

NEBRASKA - DE

SOUTHEAST

COUNTY GARDEN
HWY. NO. US 26
REF. POST. 119.26
STA. 694+45.86
DESIGNED BY 7JH
STATE OF

14271-090 SPECIAL PLAN NO.

5,

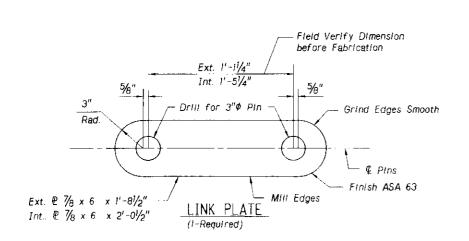
20'-0" - End of Paving Back face of Abutment --⊢-- ⊈ Grade Beam -- End of Floor Sect/on Area . \* Granular Backfill - Area 2 Compact fill according to the (At & of Clear 3'-6" 1'-1" Standard Specifications for Roadway) Highway Construction.

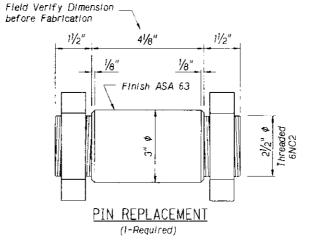
The pay limit quantity for Granular Backfill, per Abutment, has been established using the following equation: Quantity  $(yd^3) = Area \times [Ll + (2 \times L2)] + Area \times (Roadway Width)$ 

- \* The Granular Backfill in this area shall be placed in 8 inch layers and compacted by a single pass of a walk-behind, lightweight (approx. 100 ibs.) mechanical tamper, roller, or vibratory compactor. There is no density requirement. Heavy compaction equipment shall not be used in this area. Flooding the granular backfill with water is not allowed.
- \*\* The Backfill in this area shall be compacted in accordance with the Standard Specifications.

SECTION A-A

GENERAL PLAN Not to Scale





Notes. Pin shall be ASTM A-108 or ASTM A688 Class D or Approved Equal. Recessed nut shall be either pressed or cast steel. Structural steel for Link Plates shall be ASTM A36. For the purpose of impact test, all Link Plates shall be considered main tention members.

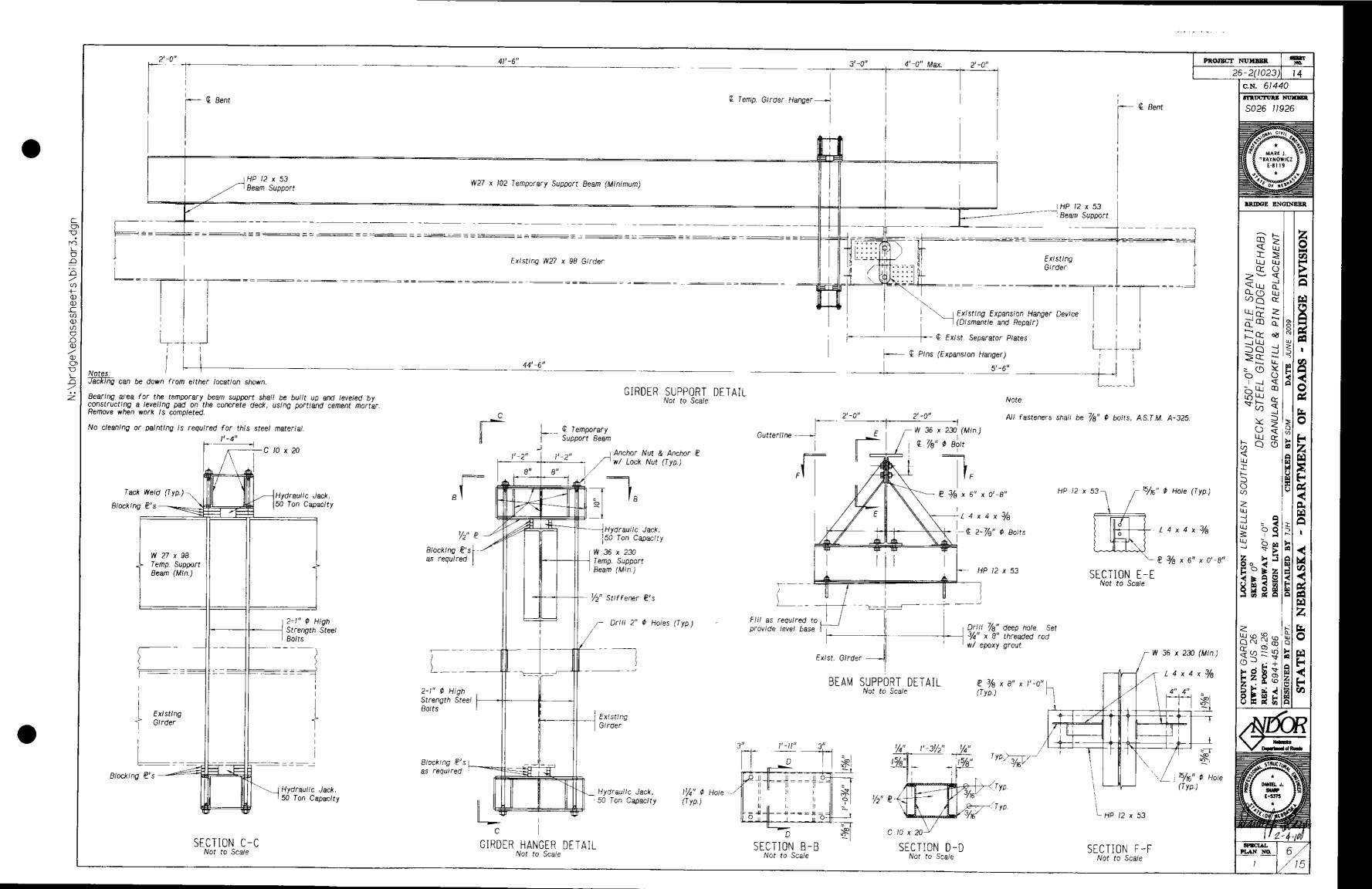
- NOTES -

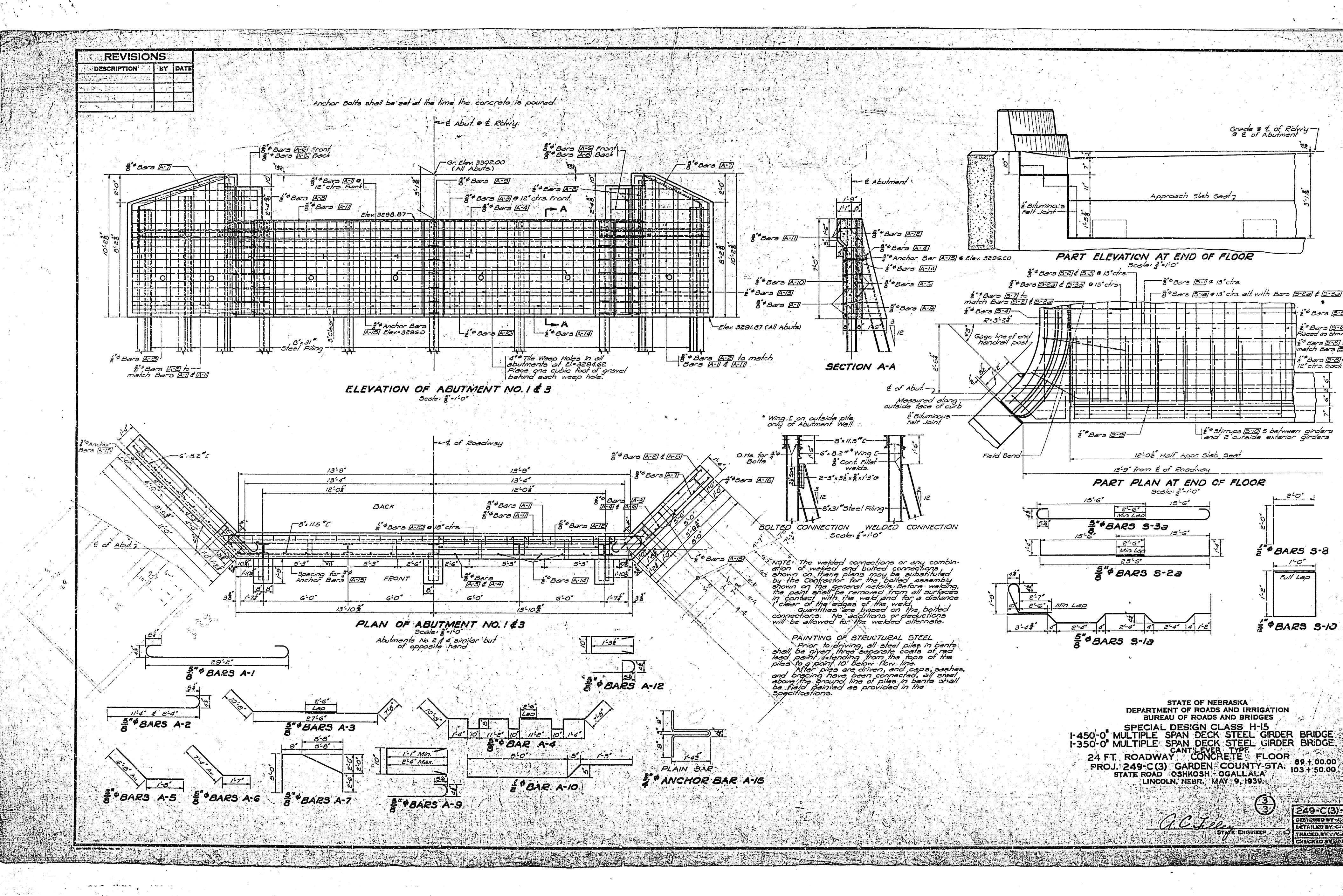
"PIN REPLACEMENT". This work shall consist of supporting the suspended girders at the expansion joint, removing the existing link plates and pins, and installing the new link plates and pins.

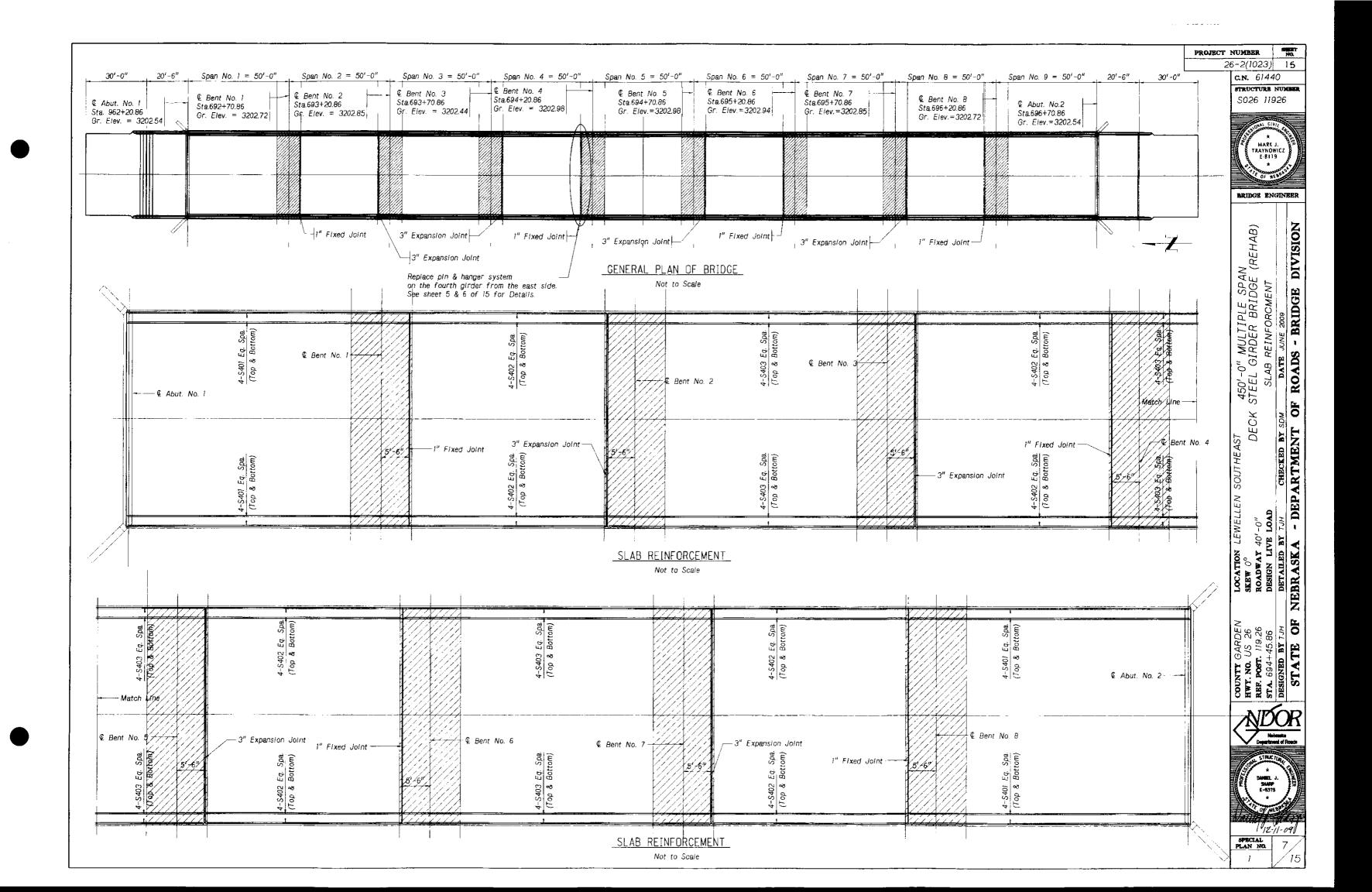
Prior to beginning any field work, a step-by-step procedure for supporting the girders and replacing the link plates and pins shall be submitted by the Contractor for the Engineer's approval. A possible method of supporting the girders is shown in the plans. The Contractor is not required to use this method of support; it is only shown as a possible method. The furnishing and installing of jacks, temporary scaffolding, blocks or other material shall be a part of this item. Any damage to the structure due to negligence by the Contractor shall be repaired by the Contractor at no expense to the State. Approval of any procedure submitted by the Contractor shall not release him of any responsibility.

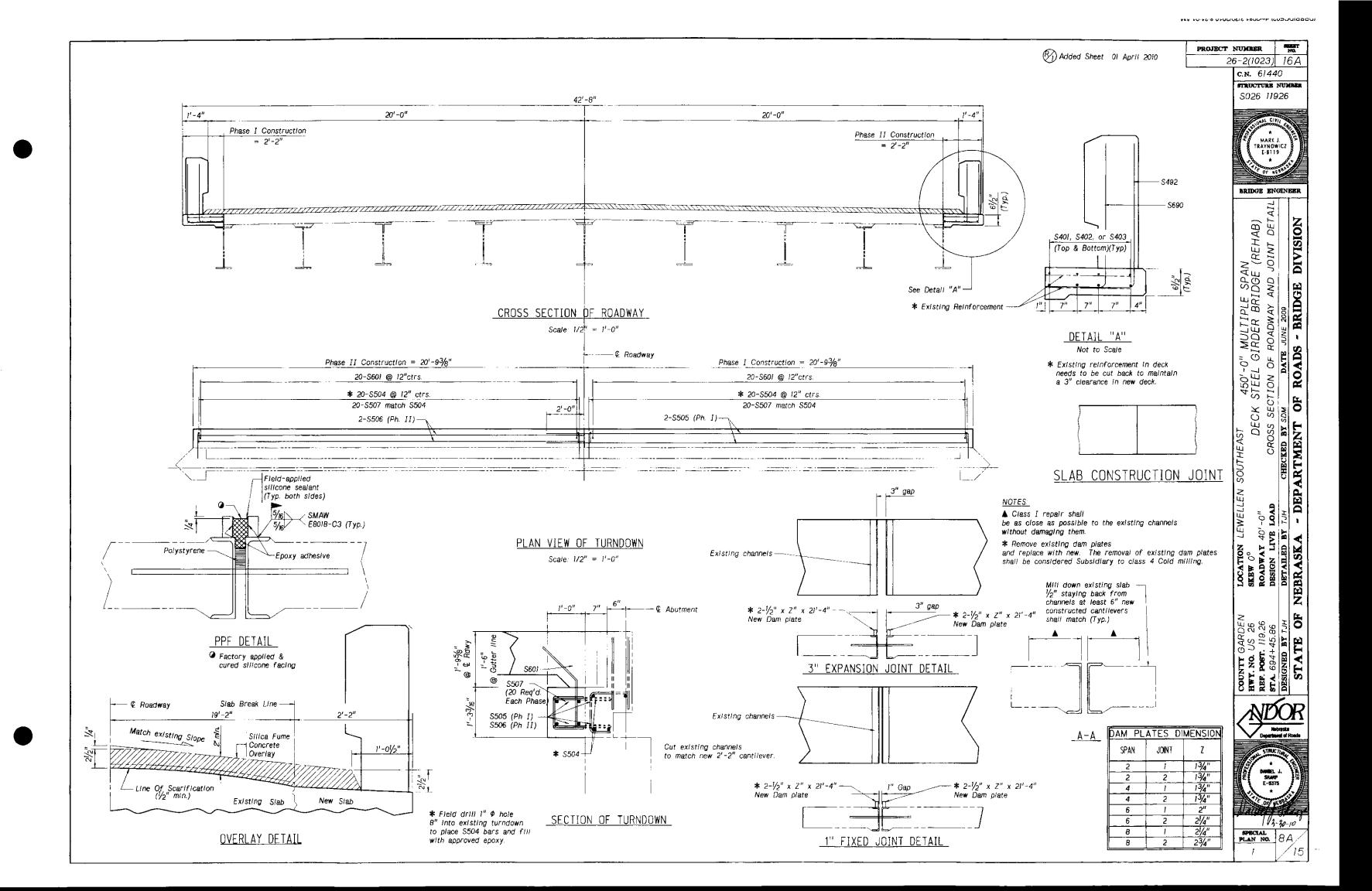
The Item "Pin Replacement" shall be measured for payment as a single unit for each set of link plates and pins replaced and accepted by the Engineer.

Payment for this work, measured as provided herein, shall be made at the contract unit price per each (EA) for the Item "Pin Replacement". This price shall be full compensation for all labor, equipment, tools, materials and any Incidentals necessary to complete the work.







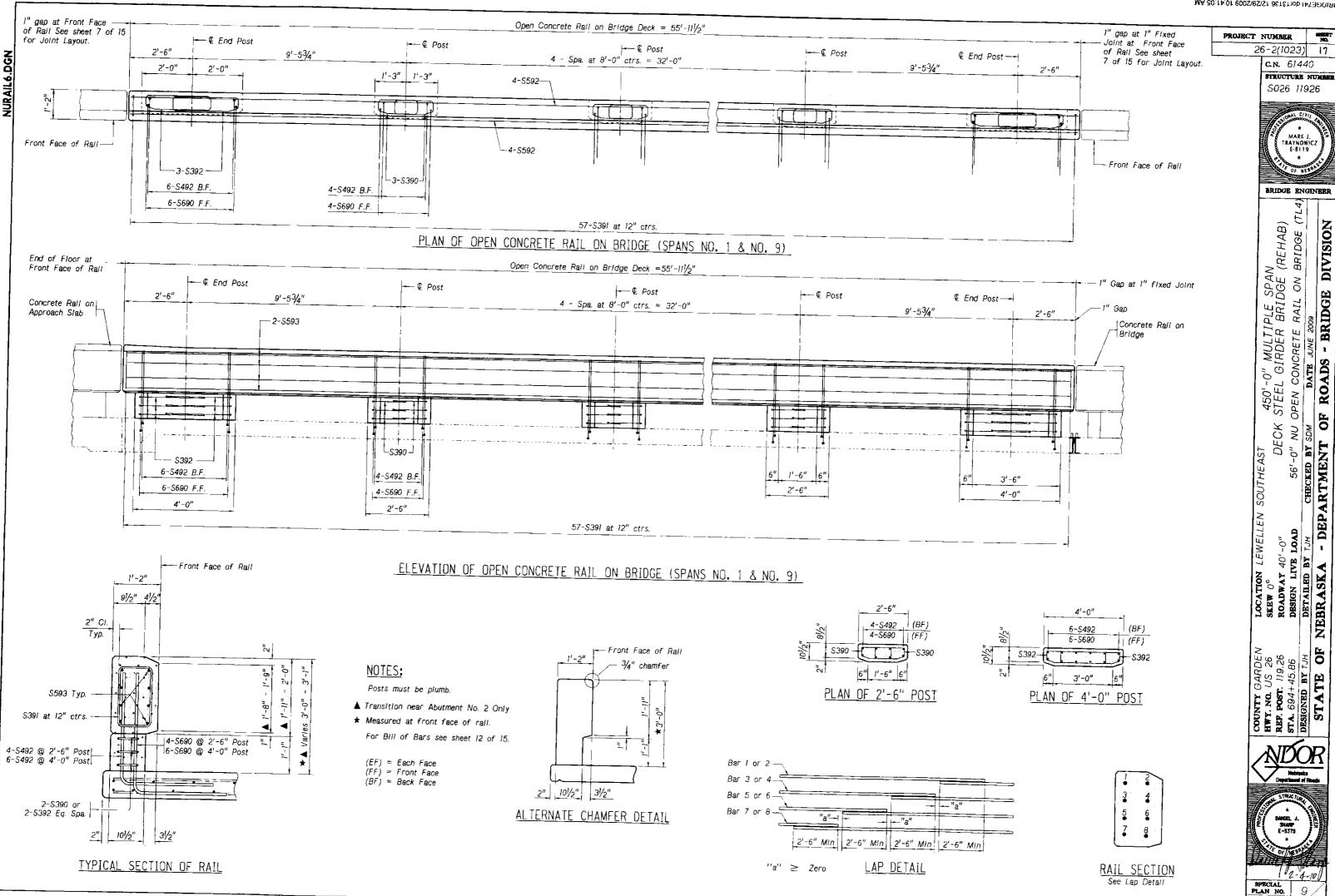


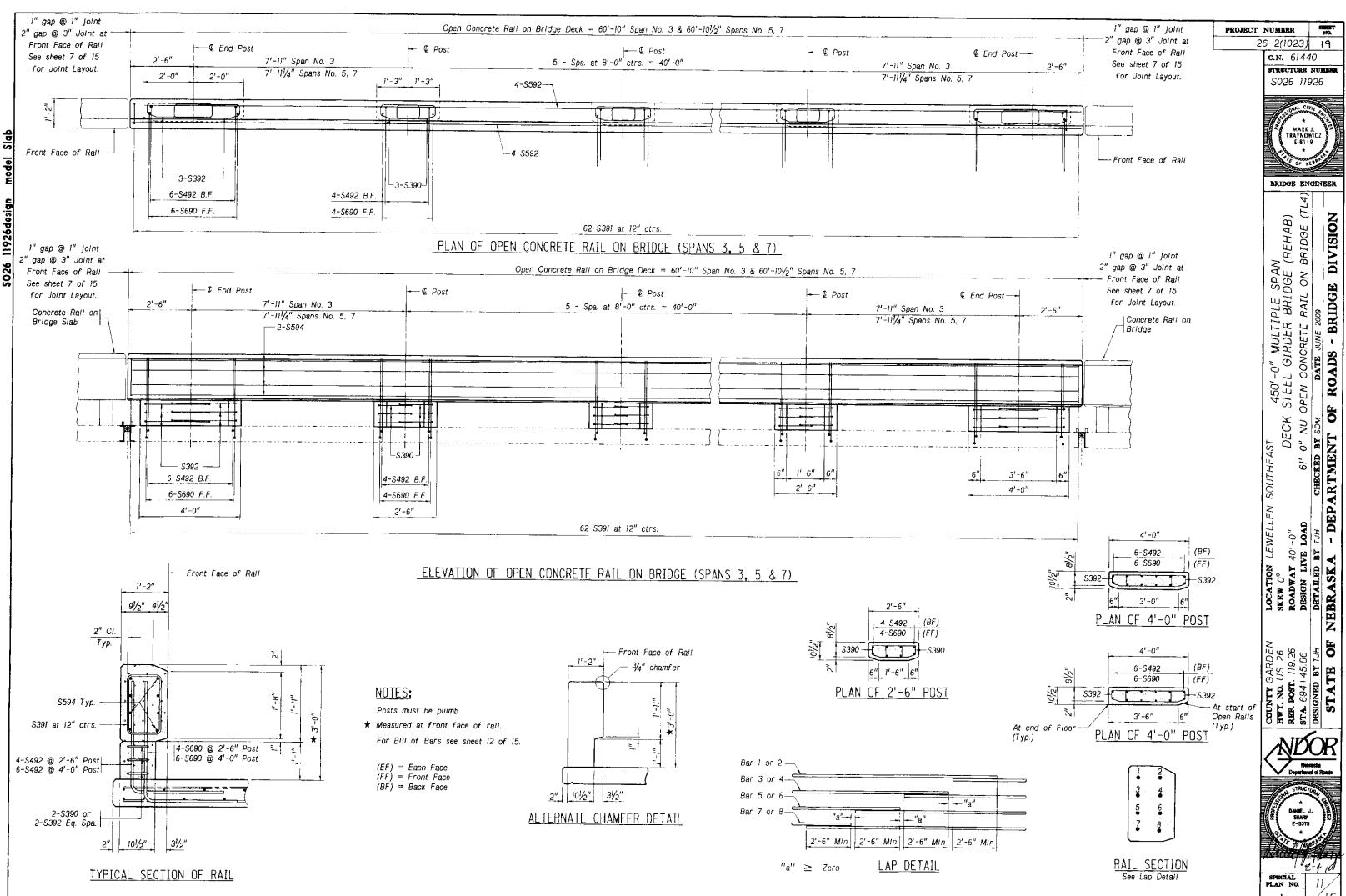
NO.

17

DIVISION

P. P.





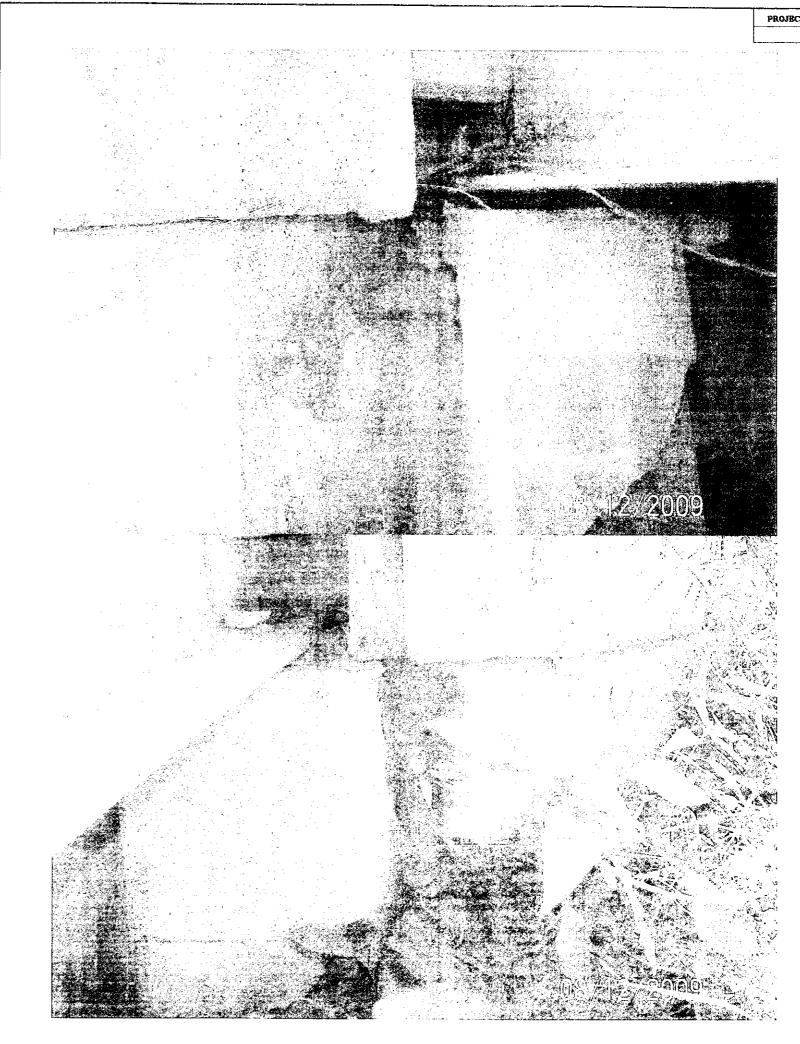
BARS BILLOF NUMBER OF BARS WEIGHT - LBS "E" "C" "D" HOOK PHASE I PHASE PHASE I PHASE II S601 40 40 3'-0" 105 1'-6" 180 180 S504 80 118 118 STR. S505 8 22'-6" 188 188 S506 20'-6" STR. 171 171 \$507 40 103 90 90 S40I 57'-4" Includes 1 - 2'-0" Lap Splice. 613 16 613 32 32 38'-3" STR. 818 818 S403 24 24 62'-3" Includes 1 - 2'-0" Lap Splice. 998 998 SUBTOTAL = 3176 3176 S690 104 1'-11" 3'-2" 64 64 5'-1" 41/2" 489 489 Include 1 - 2'-6" Lap Splice. 971 971 S492 64 64 5'-0" 104 1'-11" 214 214 6½" 10" S390 60 60 130 | 1'-11/2" 105 105 S391 114 114 5'-2" 107 1'-5" 4" 221 221 130 1'-71/2" 53**9**2 24 69 SUBTOTAL = 2069 2069 S690 96 5'-1" | 104 | 1'-11" 3'-2" 41/2" 733 733 Include 1 - 2'-6" Lap Splice. 1285 1285 \$492 104 1'-11" 321 321 S390 72 4'-8" 130 1'-11/2" 72 1'-6" 126 126 S391 160 160 5'-2" 107 1'-5" 4" 311 311 48 130 1'-71/2" S392 48 7'-8" 138 138 SUBTOTAL = 2914 2914 3'-2" S690 108 108 5'-1" 104 41/2" 825 825 24 Include 1 - 2'-6" Lap Splice. \$594 62'-11" 1575 1575 \$492 108 361 361 \$390 130 1'-11/2" 61/2" 108 108 4'-8" 190 190 S391 186 186 107 10" 361 361 130 1'-71/2" 61/2" 3'-0" 36 7'-8" 104 104 \$392 SUBTOTAL = 3415 3415

NOTE: FOR PIN DIAMETERS, HOOK LENGTHS & BENDING DIAGRAMS SEE SHEET IS OF IS.

Example shown for Abutment repair. (See pictures) Pictures were taken at the North Abutment

All damaged concrete at abutments should be removed to sound concrete and then patch in with new concrete. Pay Item for this repair Is listed under "Abutment Repair" Contact Bridge Division with any questions.

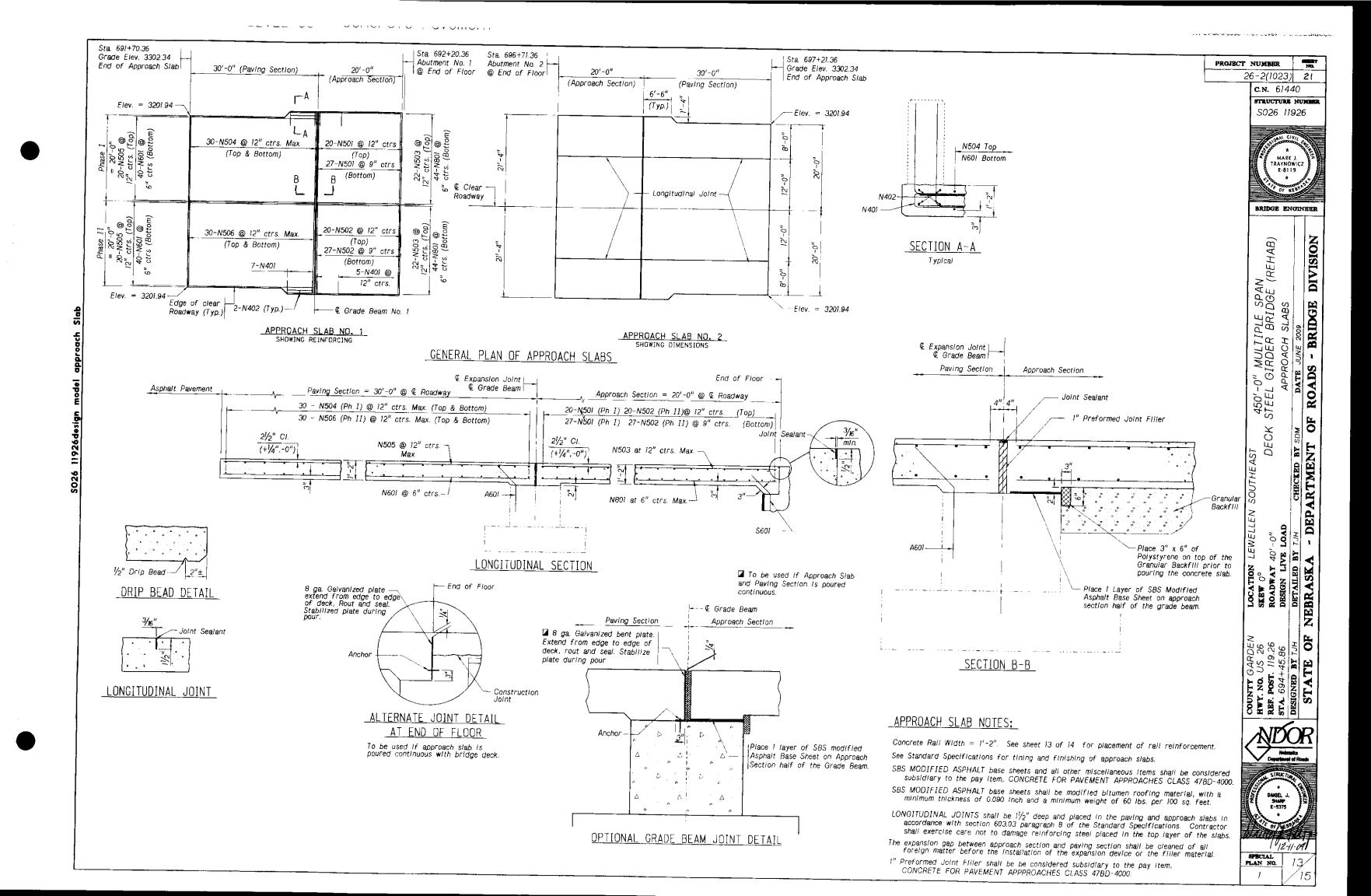
TOTAL = 23148 LBS.

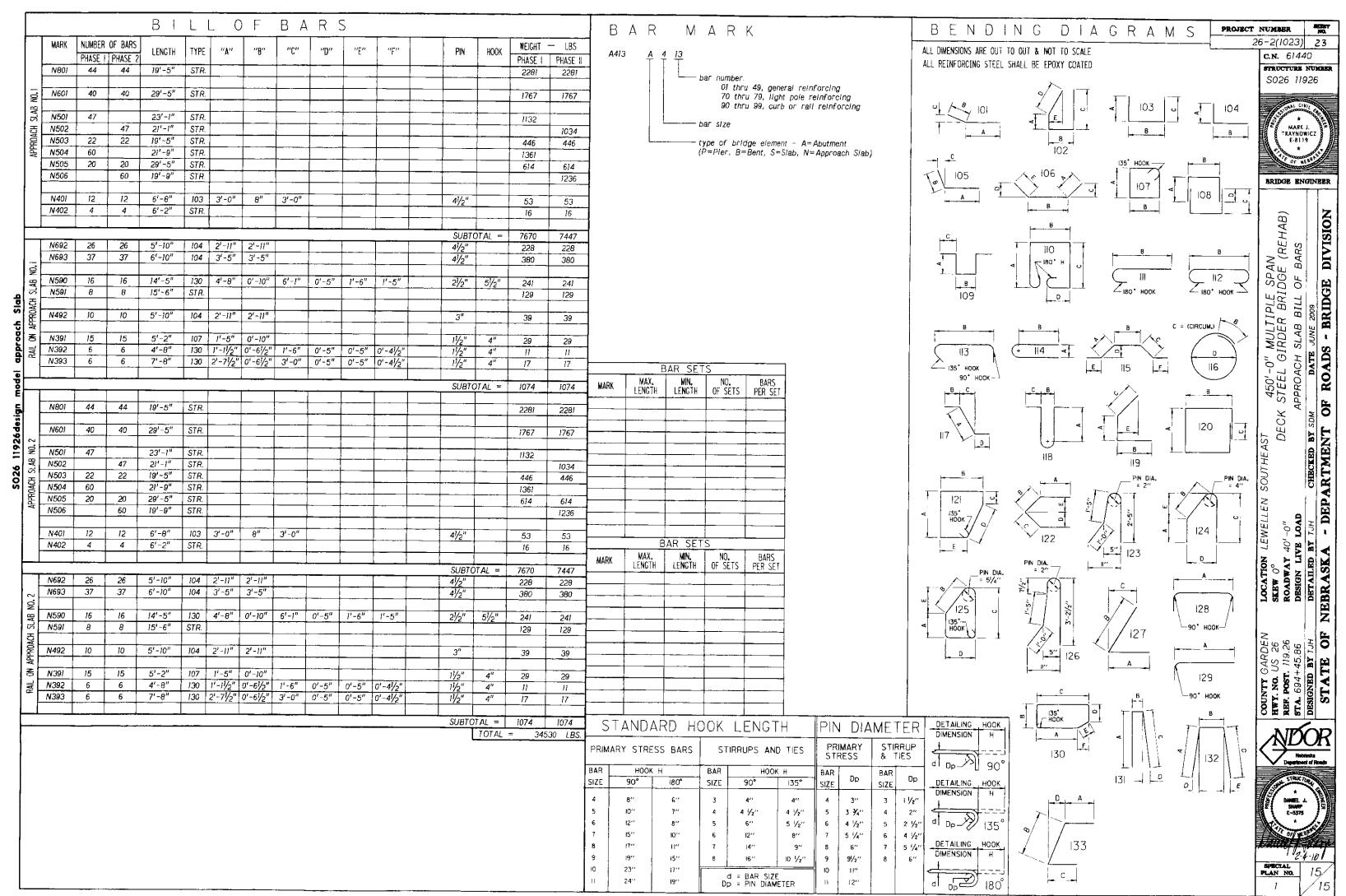


PROJECT NUMBER 26-2(1023) C.N. 61440 STRUCTURE NUMBER S026 11926 DIVISION 450'-0" MULTIPLE SPAN STEEL GIRDER BRIDGE (REHAB) SLAB AND RAIL BILL OF BARS ROADS Ö DECK DEPARTMENT NEBRASKA

ELL SU SE ES DUUGIOUGOE DA.

SPECIAL PLAN NO.





CERTIFICATE OF AUTHENTICITY

This is to certify that the microphotographs appearing on this film are true and accurate reproductions of the original records produced in the regular course of business.

It is further certified that records on this film are microfilmed in conformity with the Rules and Regulations of the State Records Administrator and the Statutes governing them, and that the microphotographic processes accurately reproduce the records and that the film forms a durable medium for reproducing the original, if necessary.

Microfilm Operator

Microfilm Operator

Reproduction Supervisor

FED. ROAD STATE FED. AID £ Abutment No. 2 REG. NO. NEBR. PROJECT NO. + 86nt No. 6 Sta 89+75,00 Sta. 91+2500 A FART AT . 22 (110.26). Sta 89+2500 \*- Sta 88+75.00 Gr. Elev. 3302.00 1 Gr. Elev. 3302.40 Gr. Elev. 330231 - \$ Pridge Stu 89+0000 NOTES Before ordering any material the contractor shall make a detailed field inspection of the existing structures and report any discrepancies, between his ,-Elev 3291.87 measurements and those shown on the extra area to the High Noto: = 2,577 eg # 1 FL LEV 32874-28 37 87 g CONTRACTOR OF THE CONTRACTOR OF THE TOTAL STREET OF THE CONTRACTOR This structure is designed in accordance with the 10th edition of the AASHO "Standard Specifications" —Profile of Natural Ground for Highway Bridges. GENERAL ELEVATION (BRIDGE NO.1) All concrete shall be Class 47E' with a working stress of 1,260 p.si. Scale: [\*=20'-0" - £ Abutment No. 2 1--- & Berit No. 6 or 1 € Bent No 3 H→ E Ecrit No. 4 ----- Appringer in a series Bont No 1 ---- Bent lo Z All exposed edges of concrete small be charafored. —Face of Rail∗ All existing concrete commo in contact with ricw concrete shall be roughered and cleared pirion to placing the new concrete." - Capacity Plate The minimum clearance measured from the face -Rodala i Expansion kaka 🚘 of the concrete to the surface of any reinforcing bar. – £ Roadway, Symm shall be 2 inches, except as snown. All renforcing steel shall conform to the requirments of A.S.T.M., Designation A615 or A617, Grade 40, except that Grade 60 may be substituted for Grade 40. -Easting steel airders The working stress for reinforcing steel is 20000 psi and sübstructure All reinforcina steel encountered in breaking back The existing structure shall be cleaned, straightened and usea in placa. extended a minimum, of 2 feet into the new concrete.
The item "Preparation of existing structures of Span No 2=50'-0" Span No 2=50'-0" Scan No 3=50'-0" Span No 4=50'-0" Span No 9=50'-0" Span No 9=50'-0" Sta. 89+00.0 and Sta. 163+50.0 shall be in accordance with £ to £ Abutments = 450'-0" The furnishing and placing of Capacity Plates. End to End of Floor=451-0" drain tiles and Elastomenió Compression Seals shall nót be pala for directly, but shall be considered subsidiary to other literas GENERAL PLANTBRIDGE HOLD Bridge Deck shall be finished with a mechanical Petrove existing concrete deck from both bridges and Lulo " unitarm state in all codes." 12 Abutment No. 4 SE Atolomer No 3 - , Cr. Lie, 330211 - Greatiev BBUKBI . Gr. Liev 330234 ୍ୟ Por Gatal ଗୁରୀ କରାଦୀର eso enom É di S \$1a. 103 15400 FIF EVEN CONTRACTOR OF THE PROPERTY OF THE PRO ,—Elev. 3291.87 --Profile of Natural Ground GENERAL ELEVATION (BRIDGE 110.2) —Existing steel operates and Thicke structures als recatous Scale: 1"=20"0" - deress tre North Patte Puer n Sell 34: Tiell: P401 n Garaen County - gybstríystyne fysed in filoga. - F Bent No 11 - E Bent No. 12 - E Bent No 13 -- £ Abutment No 3 -- £ Bent No 9 -- F Roct No. 10 Structural Steel for Superstructure 372.85 20.3625 163.60 Pounds 35920 20.480 15440 Pounds 14.80 16.80 Ft. HP8 x 36 Steel Piling 7.760 7520 20.00 Lin. Ft. HP10 x 42 Steel Piling 7.60 16.00 1.200 Lin. Ft. Structural Steel for Bridge Rail 7.6025 42.560 33.65 Pounds Linseed Oil Projective Cooting 7.600 1.600 皇二 | Prochamo (Exconsion Defice | 一貫 End of Floor Sta. 105+25,50 - Paggara - Programa (1925 - 1946) Pointing Existing Structure at Sta 105+50.00\_\_\_\_\_ EXISTING STRUCTURES PROJ. 249-C(3)-1\_\_\_\_\_\_\_\_DATE: MAY 1939 REVISIONS TRAFFIC DATA YEAR ADT DHV 1970 855 110 1990 1450 185 Span No 10-50'-0" | Span No 11-50'-0" | Span No 13-50'-0" | Span No 13-50'-0" | Span No 15-50' 0" | Span No 16-50'-0" £ to £ Abutments = 350'-0" End to End of Floor = 351'-0" GENERAL PLAN (BRIDGE NO.2) LE Abut | LE Bent | LE Ben Scale: 1"=20'-0" STRUCTURAL STEEL FOR BRIDGE RAIL STATE OF NEBRASKA P = Positive . Moment Section DEPARTMENT OF ROADS -- BRIDGE DIVISION - 898.0 Lin. Ft. of Brom 1/6×20 N=Negative Moment Section 9 904.0 Lin Ft. of Standard Guard Rail (10 Gage) MULTIPLE SPANS DECK STEEL GIRDER 153 Splice Plates 6'x1/2" x 1'-0/6" ORIGINAL POURING SEQUENCE TOTAL WEIGHT 42,560 LBS. 158 5/4" o Erid Welded Studs BRIDGE WIDENING-CANTILEVER TYPE Section "B" shall be poured after adjacent "A" sections have been poured. Section "B" may be poured continuous with either section "A", providing the other adjacent section "A" has been poured. POJETE 116 Rail Post Assemblies O' SKEW STATE ROAD OSHKOSH-OGALLALA Rail Expansion Joint Assemblizs H20-44 **DESIGN HWY. NO.** US 26 698.5 Lin Ft. of Bearn WGxCO REF. POST 119.26 AND 119.54 40 FT. ROADWAY 702.0 Lin. Ft. of Standard Guard Rall (10Gaga) **STA.** 89+0000 COUNTY GARDEN ALTERNATE POURING SEQUENCE 124 Splice Plates 6"x 1/2" x 1'-01/2" - TOTAL WEIGHT Pour slab in numerical order as shown. Slab may be 124 5/3" & End Welded Studs PLAN NUMBER 33,065 L.S DESIGNED BY C.M. 26-119.26 AND 119.54 placed in 1 to 9 pours or 1 to 7 pours. 90 Rail Post Assemblies DETAILED BY V.W.S. For details of Surface finish for concrete, see Standard Plan No. 1562-C. For details of Capacity Plate, except as shown, see Standard Plan No. 1747-RI. For details of Guardrail Element, see Standard Plan No. 420-F-RII. 6 Rail Expansion Joint Assamblize SHEET NUMBER NUMBER SHEETS Pouring POURING DIAGRAMS Sequence Not to scale STATE OF HEBRASKA 1000 4-71 DEPARTMENT OF ROADS

72"

..*L*l

449

8.

11'

17"

22"

22

34"

AU

DEPARTMENT OF ROADS
REPRODUCTION SECTION

CERTIFICATE OF AUTHENTICITY

This is to certify that the microphotographs appearing on this film are true and accurate reproductions of the original records produced in the regular course of business.

It is further certified that records on this film are microfilmed in conformity with the Rules and Regulations of the State Records Administrator and the Statutes governing them, and that the microphotographic processes accurately reproduce the records and that the film forms a durable medium for reproducing the original, if necessary.

Date 9-10-76

Microfilm Operator

Alder R. Evers

REG. NO. NEBR. PROJECT NO. Sta 101+7500 | Sta 102+2500 | Sta 102+7500 | Sta 103+2500 | Sta 103+2500 | Sta 103+2500 PILE LAYOUT Bed R on Bents 1, 8, 9 and 14 | 15" x 154" x 156" | Ecd R on Bents 2-7, and 10-13 | 15" x 1/4" x 156" | Not to scale DESIGN PILE BEARING PILE DRIVING DATA FROM-1240 PROJECT NO 249-C(3)-1 Bed Rm / 16'x 39' Cover R IO TONS/PILE 28 TONS/PILE AVERAGE \*\*AVERAGE AVERAGE LENGTH IN BEARING FALL OF HAM--Water Liev. 37.89.7 PLACE (FEET) (TONS) NER (FEET) 1 - Elev 32726 ABUTMENT NO. I HP8 x 3 -Varter Elev 32371 , Elev. 3689.6 \* Splice to existing SECTION A-A Jan 27 W. Com Scale: 1-1-0" S. 1881 , the 3.751 C8 x /3.75 -- \ J. Flev 31676 - Elev 32637 , -Elev 32587 . Alex 52576 ,-Llev 3252 w , Elev 37487 ABUTMENT 10 41 HP 6 / 31 -Elev 32476 , -Elev 32481 1940 Pring driver, with growty nammer. Weight = 3100 Lbs 🔭 Indicates Dearing equacity coisulated using current formula. ,-Elex 3243.1 y - Elev 3238.7 11'-1" to & Roodway -Elev. 3233.7 1-Elev. 32326 KS BUILT PILE NO CUT-OFF PELIET ELEVATION BELOW CO. EXTENSION BENT ELEVATION Scale: 3/4"=1'-0" REVISIONS HOLE NO. 2 HOLE NO. I As Built Pile Data DESCRIPTION BENT NO DATE STA, 77+5600 STA, 93+26.00 LOG OF BORINGS

1940 As Built Pile Data (Cont'd.)

1200 | 29.5 | 30.7 | Bent No.1 Total Pile Lowest Hi-est Location
Length Wices Bearing Ering Location
+340 \* 4 22.4 31.1 Abut. BENT NO 2 HP 10 x 42 BENT NO. 3 BENT NO 4 22.4 31.1 No.1 41/4" 23/4 23/4 4/4" BENT NO. 5 29.5 34.8 Bent No.6 29.5 32.7 Bent No.7 30.7 Bent No. 1 BENT NO. 6 29.5 31.2 Bent No.2 AT ABUTMENT BENT NO 7 29.5 39.8 Bent No.8 29.5 29.5 Bent No.3 at the locations indicated. No quarantee 200 STATE OF NEBRASKA - & Girder is made that the subsoil conditions vary +340 +4 13.7 34.5 Abut. 29.5 37.7 Dent No.4 DEPARTMENT OF ROADS -- BRIDGE DIVISION ABUTIMENT NO 2 1,2,4-7,9 & 10 \* 3295.93 3B AND & 5 \* 3297.43 32 35 47 50 HP 8 x 36 100 | 13.7 | 34.5 | No.2 | \*340 \*4 | 12.1 | 27.0 | Abut. -uniformly between or outside the giver? -locations. /-13/8 # O.H. - £ Girder 1/2" Lead R-MULTIPLE SPANS DECK STEEL GIRDER ABUTMENT NO 3 30 1.2.4-7.9 EIC \* 3298.93 35 50 HP 8 × 36 32 47 144 OH -12.1 27.0 No.3 29.5 29.5 Bent No.9 BRIDGE WIDENING-CANTILEVER TYPE CI\_ASSIFICATION OF MATERIALS 3B AND &B + 3297.43 1-13/3 4 9. Bent | \* 3298.94 | 47 BENT NO. 9 1-4 . Fine Sand 28.6 30.7 Bent No.10 STATE ROAD OSHKOSH-OGALLALA O° SKEW Time Solid 2. Coanse Sand 3. Coanse Sand to Fine Sand Gravel 4. Fine Sand to Coanse Sand Gravel 6. Fine to Coanse Sand 7. Sand to Coanse Sand Gravel 8. Fine Sand to Coanse Sand Gravel HP 10 x 42 80.6828 BENT NO 10 1-4 29.5 29.5 Bent No.11 H20-44 **DESIGN HWY. NO.** U.S. 26 50 50 HP10 x42 47 3299.13 BENT NO II 
 200
 29.5
 32.7
 Bent No.12

 200
 29.5
 32.7
 Bent No.13

 200
 29.5
 30.7
 Bent No.14

 \*340
 \*4
 14.7
 25.4
 Abut.
 LE Abutinient 40 FT ROADWAY **REF. POST** 119.26 AND 119.54 47 HP 10 x42 **\*** 3299 I3 BENT NO 12 1 -- 4 **COUNTY** GARDEN 43/4" 23/5 234 43/4" 41/4" 73/4" 23/4 41/4" .50 HP 10 x 42 \* 3299.08 BENT NO. 13 1 - 4 1'-3" 50 HP 10 x 42 BENT NO. 14 \* 3298.94 47 1'-2" 1-4 DESIGNED BY C.M. PLAN NUMBER 26-119.26 AND 119.54 HP 8 x 36 AT BENT 32 AT ABUTMENT ONLY DETAILED BY V.W.S. 147 254 No. 4 100 14.7 25.4 No. 4

Total Pile Lowest Hi-est.
Lath. Splcs. Besting Bring Location BEARING PLATE DETAILS 47 3B AND &B \* 329743 LEAD PLATE DETAIL SHEET NUMBER NUMBER SHEETS \* These elevations are to match the existing cut-off elevations of the appropriate bent and .02' higher than existing cut-off elevations of the appropriate abultment. Scale: 11/2"=1'-0" Scale: 1/2"=1'-0" DATE APRIL, 1973 \* Pile Solices of 15' Adled on to Pile Nos. 4. 5. 6 8 7. PRINTED ON CHARLES BRUNING CO. NO. 40-818 TRACING PAPER

AO

34''

CERTIFICATE OF AUTHENTICITY

This is to certify that the microphotographs appearing on this film are true and accurate reproductions of the original records produced in the regular course of business.

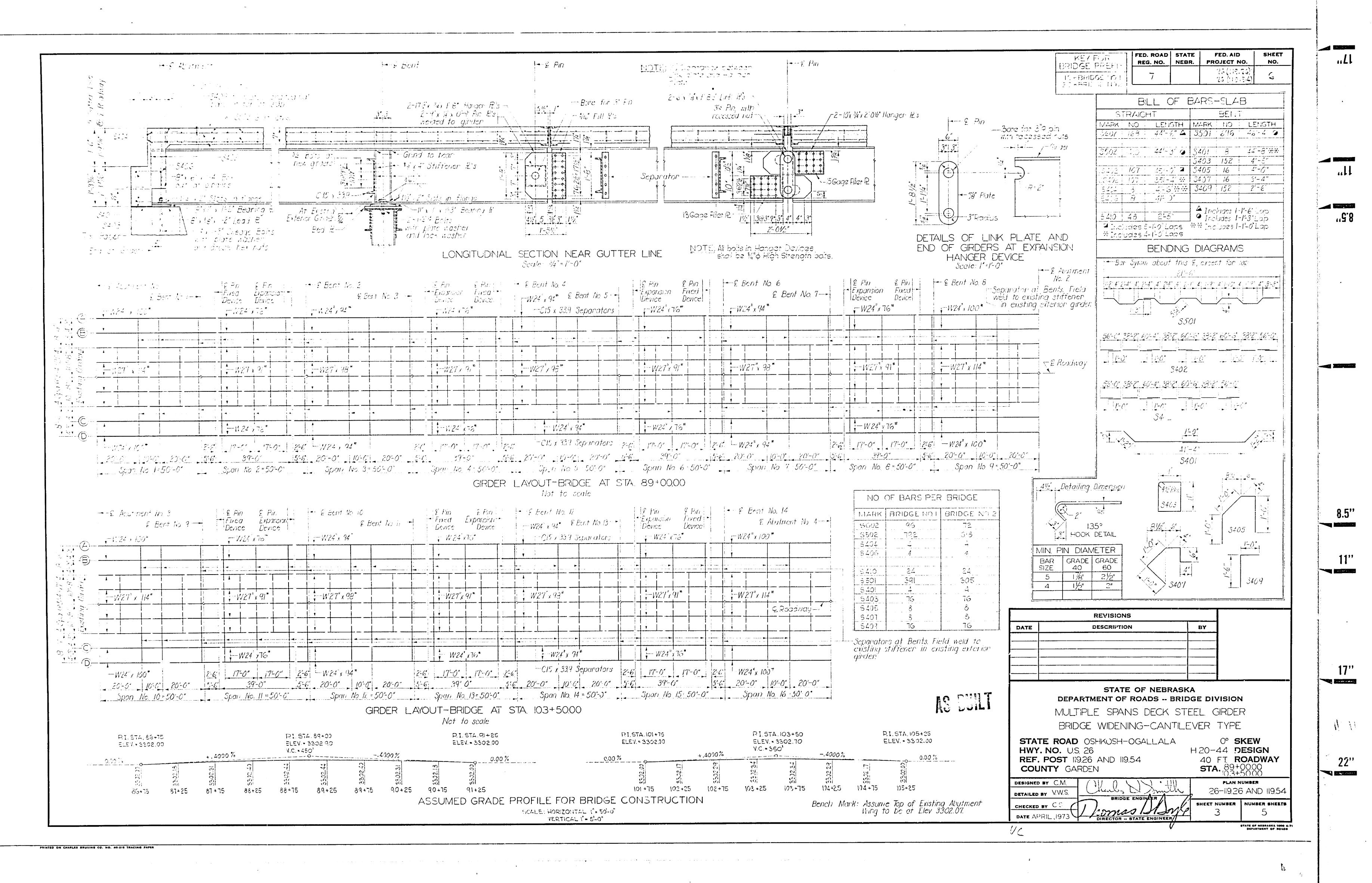
It is further certified that records on this film are microfilmed in conformity with the Rules and Regulations of the State Records Administrator and the Statutes governing them, and that the microphotographic processes accurately reproduce the records and that the film forms a durable medium for reproducing the original, if necessary.

Data 9-10-76

Microfilm Operator

Alka R. Evers

Reproduction Supervisor



AO

1 1

CERTIFICATE OF AUTHENTICITY

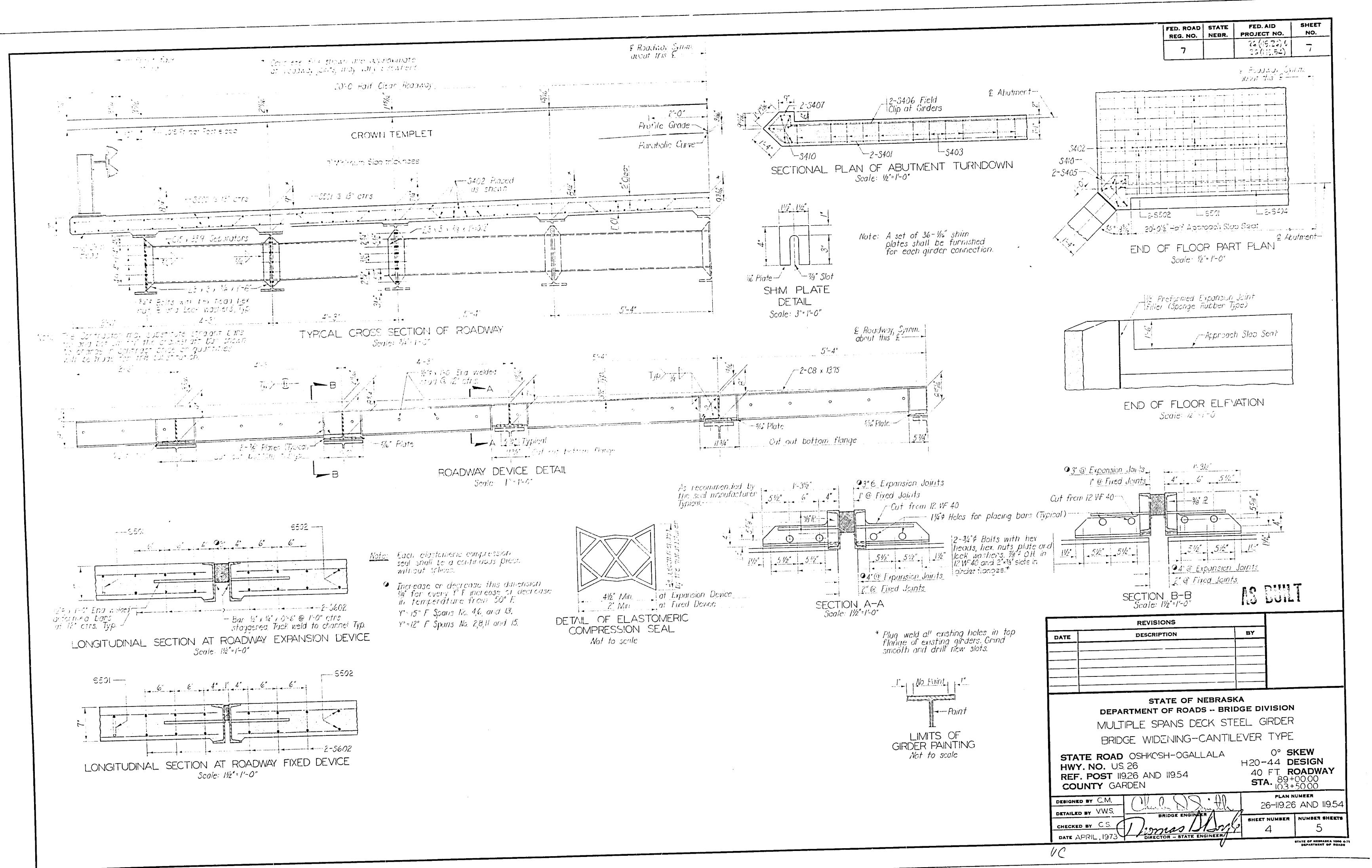
This is to certify that the microphotographs appearing on this film are true and accurate reproductions of the original records produced in the regular course of business.

It is further certified that records on this film are microfilmed in conformity with the Rules and Regulations of the State Records Administrator and the Statutes governing them, and that the microphotographic processes accurately reproduce the records and that the film forms a durable medium for reproducing the original, if necessary.

irable medium for reproducing the original,

Microfilm Operator

Alberton Supervisor



......

1 1

8.5

8.5'

11"

Company of the Control

22"

34'

CERTIFICATE OF AUTHENTICITY

This is to certify that the microphotographs appearing on this film are true and accurate reproductions of the original records produced in the regular course of business.

It is further certified that records on this film are microfilmed in conformity with the Rules and Regulations of the State Records Administrator and the Statutes governing them, and that the microphotographic processes accurately reproduce the records and that the film forms a durable medium for reproducing the original, if necessary.

Date 9-10-76

Microfilm Operator

Microfilm Operator

Reproduction Supervisor

....... NEBR. REG. NO. PROJECT NO. - 26 (119.2*a*) -- 98 - Rownstream Who - US - Wastream Who 2 11/2 24/11, 54, OF BARS-ABUTMENTS € Battered Pile—\ ← € Pile 8' 8' - Outside BENT STRAIGHT MOTE: Remove top of existing wing to an elevation 250 below roadway grade, or nemove completely. jace of wing LENGTH | MARK | NO 2-A402 US 2-A404 DS 2-A401 US 2-A411 DS 2-1406 US 14'-11' 1A409\$ A415 'Flaced as shown 8 | 9-7" 88 9-10" Av Break back existing A501 US A501 DS BAR SETS All the second s \_\_\_abutment and cut 9'-10" Av existing channels MARK! MAX! MIN! SETS to this hive A403 | 10'-10" | 8'-10" | 8 of 11 A405 10'-10" 8'-10" 8 of 8 1413 6'-0" 4'-4" 8 of 5 A413 The state of the s A415 64 4503 US 4509 DS BENDING DIAGRAMS -A407 Placed as shown 4-3 1-7 - - - Girger DETAIL OF BATTER A503 US A509 DS PILE CONNECTION 1'-0" 40 Tilz Weep Holes at Elevation 3294.62 Place one cubic foot Scole: 3/4"=1'-0" WING ELEVATION HALF PLAN OF ABUTMENT Scale: 1/2"=1"-0" Scale: 1/2" = 1'-0" of grivel behind ESTIMATED RAIL QUANTITIES each weep hole. 5'-4" 1'-0" 1'-1" RAIL POST ASSEMBLY itti v 1-31 Swedge Boits 1'-0' Sliding Guard Rail Lap (Not Bolted) J 79 0 ANCHOR BOLT LAYOUT I Post W6 x 200 € Anchor Assembly Guard Rail--<sup>1</sup> Base Plate 9" x 1" x 1'-0" 1415 Total Wt. 🤲 🐔 Abutment Lead Plate 9 x 1/8" x 1-0" j£reak back existing : 125.0 Lbs. <u>, jabutment ana eut</u> ' Anchor Plute 8½" x ½" x 1-0" Vieristing charnels = 2-/° x /+c" Swertge 4 Anchor Bolts, 4 Bolts, Washers 事務" OH in web 落" billing Harizontal Beam W6 x 200 ELEVATION 120 ga galvanized shini IR each face of web this side of gap only. 89 Lbs/Lin. Guard Rail (10 ga) Splice Plate 6" x 1/2" x 1'-01/2" 10.1 Los/ea Varies Varies C.I Lbs/en 1'-0" 3" 1'-0" %® End Welded Studs Post : 31 7 31 31 31 31 W6 x 20.0 Horizontal Beam ------ 2-R 41/2" x 1/2" x 2'-5" 15/9" x 11/2" End welded Istua front of plate. 4403 9'-4" Max 7'-4" Min. 🔪 -Guard Rail 1/2 x 5" slot in web, 1/3" -- R 6" x 1/2" x 1-01/2" --Splice Plate bolts with double nuts DETAIL OF RAIL AT NOTES SPLICE PLATE EXPANSION JOINT DETAIL This Handrail is designed in accordance with the 16th Edition Scale 34"-1'-0" Scale: 11/2"=1'-0" of the A.A.S.H.O. Standard Specifications for Highway Bridges.

Posts and Rail shall meet the requirements of A.S.T.M. A36 steel.

Anchor Bolls shall conform to A.S.T.M. A307 requirements, The nuts, washers and top four inches of bolt shall be galvanized in accordance with A.S.T.M. designation A123.

Post and Beam and handware shall be galvanized in accordance with A.S.T.M. designation A153. 8' 8" /-9" HALF ABUTMENT ELEVATION ABUTMENT SECTION Scale: 1/2"=1'-0" 13,4 /3/4 15/1 / 1-3/4 plain bors x 3-0" with hook Scale: 1/2"=1'-0" 1/2" Gop of Beam BASE PLATE DETAIL Splice as required— 4 --4-Scale: 1/2"=1'-0" REVISIONS المالات الله DESCRIPTION BY DATE - We'd Holes (Typ.) -Splice Plate W6 x 200 x 1'-101/4"--Tin beam rod R 2"x 1/2" x 1-4"--Standard Guard Roi/ No 10 ga -W6 x 20.0 ANCHOR ASSEMBLY DETAIL W6 x 20.0 Horizontal Beam -BEAM CONNECTION TO POST ・%サメル2 End Welded Studs Scale: 1"=1'-0" 1/2 Drain at 4-0" ctrs. Scale: 11/2"=1-0" \*\*\* E Abutment 2-5/8" \$ 11/2" Bolts, hex. STATE OF NEBRASKA nut and plate washer DEPARTMENT OF ROADS -- BRIDGE DIVISION 2'-0" 2'-6" 14 Spa @ 6'-3" = 87'-6" MULTIPLE SPANS DECK STEEL GIRDER W6 x 20.0 x 1'-10¾° post----3" 900 3" 900 3" 900 BRIDGE WIDENING-CANTILEVER TYPE Ent Lead R. 9" x 1/8" x 1-0" STATE ROAD OSHKOSH-OGALLALA O° SKEW 3/4" Chamfer-H20-44 **DESIGN HWY. NO.** U.S. 26 40 FT ROADWAY **REF. POST** 119.26 AND 119.54 I"\$ x 0'-91/2" Anchor bolts
Hex. nut and plaie washer
Bridge No.1 11/8" \$ O.H. in base plate end
bridge No.2 welded to 1/2" anchor plate. **STA.** 89+0000 **COUNTY** GARDEN 10 10 to 10 Anchor Assembly (See Detail) Span No.8 DESIGNED BY C.M. PLAN NUMBER -Anchor R 81/2" x 1/2" x 1'-0" Span No. 12 26-119.26 AND 119.54 Span No.11 DETAILED BY V.W.S. SIDE ELEVATION OF POS. SHEET NUMBER NUMBER SHEETS PART ELEVATION OF RAIL Scale: 1" = 1'-0" DATE APRIL 1973 NOT TO SCALE STATE OF NEBRASKA 1000 4-7: DEPARTMENT OF ROADS

34"

DEPARTMENT OF ROADS
OFFICE SERVICES SECTION

CERTIFICATE OF AUTHENTICITY

This is to certify the microphotographs at pearing of this film are true and accurate reproductions of the original records produced in the regular course of business.

It is further certified that records on this film are nucrofilmed in conformity with the Rules and Regulations of the State Records Administrator and the Statutes governing them. The microphotographic processes accurately reproduce the records and the film forms a ducable medium for reproducing the original, if necessary

Date

Microfilm Operator

Office Services Manager

Grade-	E Abutment No. 11. 310 86+7500 Gr. Elev 330200	\$ 8ent No. 1 \$to 87+25.00 Gr. Elev 3302.18	E Bent No 2 510 81+1500 Gr Elev 330231	E Bent No. 3 3 to 88 + 25 00 Gr. Elev 3302 40	E Bent No 4 Sta 86.75 CO Gr. Elev 330244  LE Bridge Stu 89.0	1	E. Bent No 6 3ta 89.1500 Gr. Elev. 3302.40	E Bent No. 7 Sta 90+2500 Gr 1 lev 330231	E Bent No 8 Sto 90-7500 Gr Elev 3302.16	Sto 9: 23 60 Gr Llev 3302.00	POTENTIA TO A CONTROL TO A CONT	ROJECT NO.
329:517				Waterwork and below for the by Works a 2,520 sq 22.	11. Liss 32814-	HW Elex 3215 of		ed a sent an acceptable with a feather than the acceptable and the sent and the sen		- Uev 329.87	NOTES	
					GENERAL ELEVATION Scale 1-20-6	N (BRIDGE NO.1)		Acfile of	Naturot Smard	10.1.1 Asph full wi the bri	altic Concrete wedge on approach of the bridge and 30 Ft. idge floor.	each slubs are from the end
	£ Abutment No. 1	Bent No I	- E Bent No ?	Fuce of Roll*		1 Bent No 5	- & Bert No 6	- E Bent No 7	- E Bent No 8	E Abutarent No 2		
	Ena of Floor				Modify Existing Roadway Expansion Device				Lod of Page	Carocily Dale		
ξ. 64 ξ. 62	Sta 86.7450		- Poddicy Fied Device -	manyara principalisa y may da	and the second s				End of flow Sto 4.7550	West Has t.		* *
8 8000 S					3				The second secon			
100 July 100	Span No 1:50:0"	54.10 to 2.50.0°	\$ 500 No 3 50-0°	Spor: No. 4: 5 10	\$ 6		5.6° 5-6 Span No 7-53'-0"		5'-6' 35'-0' 80 9-50'-0"			
		سعاد داد اداد اداد اداد اداد اداد اداد ا	Charge to the the of an a		CELERAL PLAN	A second prince of the second	en e		·		CUANTITIES	
N	And the state of t	e eratina concrete dech t Lia du diction alli acall	·				ور من المعادية			Structural Steel for Dam 1		200 11
	shown on this sheet	- 310 101 1500 Gr Llev 330200	Sto 102 - 2500 Gr. Elev 335217	Gr 1 (6) 35 (2) 19	18 Sept 10 18 18 18 19 19 19 19 19 19 19 19 19 19 19 19 19	5- 1 ke 33.72 st	310 164 125 60 Gr Eliv 33 3224	5to 104+1530 Or Lev 330217	Gr. tie. 330200	PL 14" x 3/4"	316 Lbs255 Lbs	_ 30 Lm.
<i>y</i>	Of Mr. S				St. 123				in the state of th	R 174 x 74 Total	"356 Lbs	80 Lin.
	11. 5245 X								A Contraction	Asphaltic Concrete, Type "C	PRIDGE NO. 2	
	A ST CONTRACTOR OF THE STATE OF		<b>4</b>		GELERAL ELEVATION	त्रेष्ट्र (संस्थाप्तर १७०८) । इ		Arefue of Au	tuloja en 1			
				Tyture of finish		}			1- EAD	D. 184" x 3/4"	255 Lbs	80 Lin 1
•					<u> </u>	Roadway Expansion Device		THE THOUGHT			1428 263	
						் இதிருந்து பெறு இருந்து நாட்டிய இருந்து இருந்து இருந்து இருந்து இருந்து இருந்து இருந்து இருந்து இருந்து இருந் இது நார்க்கு						
								•			REVISIONS	
					. Su bodet at . At the Month to 1990 and to but the formation		ne y na he he he he e	I Gu No h · Call ·	• **		DESCRIPTION BY Spholitic Commerce MINS	
		<del>-</del>	į		TURE AL PEARL	•		· · · · ·	• · · · · · · · · · · · · · · · · · · ·	The state of the s		
						,					STATE OF NEBRASKA TMENT OF ROADS BRIDGE DI	
										STATE ROAD HWY. NO. REF. POST (1) COUNTY	ST.	SKEW DESIGN ROADWA
										COTACARD BY	The second of th	PA A 4 FE V or B LA

DEPARTMENT OF ROADS
OFFICE SERVICES SECTION

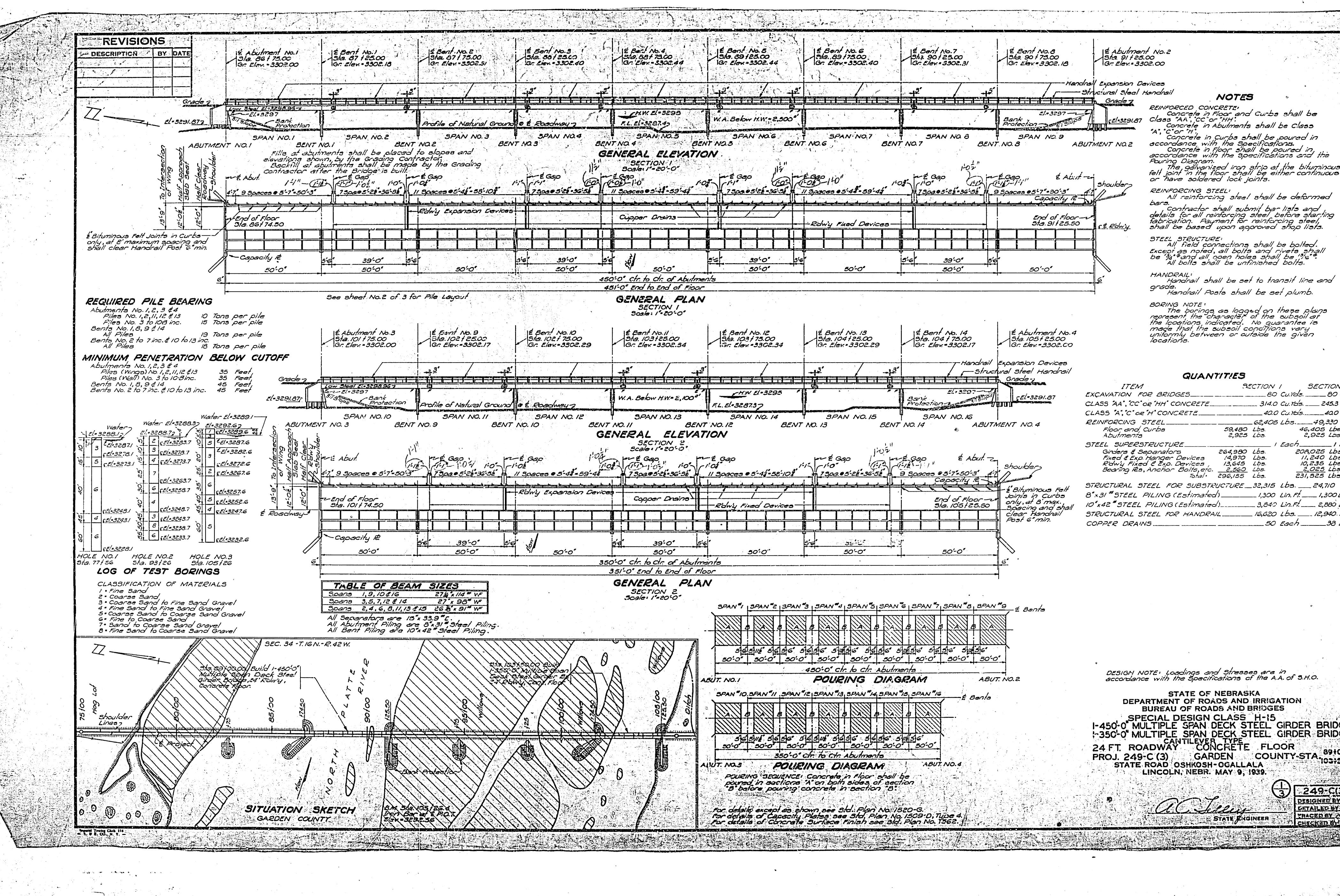
CERTIFICATE OF AUTHENTICITY

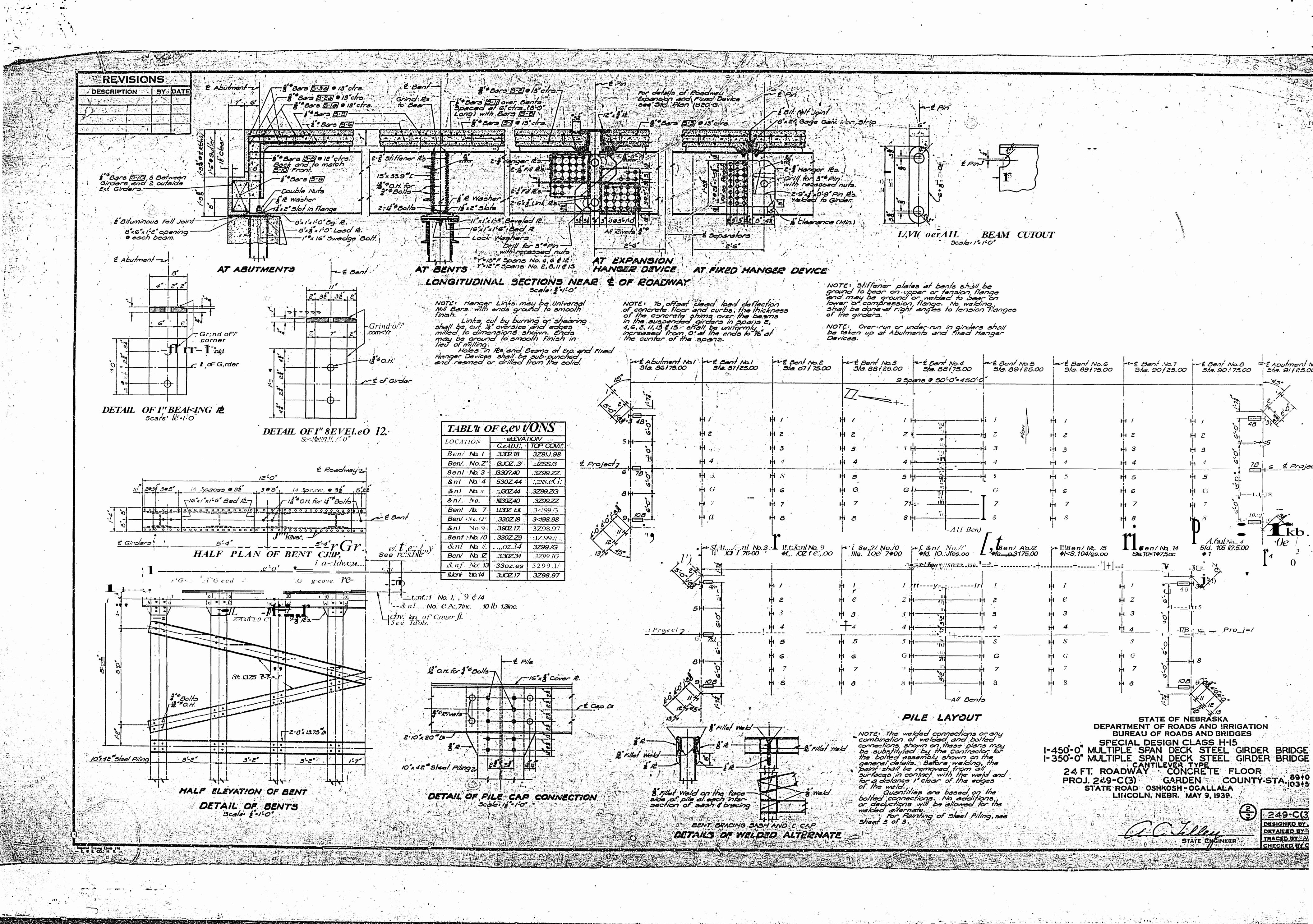
This is to certify the microphotographs app—recontinuation of the original records produced in the regular course of business.

It is further certified that records on this film are microfilmed in conformity with the Rules and Regulations of the State Records Administrator and the Statutes governing them. The microphotographic processes accurately reproduce the records and the film forms a durable medium for reproducing the original, if necessary.

- Front Face of Rail STATE HERRICH TORORT - A. Roadway Symm. about this & NEBR. 20'-0" Halt Clear Roadway .015 Ft. per Foot Slope Profile Grade CROWN TEMPLET Overlay (Thickness Varies) Parabolic Curve --Surfacing Construction Joint WANTE ATTEMATE (Optional) The address, Bent No. 1 Bent And Bent No 2 Sent No 2 Bent No.3 Bent 12 Bent No. 4 Bent 4: 12 # 7 X 7 21 10 2 M 7 7 8 رافیک او در در افغارسان Bent No. 5 Bont Vol3 3'-4" 4'-3" 4'-3" £ - • " Bent No. 6 Bont No 14 Bent No 7 11/2" TYPICAL CROSS SECTION OF ROADMAY Bent No. 8 Scale: 3/4"-1'-0" Field out to provide variable dum rought Detail A Asphaltic Concrete Overlay (Trichiness Varies)
Type "C" New 3/4" Dam B. (Thickress Varies, See Table) Top of Existing Floor Fill with sand and remove after Placing Asphaltic Concrete Overlay Existing Channels 34 wide dam plate Grind fram 1700 -Existing Elastomeric Compression Seat Existing Device DETAIL "A" I ETAIL AT ROMBWAY EXPANSION DEVICE Not to Scale Scale: 1/2"=1'-0" WHILE IN INC. MADE IN THE COURT OF THE Not to Scale Asphaltic Concrete Overlay (Thickness varies)
Type "C" len 14 Dam & OThichness Varies, See . . Detail B" Table) Top of Existing Floor Fill with sand and remove after placing Asphaltic Concrete Overlay NEBRASKA DEPARTMENT OF ROADS instre Elastemeric Com-Existing Channels STATE ROAD SKEW HWY. NO. DESIGN REF. POST ROADWAY Not to Scale COUNTY AREES STA. THE AT RIMINAL FRED DEVICE Scale 1/2"=1'-0" A Company of the Comp The way with PROJECT TOWNER TO SEE THE SEE DESIGNED BY DETAILED BY Superior and the second CHECKED BY

> , ,





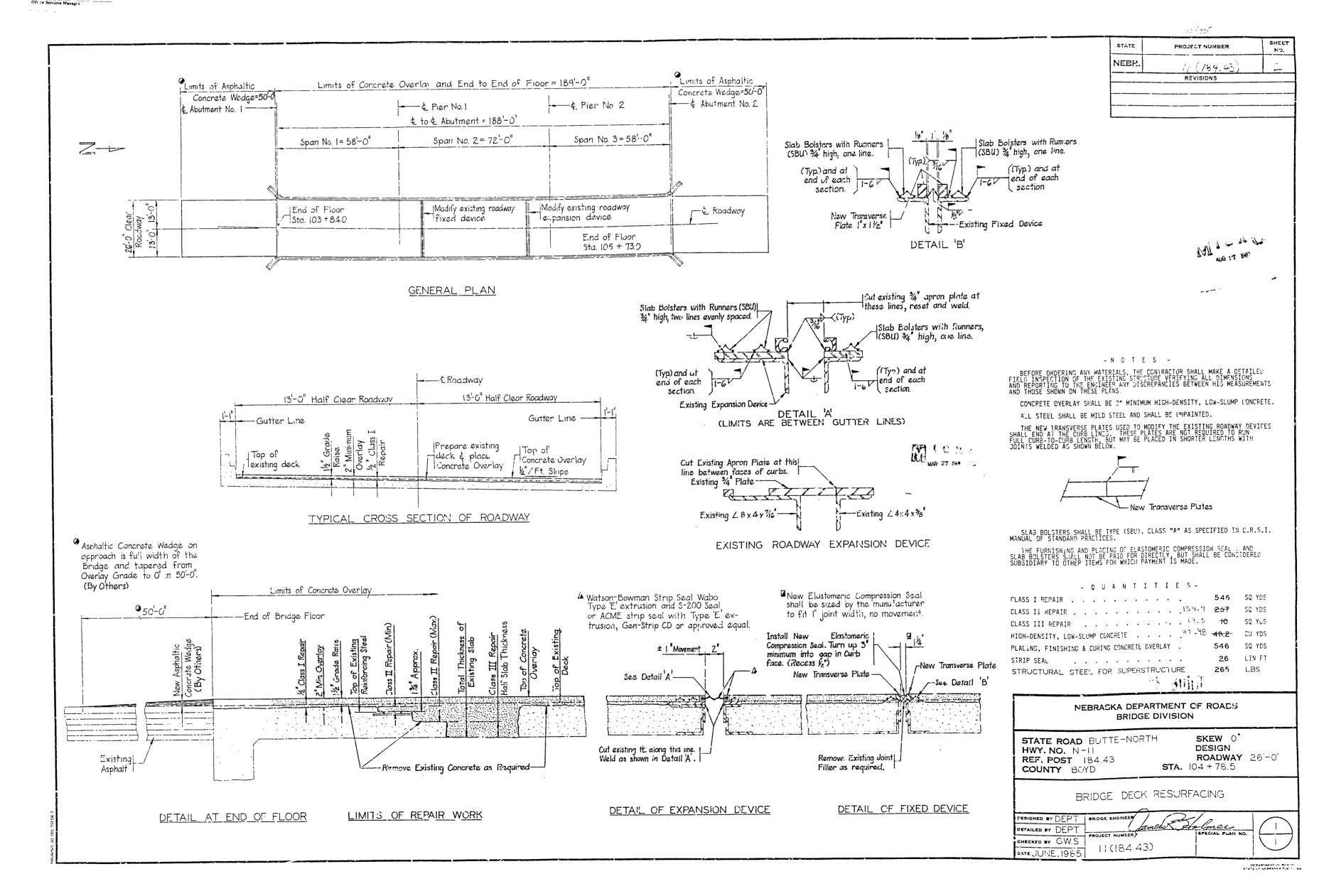
LEPARTMENT OF ROADS
OFFICE SERVICES SECTION
CERTIFICATE OF AUTHENTICITY

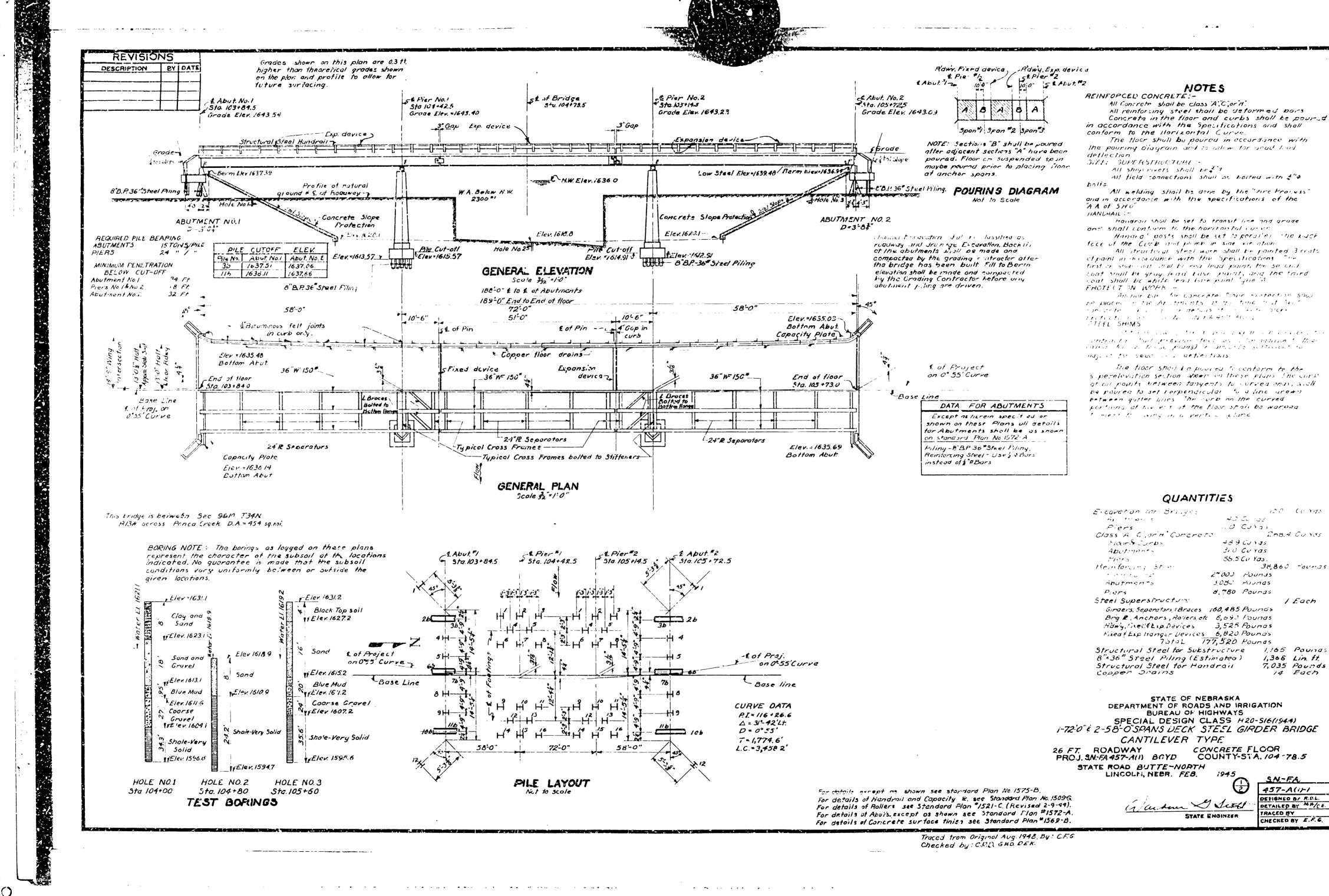
This is to certify the microphotographs appearing or the film are true and securate reproductions of the original records produced in the requisir course of busin as for the control of the film are microfilmed in conformity with the Rules and Regulations of the State Records. Insultantar and the Statutes governing them the microphotographic processes accurately secured the records and the film forms a durable medium for reproducing the original, if necessary.

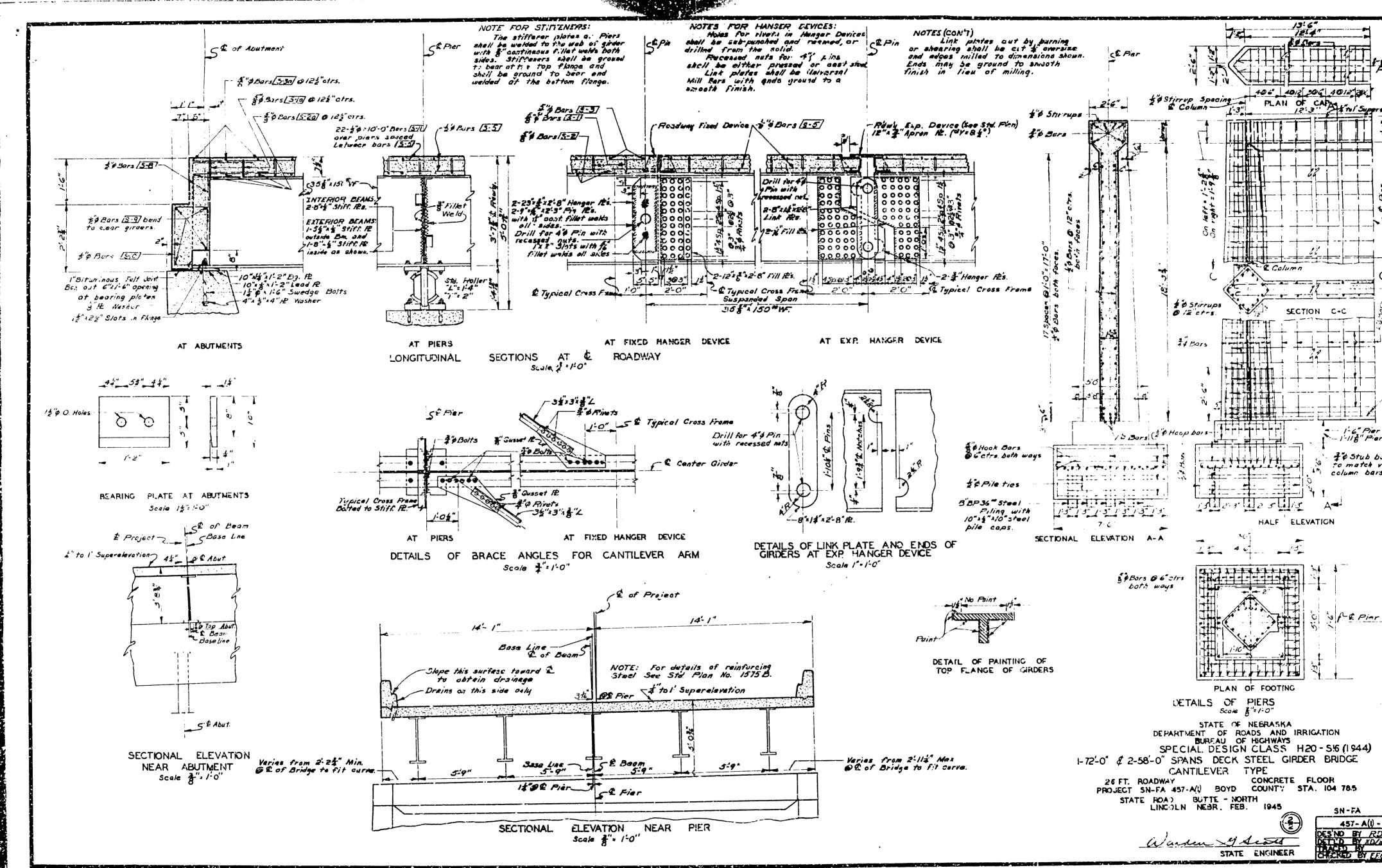
Date.

Microfilm Operator

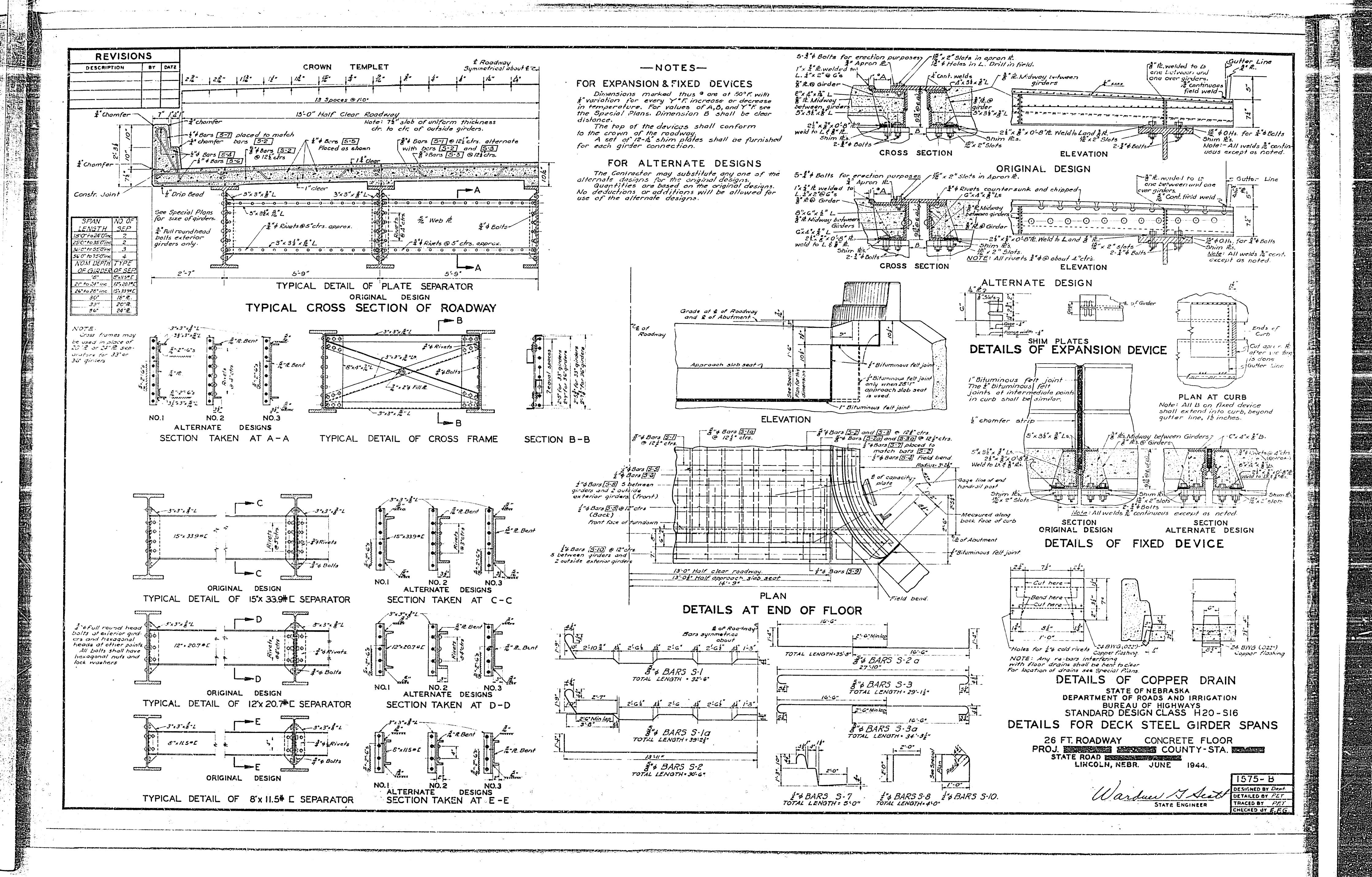
Aller R. Relian

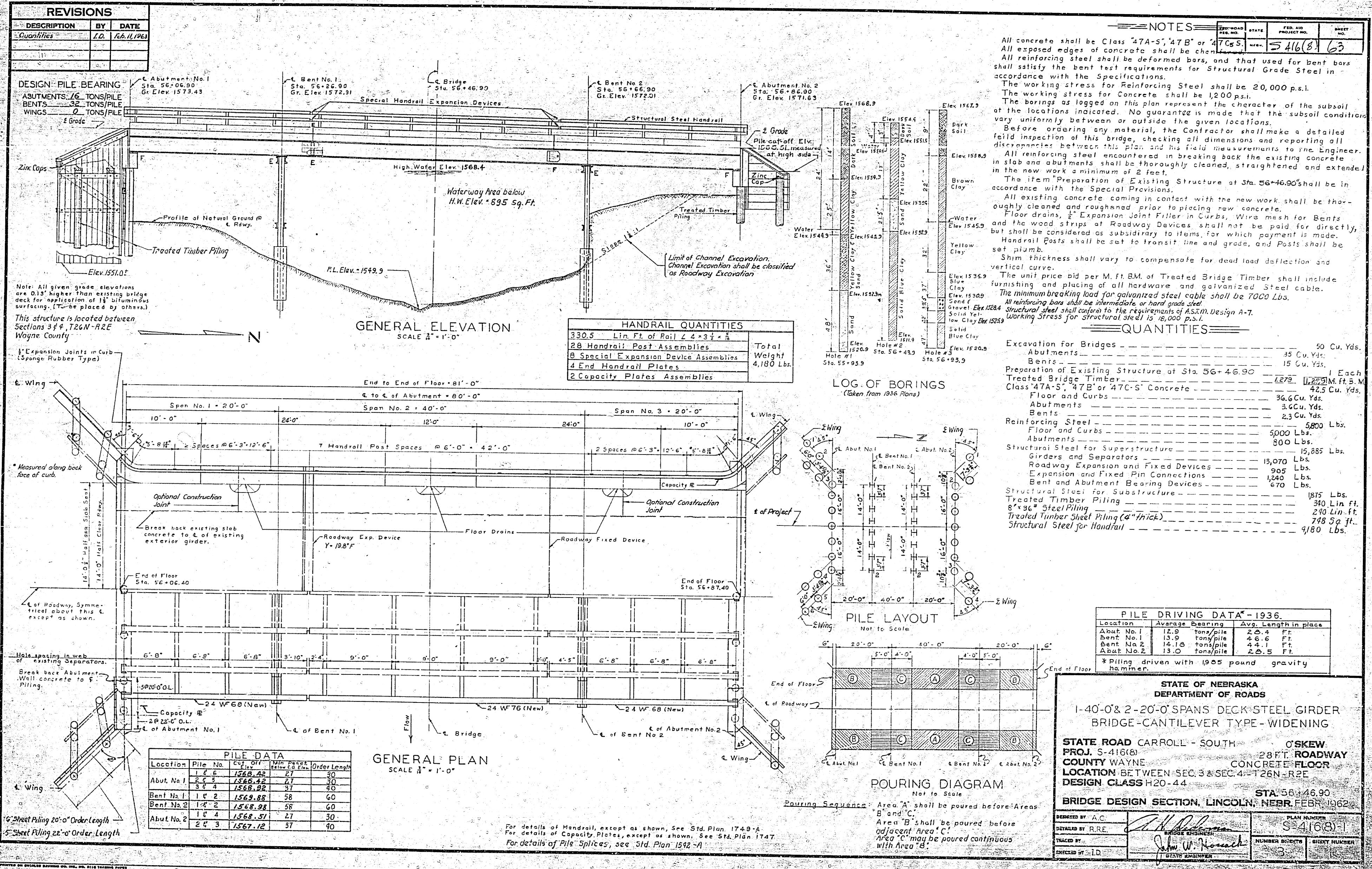


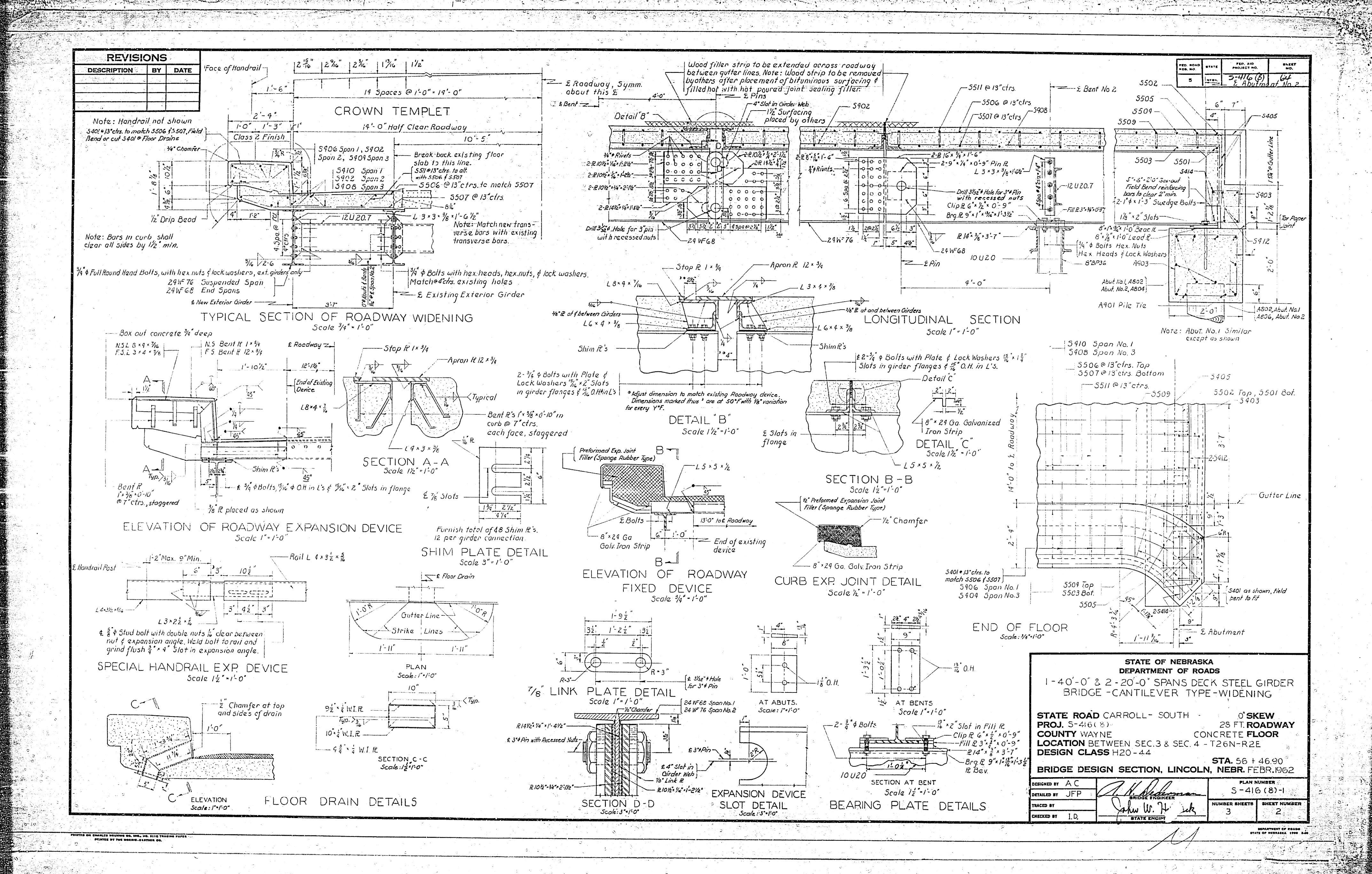


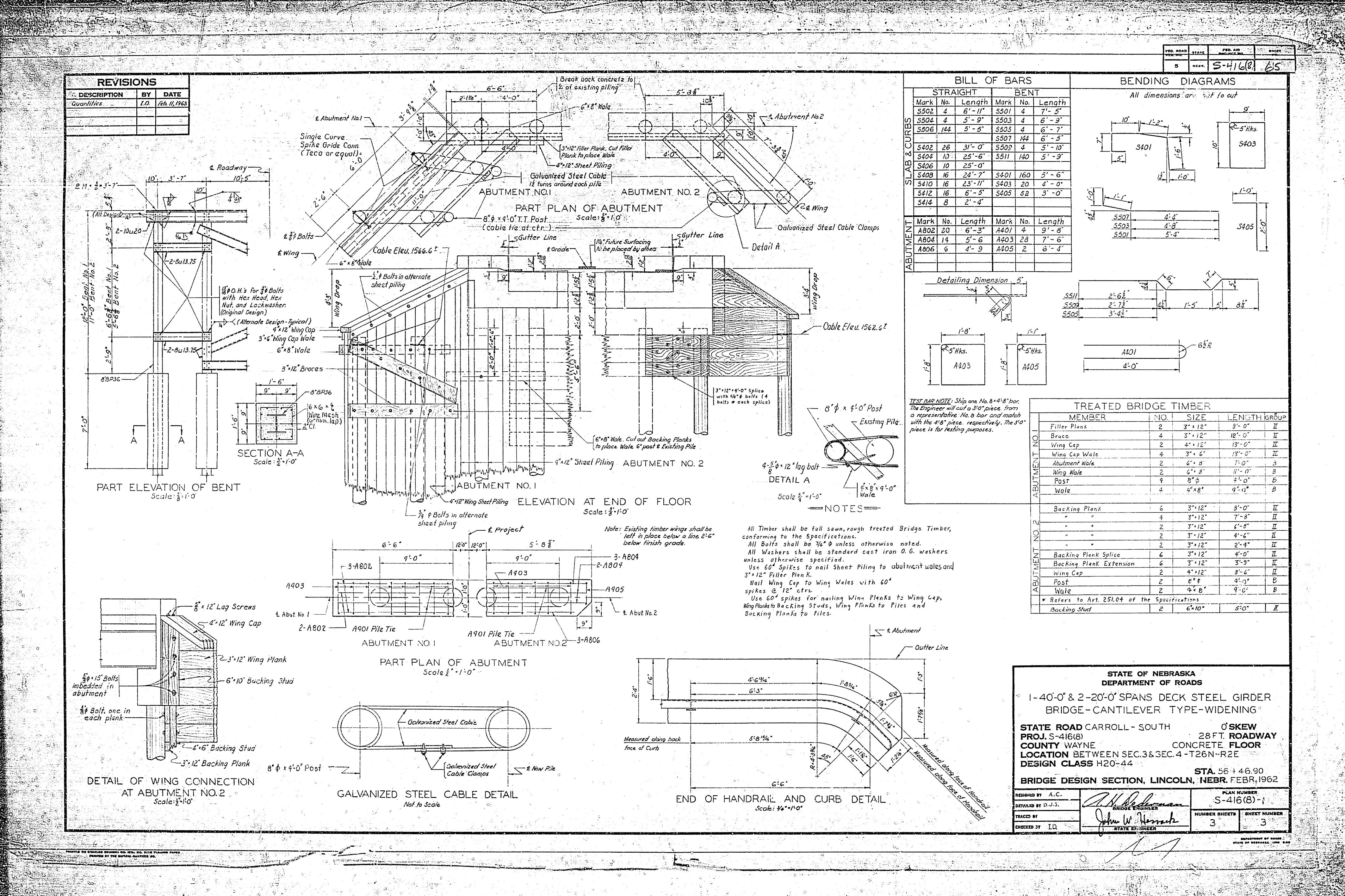


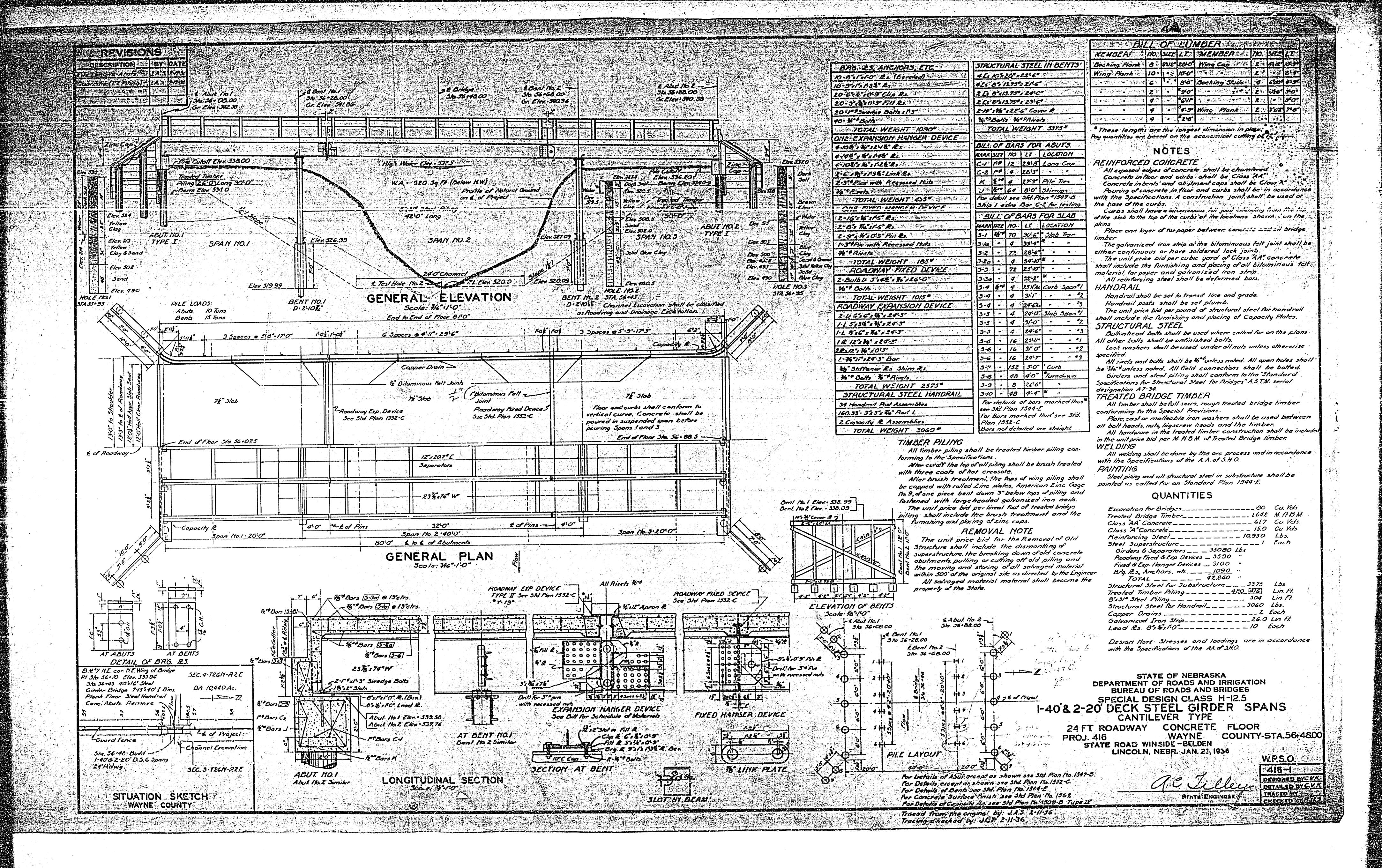
Traced from Original Supt. 7, 1948 By: UD. Chanked Du: LUW. DWW RRD

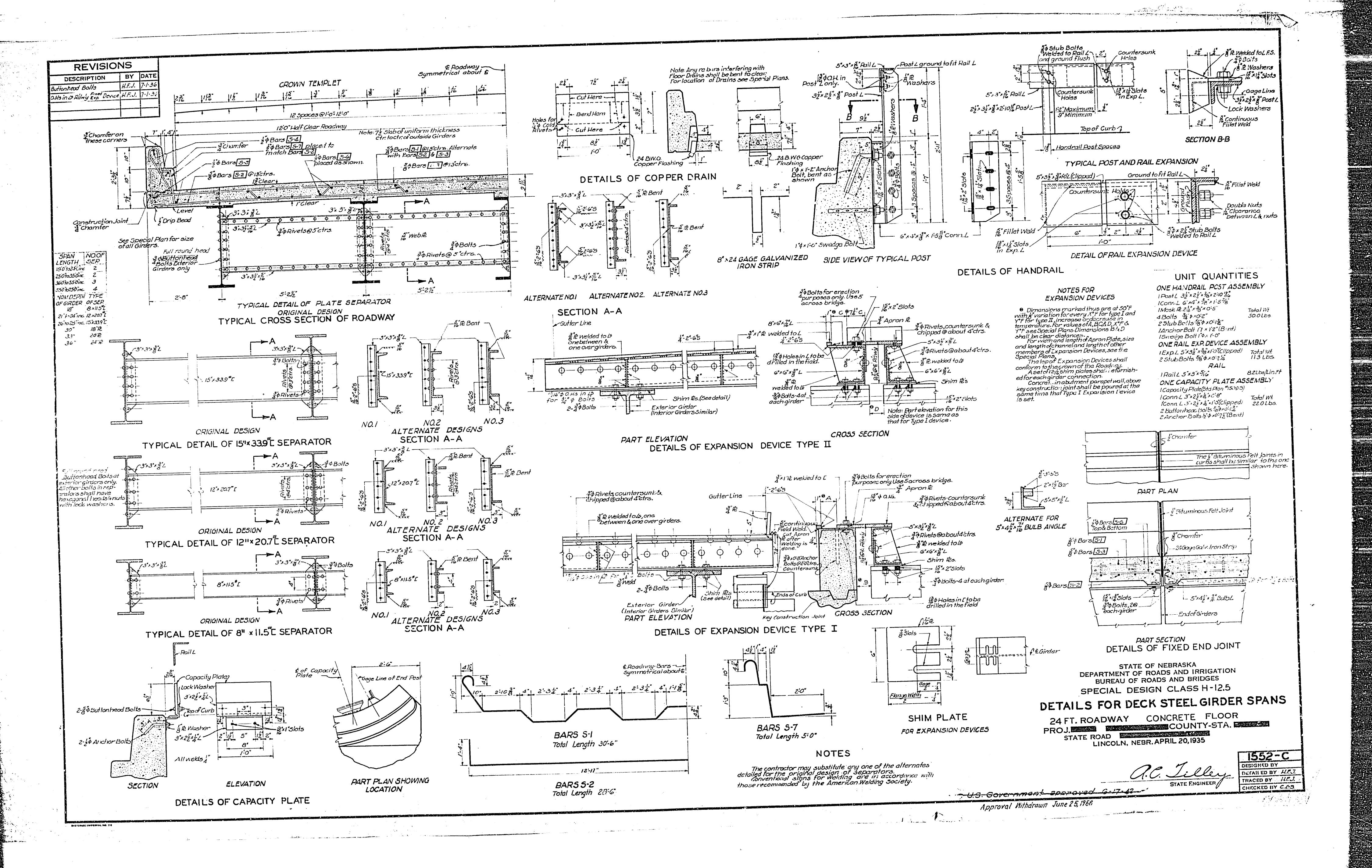




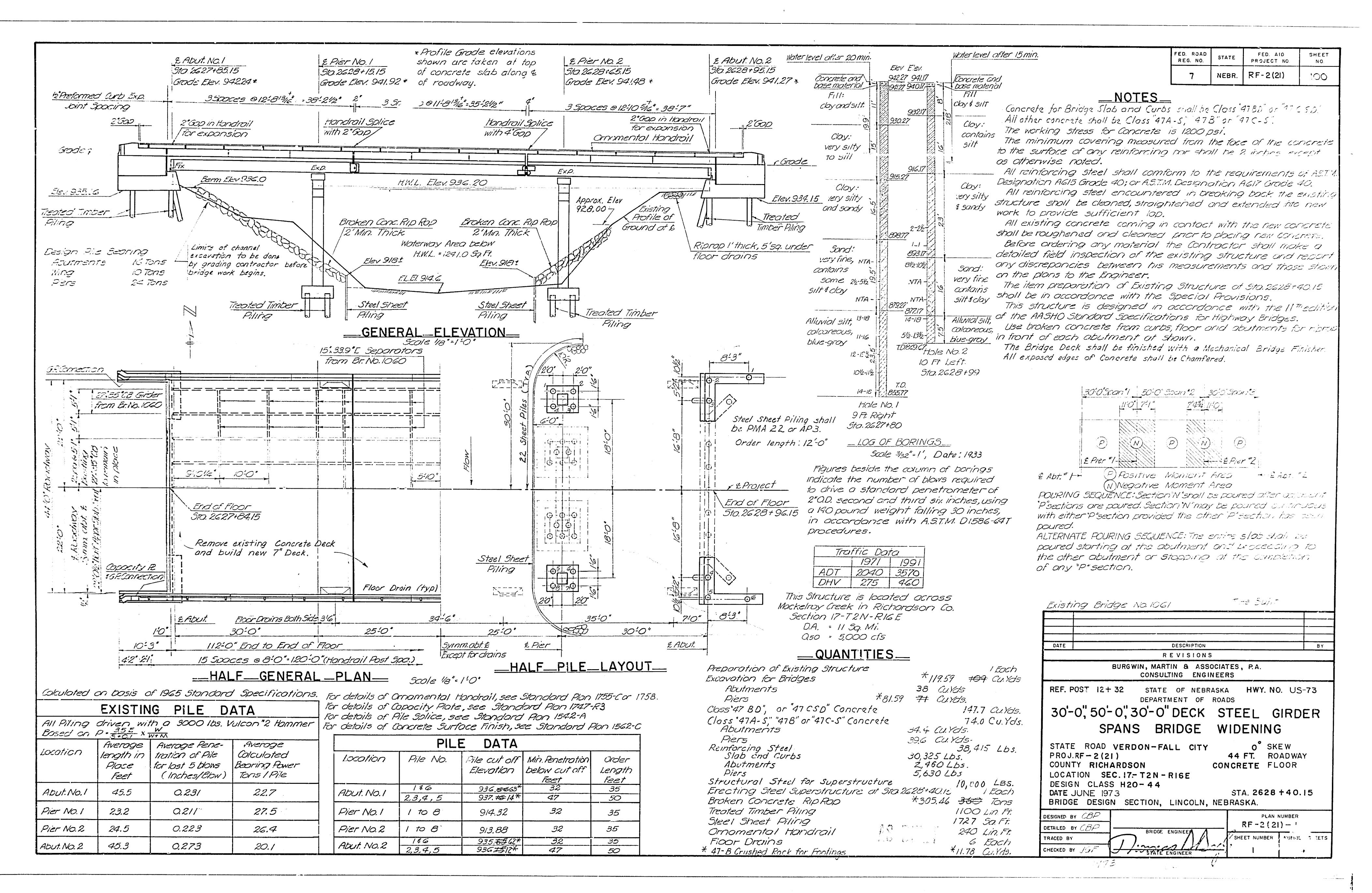




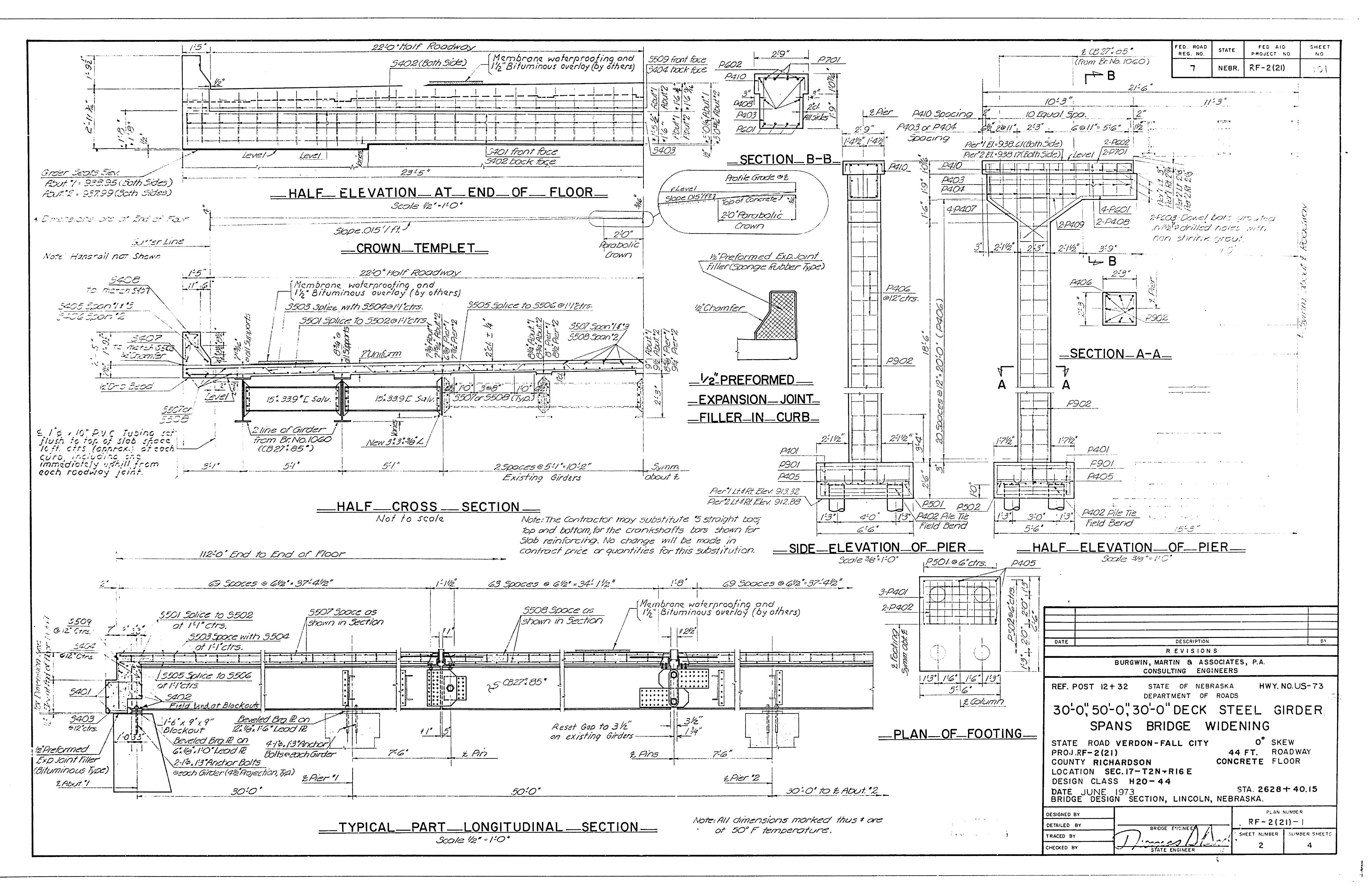




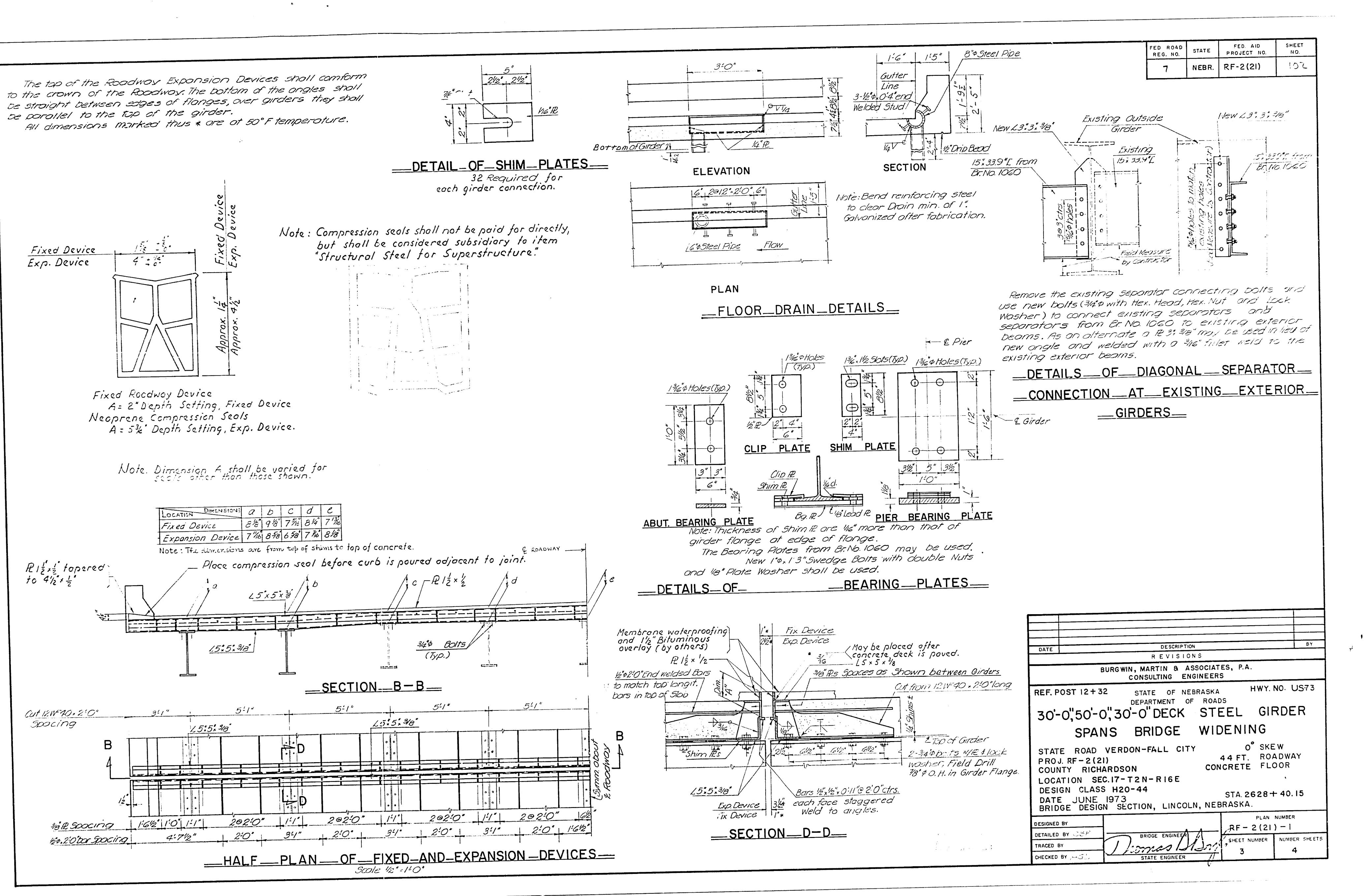
·(O)



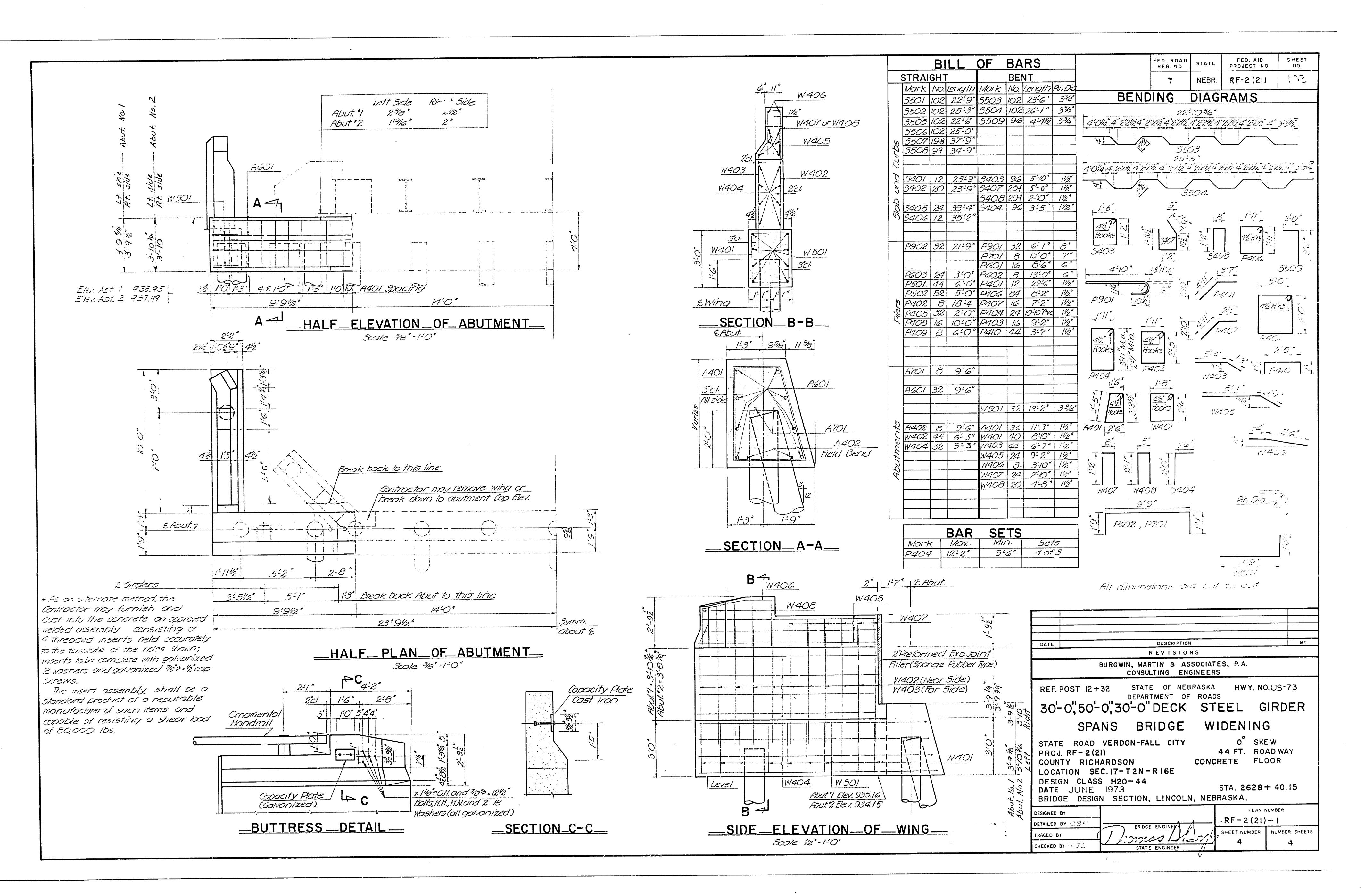
This is to certify that the microphotographs appearing on this film are true and accurate



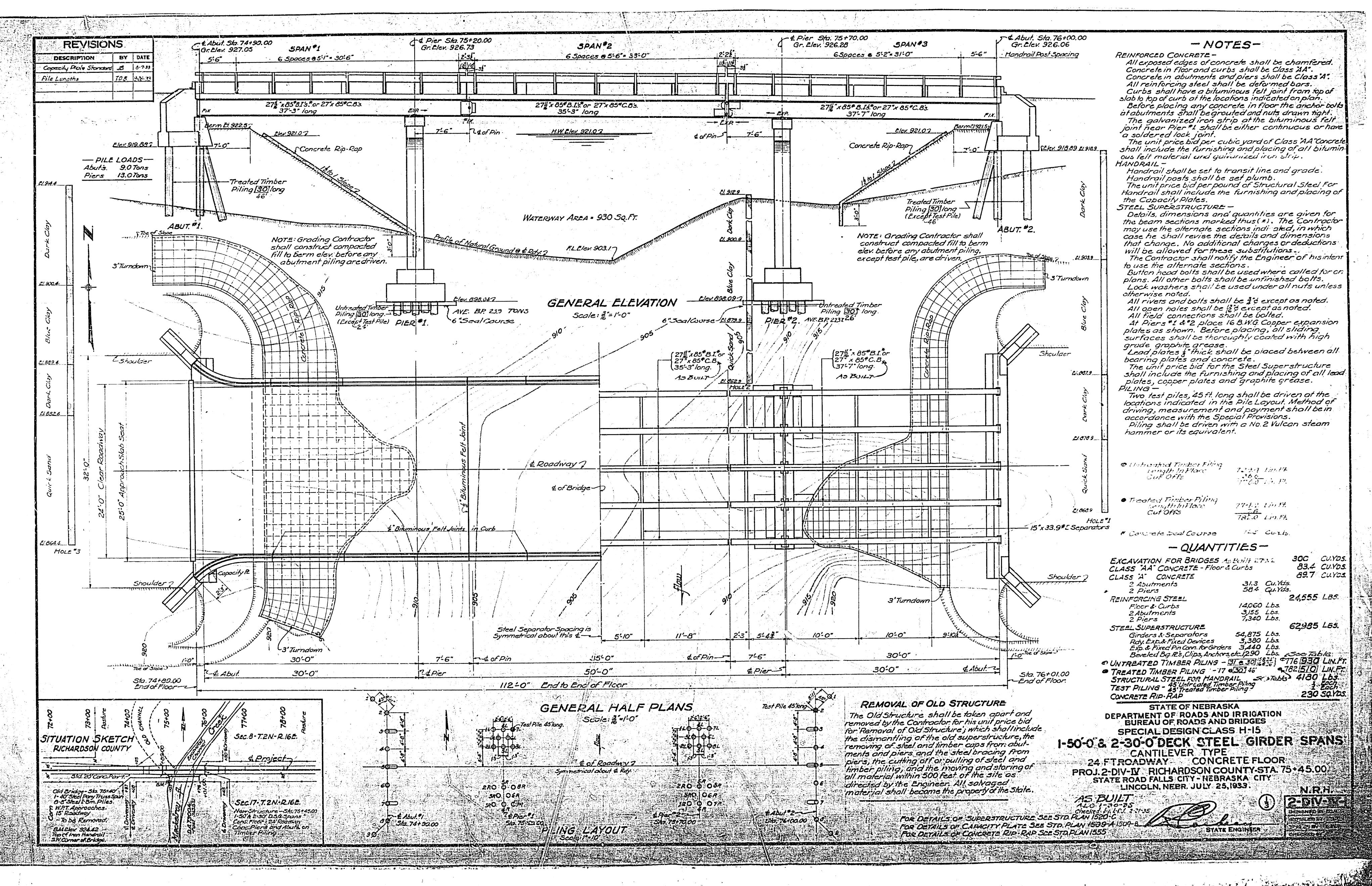
This is to certify that the microphotographs appearing on this film are true and accurate

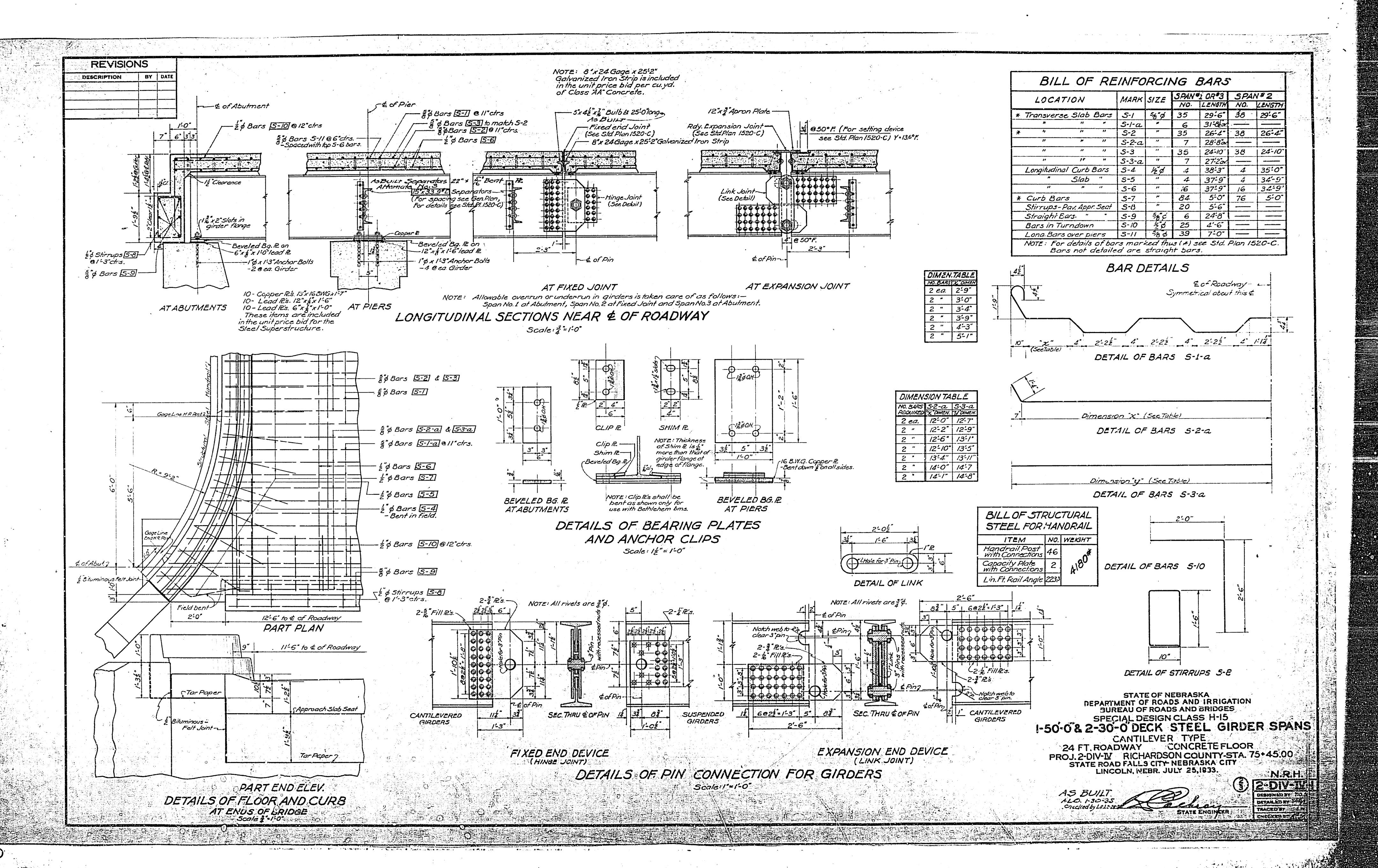


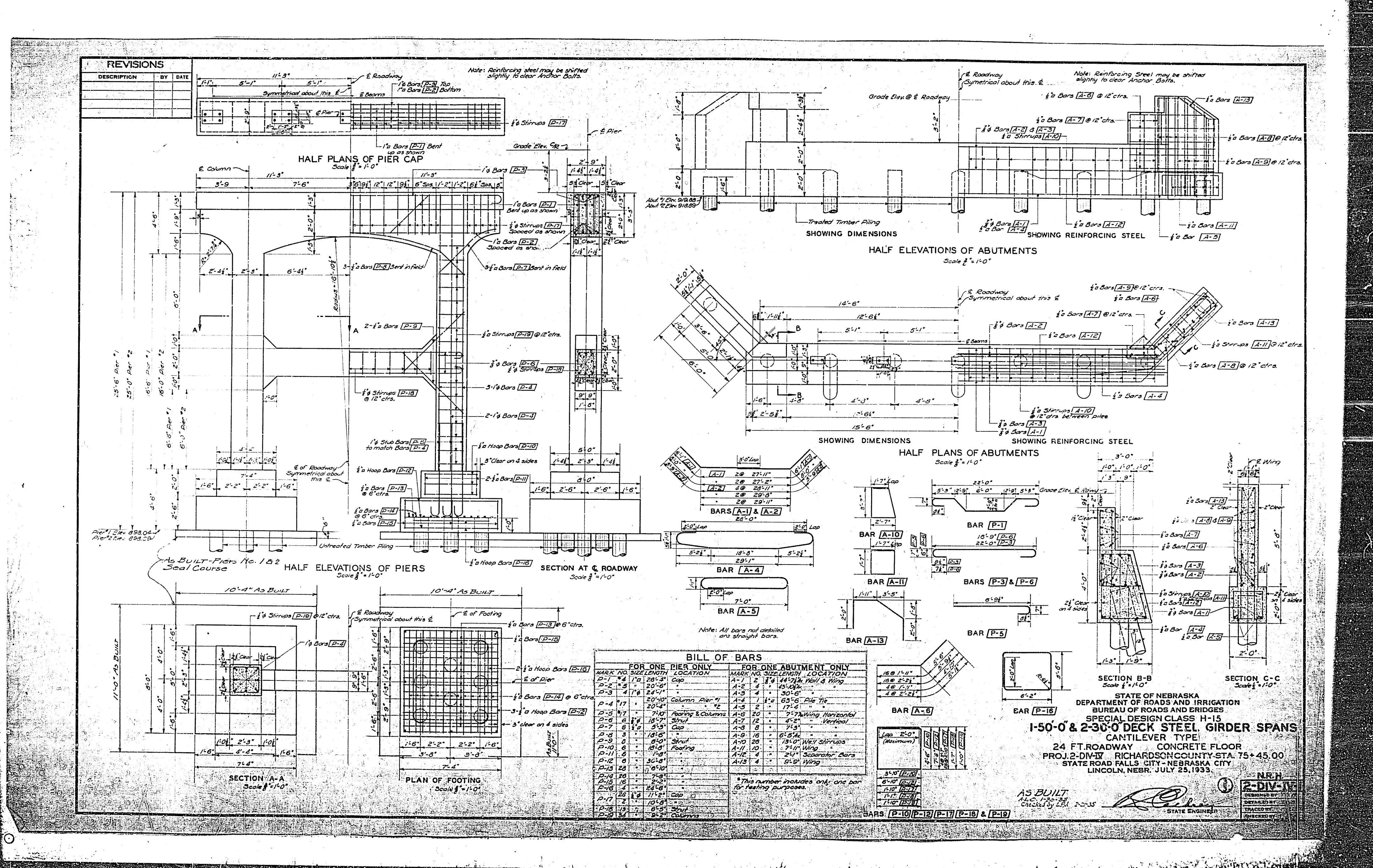
REPRODUCTION SECTION

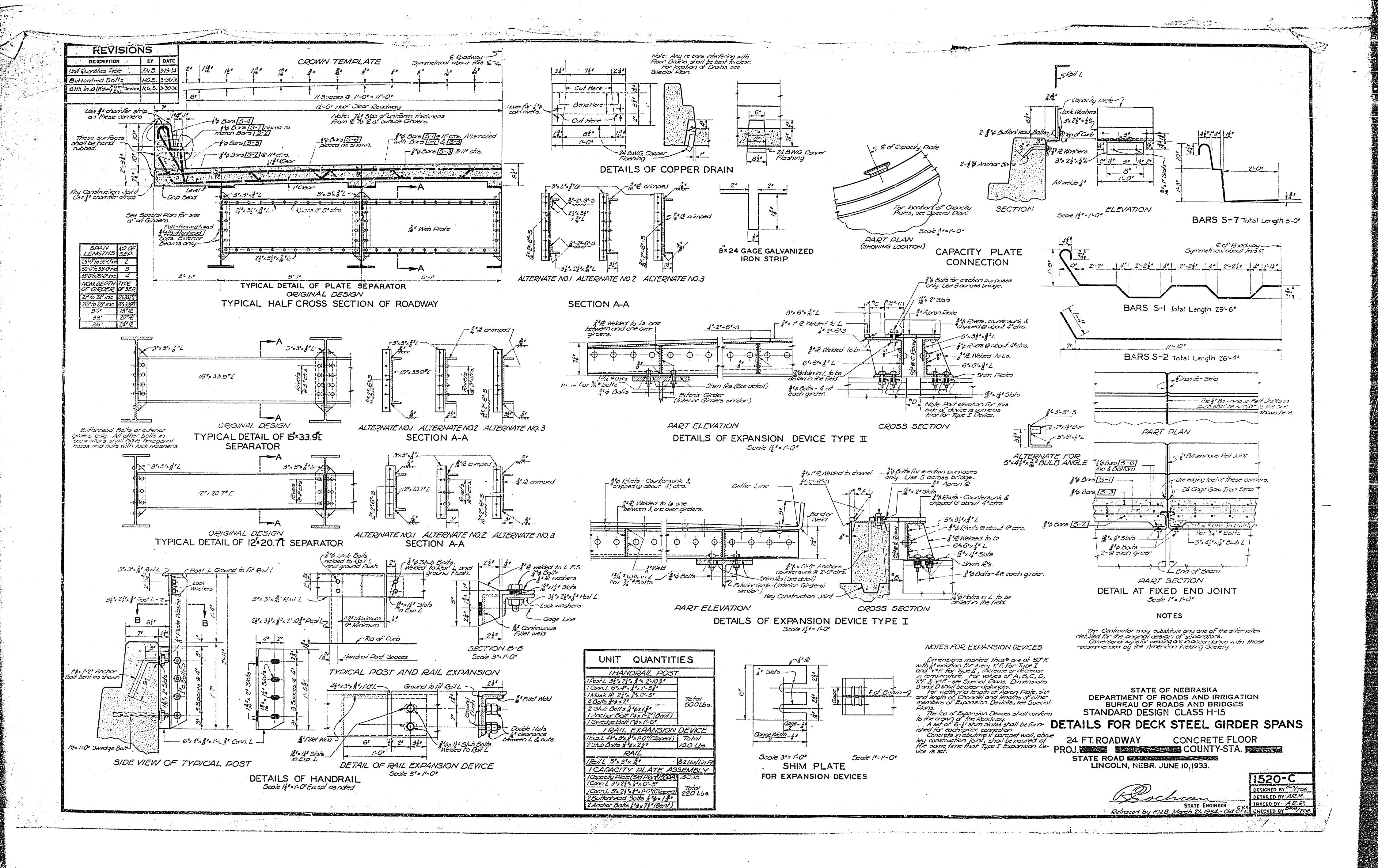


This is to certify that the microphotographs appearing on this film are true and accurate reproductions of the original records produced in the regular course of business.





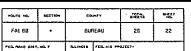




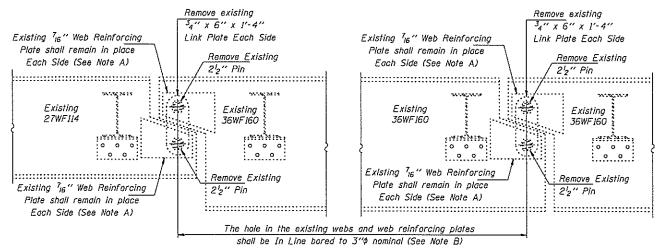
# Illinois Department of Transportation

Standard drawings - pin and hanger assembly replacement.

\* D-2 BRIDGE PIN REPLACE 1997-1



SHEET NO. I5 SHEETS



NUT DETAIL

R = 3" (Typ.)LINK PLATE DETAIL

4" Woven Teflon Bushings (See Note D) 134" Thread (Typical) (Typ.) 16)

- <sup>5</sup>a" thick Hex Nuts (Each Side) Nuts shall be ASTM A-576, Grade 12L14, minimum yield of 36 ksi. (See Noté E)

21/2" nominal diameter Pin (diameter tolerances subject to Specifications of Teflon Bushing Manufacturer and shall be approved by the Engineer). Pin shall be ASTM A276, UNS 21800 (Nitronic 60 or equal) (No step at threads) 12 threads per inch. Install prior to new link plates.

Silicone Sealant suitable for Structural Steel (See Note F)

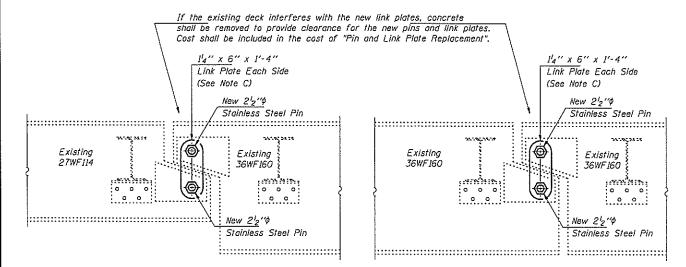
### SECTION THRU PIN (20 Required)

# ELEVATION AT EXISTING PIN ASSEMBLY

FOR INTERIOR BEAMS

ELEVATION AT EXISTING PIN ASSEMBLY FOR EXTERIOR BEAMS

Any Pins that can be easily removed without damage to the pin shall be salvaged and the Bridge Engineer shall be contacted for disposition. Cost of salvage is included in "Pin and Link Plate Replacement".



ELEVATION AT NEW PIN ASSEMBLY FOR INTERIOR BEAMS

APRIL 29.

ELEVATION AT NEW PIN ASSEMBLY FOR EXTERIOR BEAMS

Existing welds shall be inspected for cracks using liquid dye penetrant or magnetic particle testing. Any cracks that are found shall be identified and reported to the Bureau of Bridges and Structures for further disposition. Clean and paint before installing new link plates.

### Note B:

Bore diameter for bushing in link plate, existing webs and web reinforcement plates shall correspond to bushing manufacturer's allowable tolerances for proper functioning. Hole diameter may be adjusted to allow use of stock bushings.

Inside face of new link plates shall receive first field coat in shop. The primer shall pass the M.E.K. Rub Test before the first field coat is applied.

Actual bushing thickness per manufacturer's specifications, 14" is approximate. Bushings shall be a self lubricating filament wound epoxy matrix backed Duralon Bearing, metal backed Fiber Glide Bearing or equivalent. No primer or grease shall be allowed on bushings. Bushings shall be suitable for dynamic loads of 20,000 psi.

Tighten inside nuts to bring all bushings into firm contact. then back off is turn and tighten outer nuts.

### Note F:

Apply 38" bead to face of the web reinforcing plates approximately '2" from bushing immediately before installing new link plates. Place sealant around nuts after installation. Sealant shall be suitable for prolonged exterior exposure without losing flexibility or adhesion to painted steel surfaces. Proposed products shall be subject to Department's acceptance based on documented testing or other evidence

## GENERAL NOTES

All new structural steel shall conform to AASHTO Classification M-270 Gr. 36. unless otherwise noted.

The Contractor shall provide support and/or sharing systems for the beam in the area of existing pin and link plate replacement. See Special Provision "Temporary Support System."

The inorganic zinc rich primer/acrylic/acrylic paint system shall be used for shop and field painting of new structural steel except where otherwise noted. The color of the acrylic finish coat shall be Interstate Green, Munsell No. 7.5G 4/8. See Special Provisions "Cleaning and Painting New Metal Structures". Cost shall be included in the cost of "Pin and Link Plate Replacement".

Existing Structural steel shall be cleaned and painted as required by the Special Provision "Cleaning and Painting Adjacent Areas of Existing Steel Structures". Cost shall be included in the cost of "Pin and Link Plate Replacement,"

All existing steel surfaces behind link plates shall be cleaned and primed before installation of new link plates. Cost shall be included in the cost of "Pin and Link Plate Replacement."

Plan dimensions and details relative to existing structure have been taken from existing plans and are subject to nominal construction variations. It shall be the Contractor's responsibility to verify such dimensions and details in the field, except the pin diameters, and make necessary approved adjustments prior to construction or ordering of materials. Such variations shall not be cause for additional compensation for a change in the scope of the work, however, the Contractor will be paid for the quantity actually furnished at the unit price bid for the work.

The Pins and Link Plates shall conform to the minimum Charpy V-Notch Taughness of 25 ft.-lbs. at 40° F.

The pins, link plates, bushings, nuts and silicone sealant are the items included in "Pin and Link Plate Replacement".

## TOTAL BILL OF MATERIAL

ITEM	UNIT	<b>OUANTITY</b>
Temporary Support System	Each	10
Pin and Link Plate Replacement	Each	10
Silicone Joint Sealer	Faat	75
	Ì	

PIN REPLACEMENT FAS 309 SEC. 06-7HB-1 BUREAU COUNTY STA. 1738+38 STR. No. 006-0133

## MAXIMUM REACTIONS AT PIN

RĐ	(K)	22.3
RŁ	(K)	30.3
Imp.	(K)	9.1
R (Total)	(K)	61.7

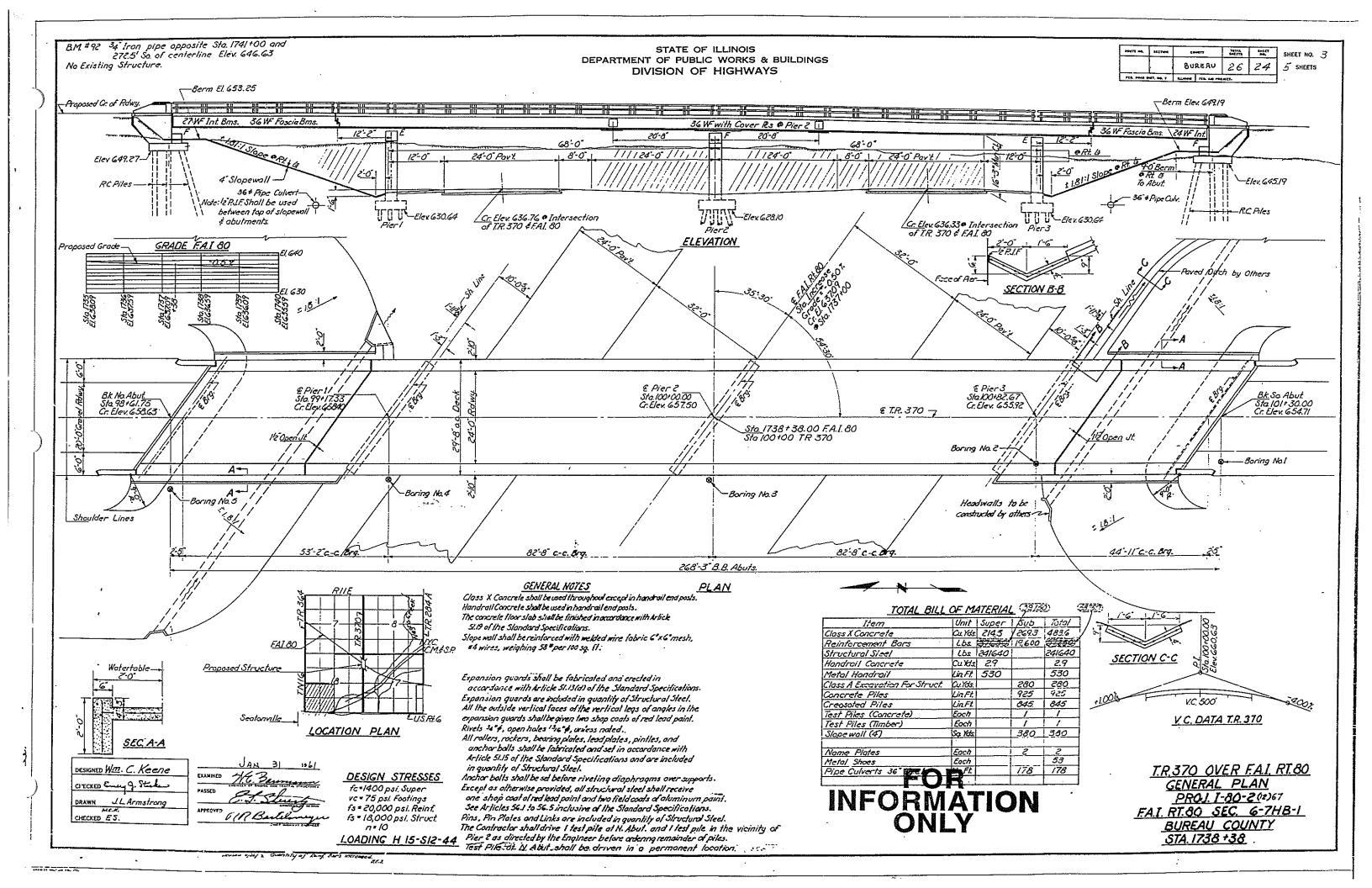
KPS

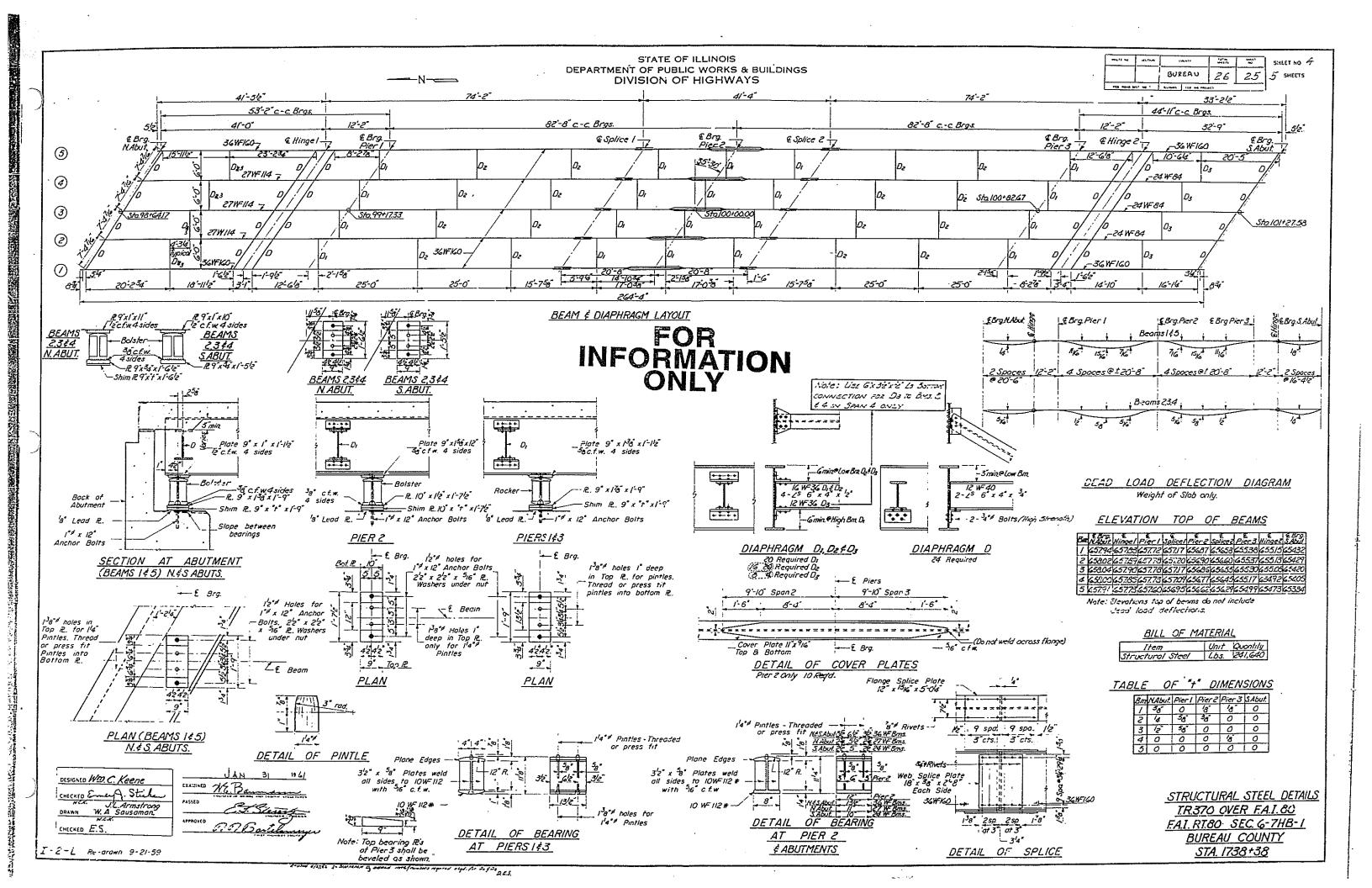
DESIGNED

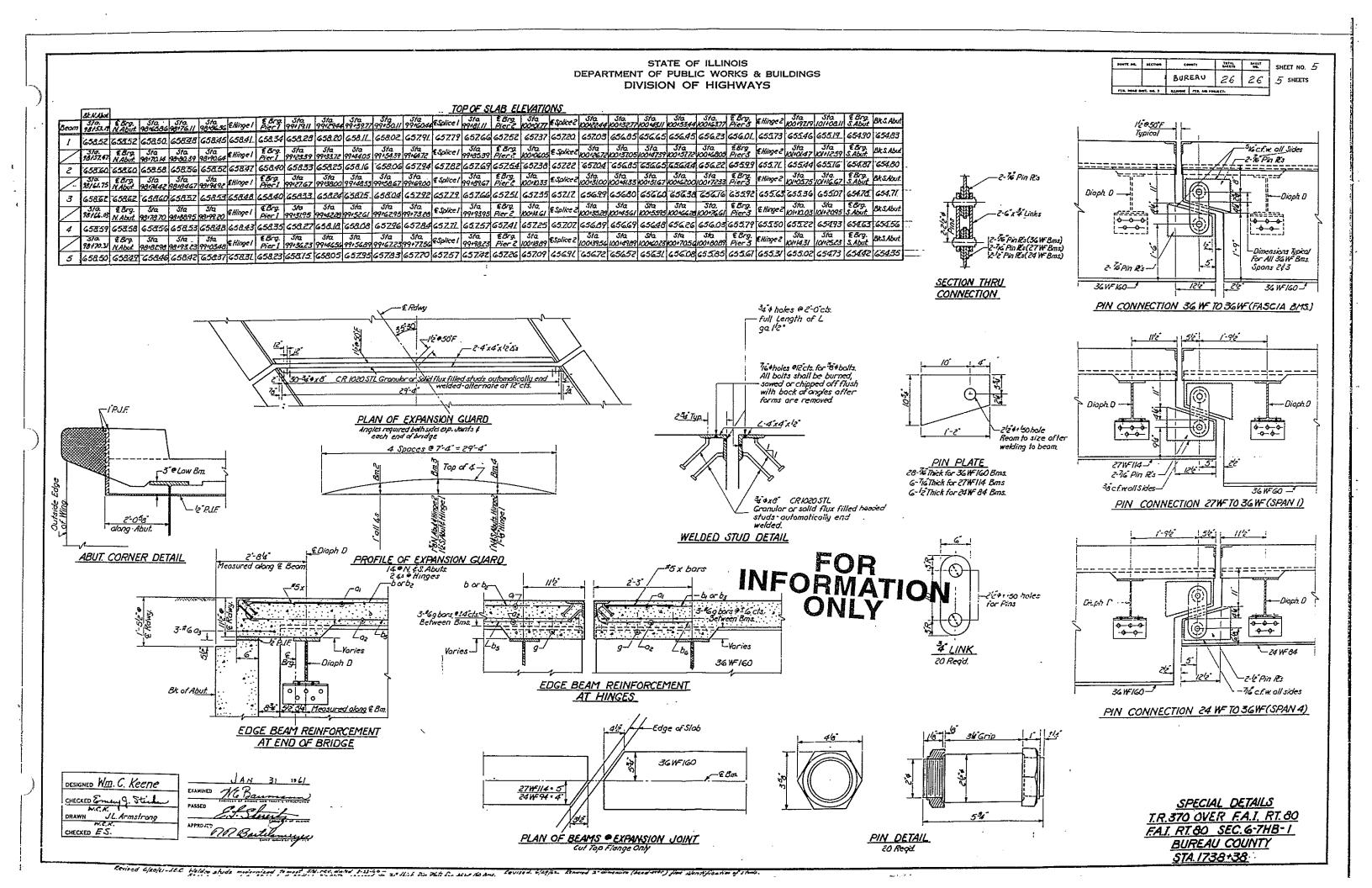
CHECKED NJS

DRAWN Paul Summer

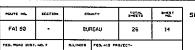
CHECKED KPS NJS



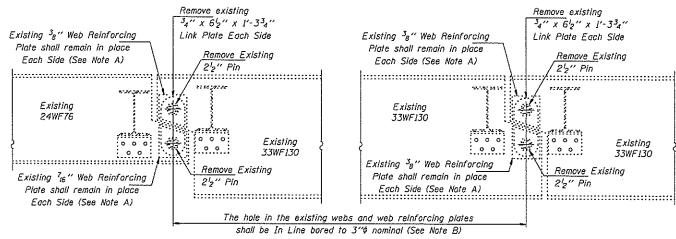




\* D-2 BRIDGE PIN REPLACE 1997-1



SHEET NO. I4 SHEETS



NUT DETAIL

R = 314" (Typ.) Sec 65" LINK PLATE DETAIL

' Woven Teflon Bushings (See Note D) 134" Thread (Typical) (Typ.) 16 X

SECTION THRU PIN

(20 Required)

- <sup>5</sup>a" thick Hex Nuts (Each Side) Nuts shall be ASTM A-576, Grade 12L14, minimum yield of 36 ksi. (See Note E)

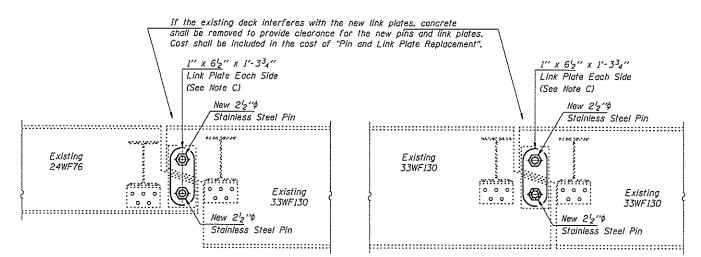
21/2" nominal diameter Pin (diameter tolerances subject to Specifications of Teflon Bushing Manufacturer and shall be approved by the Engineer). Pin shall be ASTM A276, UNS 21800 (Nitronic 60 or equal) (No step at threads) 12 threads per inch. Install prior to new link plates.

Silicone Sealant suitable for Structural Steel (See Note F)

ELEVATION AT EXISTING PIN ASSEMBLY

ELEVATION AT EXISTING PIN ASSEMBLY FOR EXTERIOR BEAMS

Any Pins that can be easily removed without damage to the pin shall be salvaged and the Bridge Engineer shall be contacted for disposition. Cost of salvage is included in "Pin and Link Plate Replacement".



ELEVATION AT NEW PIN ASSEMBLY FOR INTERIOR BEAMS

APRIL 29.

FOR INTERIOR BEAMS

ELEVATION AT NEW PIN ASSEMBLY FOR EXTERIOR BEAMS

### MAXIMUM REACTIONS AT PIN

R₽	(K)	14.3
R4	(K)	25.6
Imp.	(K)	7.7
R (Total)	(K)	47.6

Note A:

Existing welds shall be inspected for cracks using liquid dye penetrant or magnetic particle testing. Any cracks that are found shall be identified and reported to the Bureau of Bridges and Structures for further disposition. Clean and paint before installing new link plates.

Note B:

Bore diameter for bushing in link plate, existing webs and web reinforcement plates shall correspond to bushing manufacturer's allowable tolerances for proper functioning. Hole diameter may be adjusted to allow use of stock bushinas.

Inside face of new link plates shall receive first field coat in shop. The primer shall pass the M.E.K. Rub Test before the first field coat is applied.

Actual bushing thickness per manufacturer's specifications. '4" is approximate. Bushings shall be a self lubricating filament wound epoxy matrix backed Duralon Bearing, metal backed Fiber Glide Bearing or equivalent. No primer or grease shall be allowed on bushings. Bushings shall be suitable for dynamic loads of 20,000 psi.

Tighten inside nuts to bring all bushings into firm contact. then back off 4 turn and tighten outer nuts.

Apply 38" bead to face of the web reinforcing plates approximately 2" from bushing immediately before installing new link plates. Place sealant around nuts after installation. Sealant shall be suitable for prolonged exterior exposure without losing flexibility or adhesion to painted steel surfaces. Proposed products shall be subject to Department's acceptance based on documented testing or other evidence.

## GENERAL NOTES

All new structural steel shall conform to AASHTO Classification M-270 Gr. 36. unless otherwise noted.

The Contractor shall provide support and/or shoring systems for the beam in the area of existing pin and link plate replacement. See Special Provision "Temporary Support System."

The inorganic zinc rich primer/acrylic/acrylic paint system shall be used for shap and field painting of new structural steel except where otherwise noted. The color of the acrylic finish coat shall be Interstate Green, Munsell No. 7.56 4/8. See Special Provisions "Cleaning and Painting New Metal Structures". Cost shall be included in the cost of "Pin and Link Plate Replacement".

Existing Structural steel shall be cleaned and painted as required by the Special Provision "Cleaning and Painting Adjacent Areas of Existing Steel Structures". Cost shall be included in the cost of "Pin and Link Plate Replacement." All existing steel surfaces behind link plates shall be cleaned and primed

before installation of new link plates. Cost shall be included in the cost of "Pin and Link Plate Replacement."

Plan dimensions and details relative to existing structure have been taken from existing plans and are subject to nominal construction variations. It shall be the Contractor's responsibility to verify such dimensions and details in the field, except the pin diameters, and make necessary approved adjustments prior to construction or ordering of materials. Such variations shall not be cause for additional compensation for a change in the scope of the work, however, the Contractor will be paid for the quantity actually furnished at the unit price bid for the work.

The Pins and Link Plates shall conform to the minimum Charpy V-Notch Toughness of 25 ft.-lbs. at 40° F.

The pins, link plates, bushings, nuts and silicone sealant are the items included in "Pin and Link Plate Replacement".

## TOTAL BILL OF MATERIAL

ITEM	UNIT"	QUANTITY
Temporary Support System	Each	10
Pin and Link Plate Replacement	Each	10
Silicone Joint Sealer	Foot	64

PIN REPLACEMENT TR ROUTE 148 SEC. 06-3HB BUREAU COUNTY STA. 640+74.80 STR. No. 006-0123

006 - 0/23

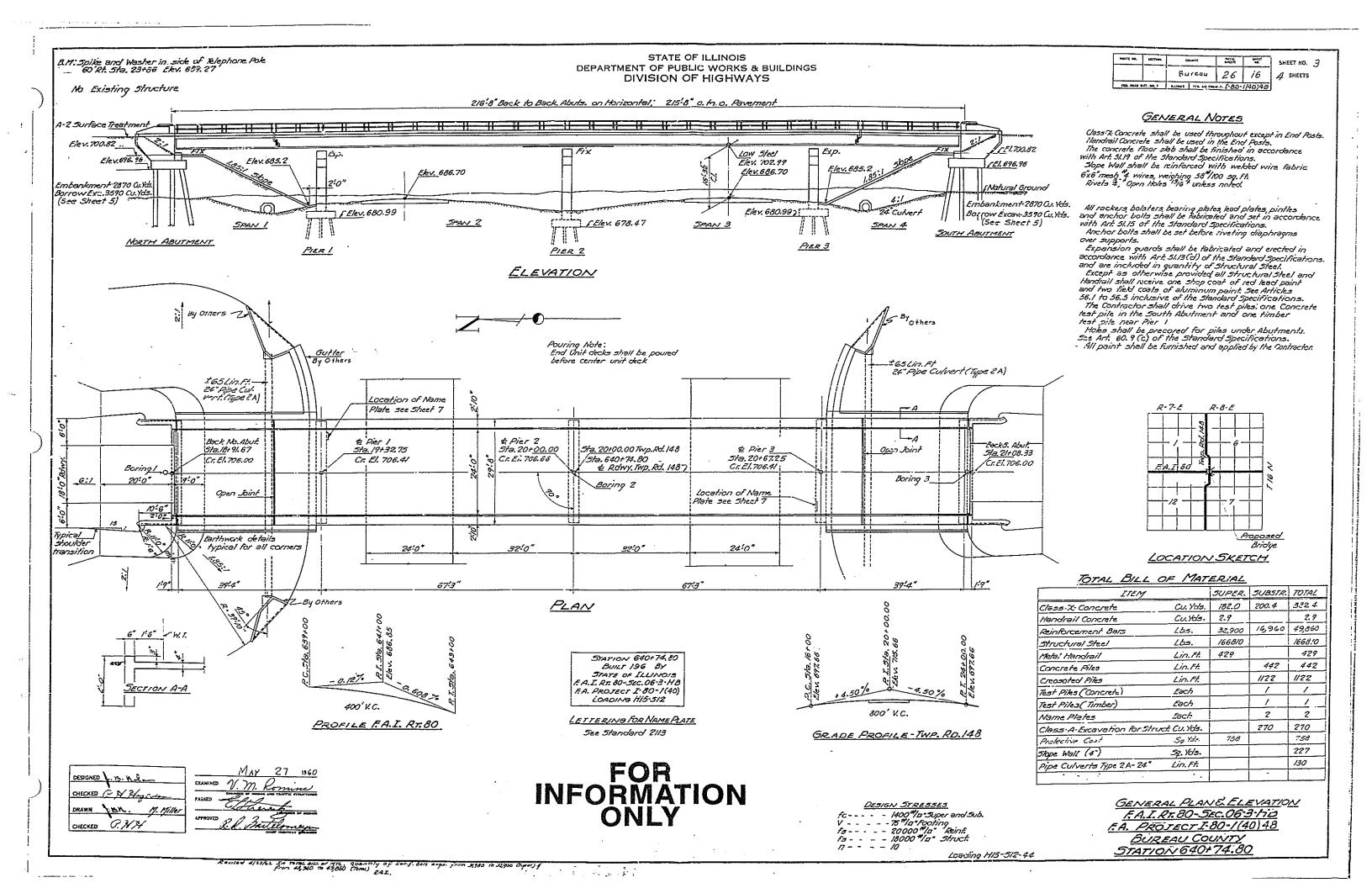
PASSED

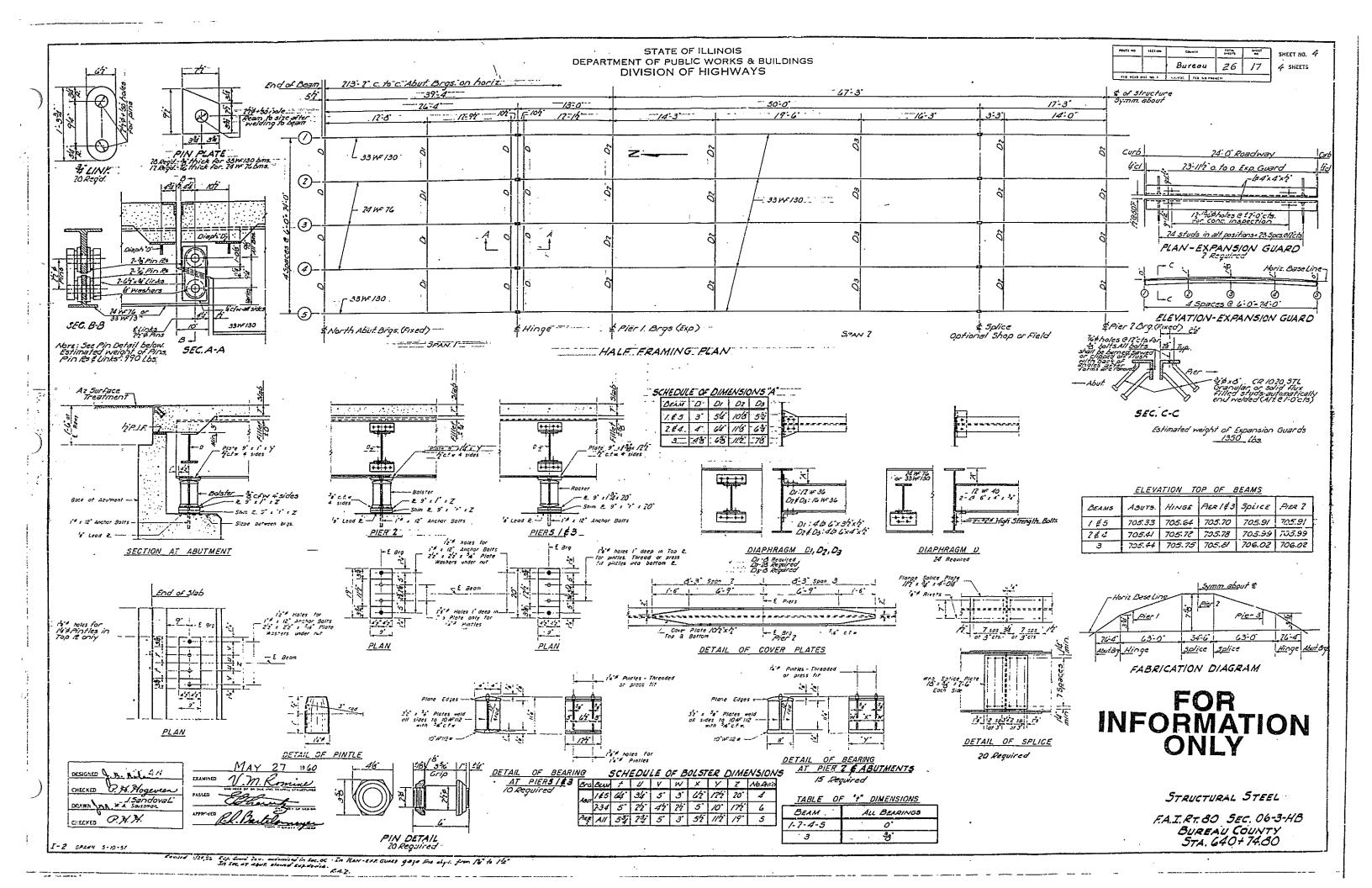
DESIGNED

CHECKED NJS

DRAWN Paul Summer

CHECKED KPS NJS

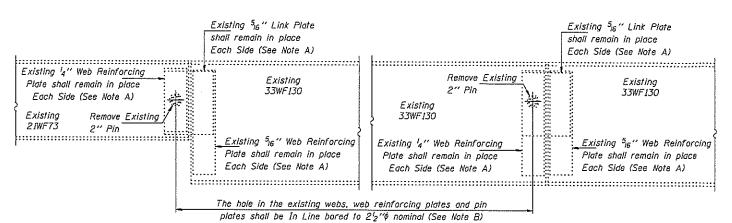




\* D-2 BRIDGE PIN REPLACE 1997-1

county 10171 FAL 60 BUREAU

"SE" SHEET NO. 1 4 SHEETS



'4" Woven Teflon Bushings (See Note C) 134" Thread (Typical) (Typ.) 16)

SECTION THRU PIN

(IO Required)

- <sup>5</sup>a" thick Hex Nuts (Each Side) Nuts shall be ASTM A-576, Grade 12L14, minimum yield of 36 ksi. (See Note D)

2" nominal diameter Pin (diameter tolerances subject to Specifications of Teflon Bushing Manufacturer and shall be approved by the Engineer). Pin shall be ASTM A276, UNS 21800 (Nitronic 60 or equal) (No step at threads) 12 threads per inch.

Silicone Sealant suitable for Structural Steel (See Note E)

# ELEVATION AT EXISTING PIN ASSEMBLY

ELEVATION AT EXISTING PIN ASSEMBLY FOR EXTERIOR BEAMS

Any Pins that can be easily removed without damage to the pin shall be salvaged and the Bridge Engineer shall be contacted for disposition. Cost of salvage is included in "Pin Replacement".

}-----Existing 21WF73 ➅ Existing New 2"d 33WF130 Stainless Steel Pin ..........

-----New 2"4 • Stainless Steel Pil Existina 33WF13Q Existina 33WF130 

ELEVATION AT NEW PIN ASSEMBLY FOR INTERIOR BEAMS

FOR INTERIOR BEAMS

ELEVATION AT NEW PIN ASSEMBLY FOR EXTERIOR BEAMS

Existing welds shall be inspected for cracks using liquid dye penetrant or magnetic particle testing. Any cracks that are found shall be identified and reported to the Bureau of Bridges and Structures for further disposition. Clean and paint before installing

Bore diameter for bushing in existing link plates, webs and web reinforcement plates shall correspond to bushing manufacturer's allowable tolerances for proper functioning. Hole diameter may be adjusted to allow use of stock bushings.

Actual bushing thickness per manufacturer's specifications, 14" is approximate. Bushings shall be a self lubricating filament wound epoxy matrix backed Duralon Bearing, metal backed Fiber Glide Bearing or equivalent. No primer or grease shall be allowed on bushings. Bushings shall be suitable for dynamic loads of 20,000 psi.

Note D:

Tighten inside nuts to bring all bushings into firm contact. then back off 4 turn and tighten outer nuts.

Place sealant around nuts after installation. Sealant shall be suitable for prolonged exterior exposure without losing flexibility or adhesion to painted steel surfaces. Proposed products shall be subject to Department's acceptance based on documented testing or other

## GENERAL NOTES

All new structural steel shall conform to AASHTO Classification M-270 Gr. 36. unless otherwise noted.

The Contractor shall provide support and/or shoring systems for the beam in the area of existing pin replacement. See Special Provision "Temporary Support System."

The inorganic zinc rich primer/acrylic/acrylic paint system shall be used for shop and field painting of new structural steel except where otherwise noted. The color of the acrylic finish coat shall be Interstate Green, Munsell No. 7.5G 4/8. See Special Provisions "Cleaning and Painting New Metal Structures". Cost shall be included in the cost of "Pin Replacement".

Existing Structural steel shall be cleaned and painted as required by the Special Provision "Cleaning and Painting Adjacent Areas of Existing Steel Structures". Cost shall be included in the cost of "Pin Replacement,"

Plan dimensions and details relative to existing structure have been taken from existing plans and are subject to nominal construction variations. It shall be the Contractor's responsibility to verify such dimensions and details in the field, except the pin diameters, and make necessary approved adjustments prior to construction or ordering of materials. Such variations shall not be cause for additional compensation for a change in the scope of the work, however, the Contractor will be paid for the quantity actually furnished at the unit price bid for the work.

The Pins shall conform to the minimum Charpy V-Notch Toughness of 25 ft.-lbs. at 40° F.

The pins, bushings, nuts and silicone sealant are the items included in "Pin Replacement".

## TOTAL BILL OF MATERIAL

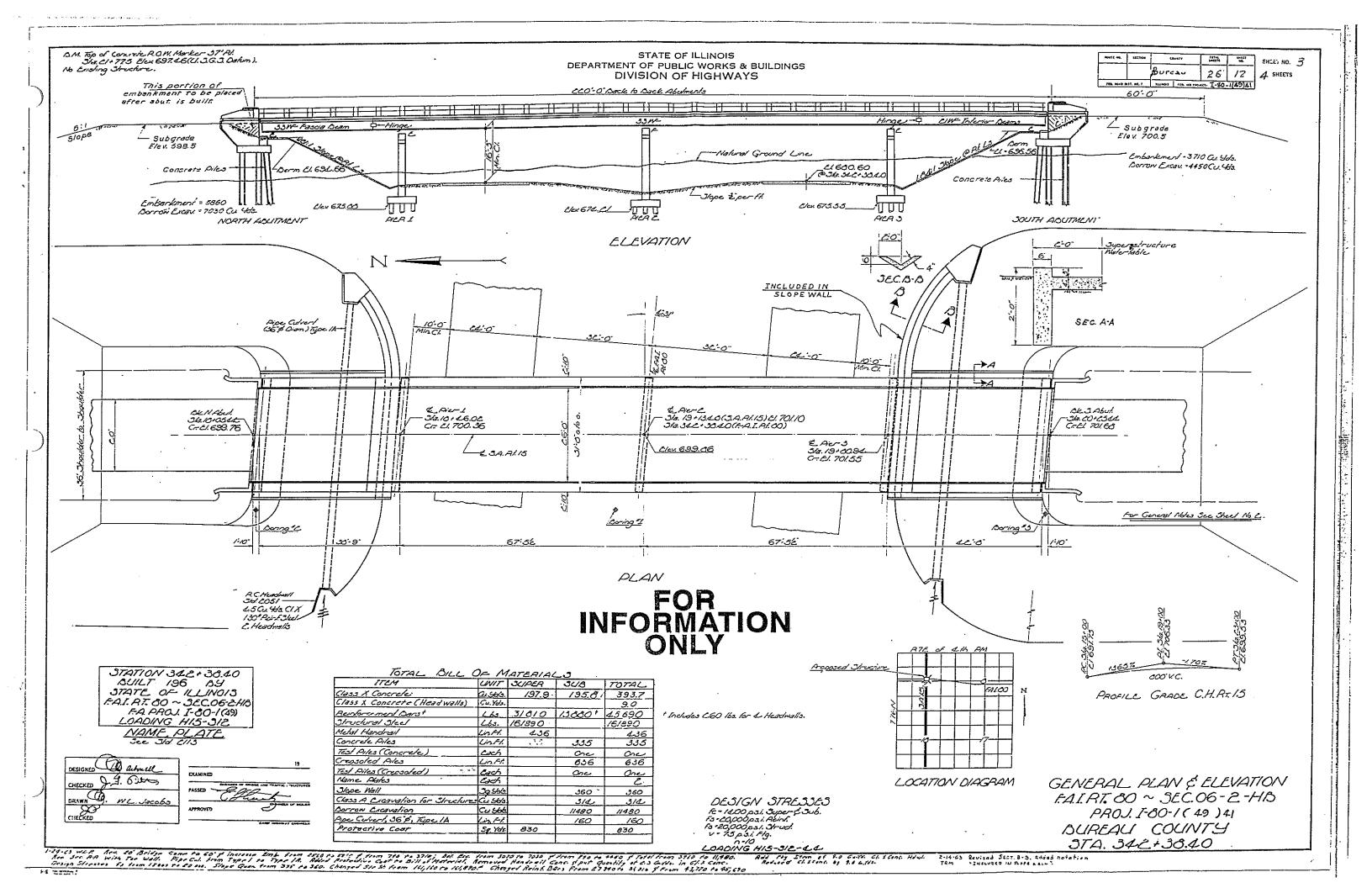
ITEM	UNIT	QUANTITY
Temporary Support System	Each	10
Pin Replacement	Each	10
Silicone Joint Sealer	Foot	68

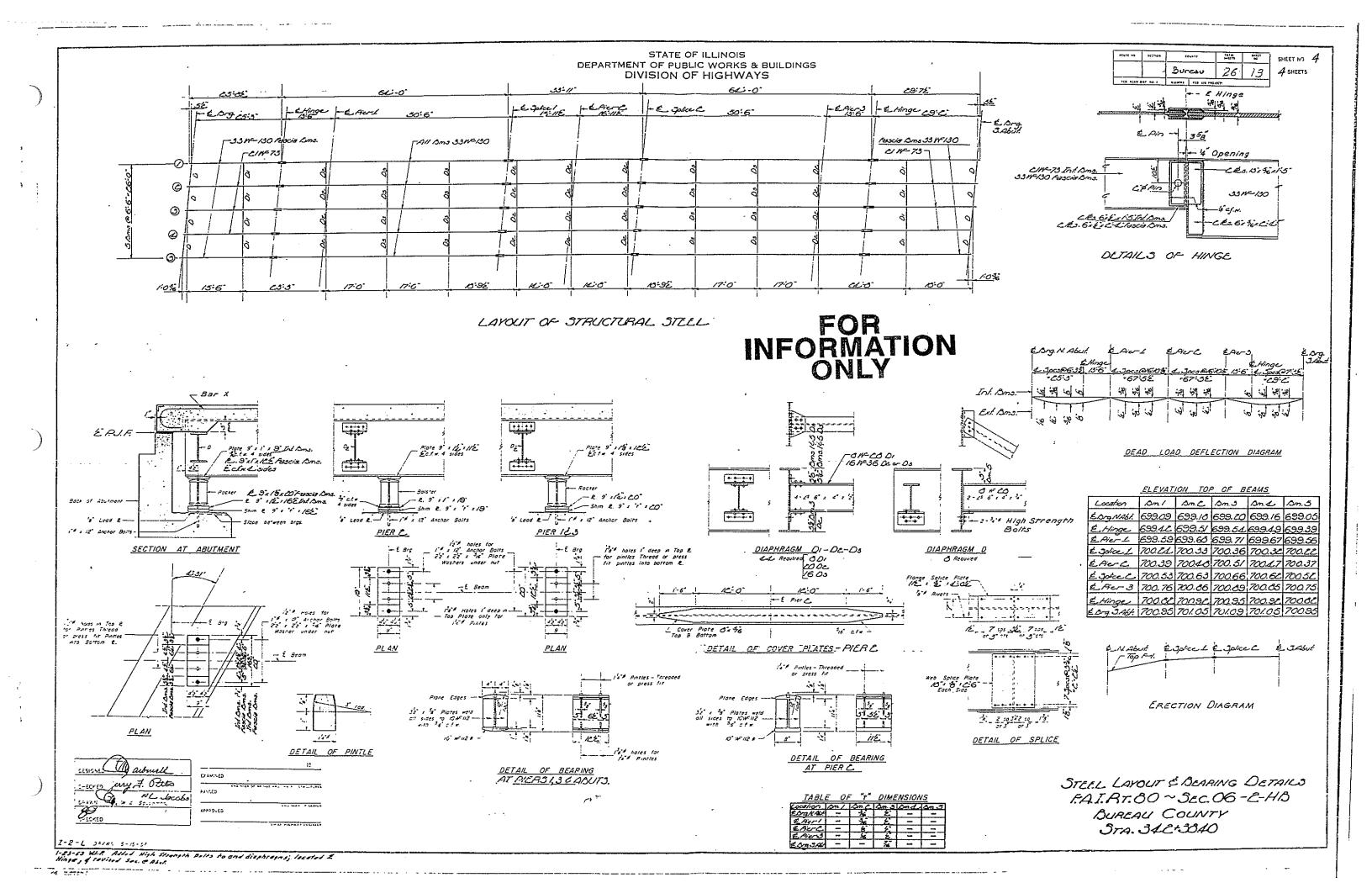
PIN REPLACEMENT FAS 1248 SEC. 06-2HB BUREAU COUNTY STA. 342+38.40 STR. No. 006-0117

# MAXIMUM REACTIONS AT PIN

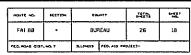
RQ	(K)	16.0	1
RŁ	(K)	21.7	l
Imp.	(K)	6.5	l
R (Total)	(K)	44.1	l

KPS APRIL 29. DESIGNED EXAMINED - Total CHECKED NJS PASSED DRAWN Paul Summer CHECKED KPS NJS

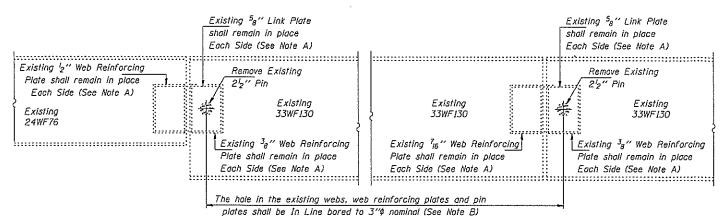




\* D-2 BRIDGE PIN REPLACE 1997-1



SHEET NO.  ${\cal I}$ 



NUT DETAIL

NUT DETAIL (40 Required)

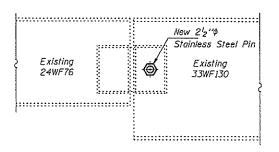
14" Woven Teflon Bushings (See Note C) 58" thick Hex Nuts (Each Side) Nuts shall be ASTM A-576, Grade 12L14, minimum yield of 36 ksi. (See Note D) 1<sup>3</sup><sub>4</sub>" Thread (Typical) 2<sup>1</sup>2" nominal diameter Pin (diameter tolerances (Typ.) 16> subject to Specifications of Teflon Bushing Manufacturer and shall be approved by the Engineer). Pin shall be ASTM A276, UNS 21800 (Nitronic 60 or equal) (No step at threads) 12 threads per inch. Silicone Sealant suitable for Structural Steel (See Note E)

SECTION THRU PIN
(IO Required)

# ELEVATION AT EXISTING PIN ASSEMBLY FOR INTERIOR BEAMS

ELEVATION AT EXISTING PIN ASSEMBLY
FOR EXTERIOR BEAMS

Any Pins that can be easily removed without damage to the pin shall be salvaged and the Bridge Engineer shall be contacted for disposition. Cost of salvage is included in "Pin Replacement".



New 2½"\$
Stainless Steel Pin

Existing

33WF130

New 2½"\$
Stainless Steel Pin

33WF130

ELEVATION AT NEW PIN ASSEMBLY
FOR INTERIOR BEAMS

APRII 29.

EXAMINED Jose C. AB.

ELEVATION AT NEW PIN ASSEMBLY
FOR EXTERIOR BEAMS

Note A:

Existing welds shall be inspected for cracks using liquid dye penetrant or magnetic particle testing. Any cracks that are found shall be identified and reported to the Bureau of Bridges and Structures for further disposition. Clean and paint before installing new pins.

Note

Bore diameter for bushing in existing link plates, webs and web reinforcement plates shall correspond to bushing manufacturer's allowable tolerances for proper functioning. Hole diameter may be adjusted to allow use of stock bushings.

Note (

Actual bushing thickness per manufacturer's specifications,  $^{1}\!_{4}$ '' is approximate. Bushings shall be a self lubricating filament wound epoxy matrix backed Duralon Bearing, metal backed Fiber Glide Bearing or equivalent. No primer or grease shall be allowed on bushings. Bushings shall be suitable for dynamic loads of 20,000 psi.

Note O

Tighten inside nuts to bring all bushings into firm contact, then back off <sup>1</sup>4 turn and tighten outer nuts.

Note i

Place sealant around nuts after installation. Sealant shall be suitable for prolonged exterior exposure without losing flexibility or adhesion to painted steel surfaces. Proposed products shall be subject to Department's acceptance based on documented testing or other evidence.

# GENERAL NOTES

All new structural steel shall conform to AASHTO Classification M-270 Gr. 36. unless otherwise noted.

The Contractor shall provide support and/or shoring systems for the beam in the area of existing pin replacement. See Special Provision "Temporary Support System."

The inorganic zinc rich primer/acrylic/acrylic paint system shall be used for shop and field painting of new structural steel except where otherwise noted. The color of the acrylic finish coat shall be Interstate Green, Munsell No. 7.56 4/8. See Special Provisions "Cleaning and Painting New Metal Structures". Cost shall be Included in the cost of "Pin Replacement".

Existing Structural steel shall be cleaned and painted as required by the Special Provision "Cleaning and Painting Adjacent Areas of Existing Steel Structures". Cost shall be included in the cost of "Pin Replacement."

Plan dimensions and details relative to existing structure have been taken from existing plans and are subject to nominal construction variations. It shall be the Contractor's responsibility to verify such dimensions and details in the field, except the pin diameters, and make necessary approved adjustments prior to construction or ordering of materials. Such variations shall not be cause for additional compensation for a change in the scope of the work, however, the Contractor will be paid for the quantity actually furnished at the unit price bid for the work.

The Pins shall conform to the minimum Charpy V-Notch Toughness of 25 ft.-lbs. at 40° F.

The pins, bushings, nuts and silicone sealant are the items included in "Pin Replacement".

# Silicone Joint S

ITEM	UNIT	QUANTITY
Temporary Support System	Each	10
Pin Replacement	Each	10
Silicone Joint Sealer	Foot	68

TOTAL BILL OF MATERIAL

<u>PIN REPLACEMENT</u>

<u>FAS 188 SEC. 06-3HB-1</u>

<u>BUREAU COUNTY</u>

<u>STA. 745+74.52</u>

STR. No. 006-0112

# MAXIMUM REACTIONS AT PIN

R₽	(K)	15.1
R4	(K)	27.7
Imp.	(K)	8.3
R (Total)	(K)	51.1

CRAWN Paul Summer PASSED

CHECKED KPS NJS

Displeas of Bridge:

KPS

DESIGNED

CHECKED NJS

006-01/2

8. M. spike and washer in side of Telephone Pole 32' Lt. Sta. Z41490 EA.T. 80-1 Elev. 660.31 (U.S. 6.5. Datum) STATE OF ILLINOIS SHEETS NO. 3 DEPARTMENT OF PUBLIC WORKS & BUILDINGS BUREAU 26 20 NO Existing Structure DIVISION OF HIGHWAYS 4 SHEETS 168. 8040 0157. NO. 7 ILLINOIS | FEB. AID PROXECT. I-80-2(7)50 216 8 Back to Back Abutments Two Bent Plate Rail 33" W 130 33 W 130 Facia Beam 24 W & Interior Beam Elev. 672.20 15-3" \ Expi-3" 1- 24-0° 32-0 32-0 11-5 PEXP. 13-3. 3 Elev. 657.93 Elev. 657.93 Te R. Name R. Elev. GG8. 32 Elev. 668.32 Natural Ground Class. X. Concrete shall be used throughout except in transfail and Posts.

Handrail Concrete shall be used in transfail and Posts.

The Concrete shall be used in transfail and Posts.

The Concrete shall be used in transfail and Posts.

The Concrete shall be used in transfail and Posts.

The Concrete from slow shall be finished in accordance with Art 5119 of the Shandard Specifications.

Jope Wall shall be reinforced with Wolding as per 100 sq. ft.

All rockers bearing plates, lead plates pintles and anchor buths shall be labricated and set in accordance with Art 5115 of the shandard specifications, and are included in quantity of Structural steel 5st Wit: 6740 disphayms over supports.

Expansion Guards shall be fabricated and exceled in accordance with Art 5116 for Invetting disphayms over supports.

Expansion Guards shall be fabricated and exceled in accordance with Art 5116 for the Shandard Specifications.

Expansion Guards are included in quantity of Structural Steel 5th Weight 2200 ##

Except as otherwise provided all structural Steel shall fective one shop coat of feel lad paint and two field Coats of aluminum paint.

See Art 56.1 to 56.5 inclusive of the Shandard Specifications.

All paint shall be furnished and applied by the Contractor. The Contractor shall drive two test places as directed by the Expanser before ordering ramaineer of Place.

One timber test pile in a permanent beatron)

at South Abutment.

All Structural Steel shall conform to the A.S.I.M Spec. A.S.C.

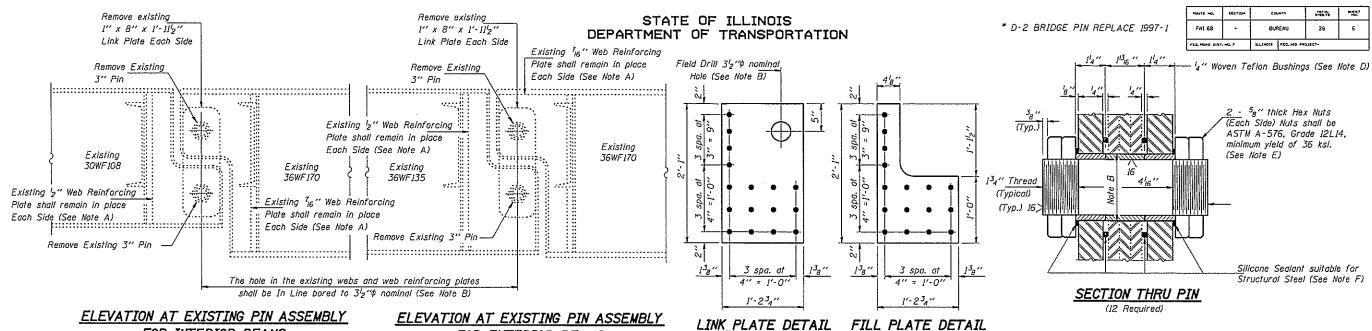
Rivets 344, Open Holes Steel Stall conform to the see of the Stall Stall. GENERAL NOTES n f Elev. 652.30 Elev. 652.30 Concrete piles Elev. 656.18 Elex. 656.18-24 Culveri Elev. 649.927. 7 7 -Creosoted Piles ( PIER ! PIER 3 NORTH ABUTMENT PIER 2 SOUTH ABUTMENT **FOR** ELEVATION INFORMATION ONLY Scale 32 = 1-0 Class X concrete for headwalls (4.6 cu yd) and reinforcement (140°) included with the totals for substructure. Paved Ditch Paved Ditch Back No. Aburt # Pier / <u>\$ Pier 3</u> | Station 20+69.08 | Cr. Elev. G77.GG Back So. Abut. Station 18+93.50 Cr. Elev. G77.43 Station 20+01.83 Cr. Elev. G77.81 Station 19+34.58 Cr. Elev. G77.GG Rivets 3, 4, Open Holes 13,6 & Unless noted. Enring 2 Layout of paved ditch may be varied to suit ground conditions in the field as directed by the Engineer. Quantity of paved ditch is included with supervall. ΓNam R. Abutment Piles shall be precored thru embankment in accordance with article 60.9(c) of the Standard Specifications.

All the outside vertical faces of the vertical legs of angles in the expansion goard shall be given two stop coals of red lead paint. 1º open Joint Station 20+01.83 S.A.Rt. 8 B Station 745+74.52. FA.I.Rt. 80 £ Pin -Face of Piers 1 or 3 Sta 19+21.33 Cr. Elev. GTT.59 \$ Roadway SECTION BB € Pin 26-0 Sta. 20 + 82.23 Cr. Elev. 677.59 2-0 26:0 1:6" Superstructure City . - Shoulder Line 50 24:0 SEC. A.A 67:3° C-C Brg. 67:3" C.- C. Brg. 39:3" C.- C. Brg. PLAN TOTAL BILL OF MATERIAL UNIT SUPER. SUBSTR. TOTAL RBE of the 4th P.M Cu. 165. 188.5. 204.3. -392.8 Class-X- Concrete Cu. Yels. 2.3 : 2.3 Las. 31990 14530 465520 Handrail Concrete Reinforcement Bars Structural Steel 465. 163,070 163070 STATION 745+74.52 Name Plates Each BUILT 19 BY Metal Handrail Lin. Ft. 430 430 920' V.C. F.A. I. RT. 80- SEC. 06-3HB-1 Class · A · Excav. For Structures Cuttle 107 107 SECTION C.C PROJ. 1-80-11 ) I-80-2(7)50 Slope Wall 4" 440 440 59.76/3. GRADE PROFILE-5.A. RT. 8 LOADING HIS-512 544 544 Concrete Piles Lin. F. Test Piles (Concrete) Each . / 1 Name Plate Lettering -0.70% Creasated Piles Lin.Ft 6.30 630 . Jee Std. 2113 Test Piles (Timber) Each 1 1 Sta. 658.2 For Location see . Sta. 770 152 Pipe Culvert Type 2-24" Lin Ft. SEPT. 22 Elex. 661.95 DESIGNED J. M. Jamoth Sheet 7 of 9 Proposed Structure Elev. 640.95 EXAM'NED TO BOOK AND TRAINED BLOCK CHECKED R.A. Beausan GRADE PROFILE F.A.I. RT. 80 LOCATION SKETCH DRAWN J.A.J JR M. Miller GENERAL PLAN & ELEVATION DESIGN STRESSES - 1400 % = 5 CHECKED R.O.P. Super & Sub. PROJ I-80-2(7)50 F. A.I. RT. 80-5EC.06-3118-1 BUREAU COUNTY STATION 745+74.52 Loading H15-512-44 Revised 6-27-63 H.P.G. Project Number Revised in Name Plate Lettering Revised 1-3-G1 J.M.J. Change Clearance from 15'; O" to 1G'-3" Changed all Cr. Elev. and revised Total Bill of Material. 1844 12/41/61: In ELLIATION TEMPORE Combination bornel of N. Abut Emb 1680 Borney 3120, So. Abut Emb. 1860, Borney Abit) and 187 in between Steph Abut and Abut Cop in Play Tomoring Alatina To Steph Abut Order in GANEAR Notes and note for A-K Stock in 18/10. Bit of MATERIA Notes and note for A-K Stock in 18/10. Bit of MATERIA Notes and note for A-K Stock in 18/10.

we't'

SHEET NO. 3

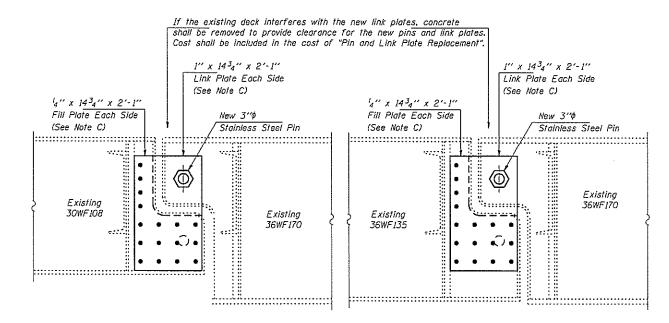
6 SHEETS



ELEVATION AT EXISTING PIN ASSEMBLY FOR INTERIOR BEAMS

ELEVATION AT EXISTING PIN ASSEMBLY FOR EXTERIOR BEAMS

Any Pins that can be easily removed without damage to the pin shall be salvaged and the Bridge Engineer shall be contacted for disposition. Cost of salvage is included in "Pin and Link Plate Replacement".



ELEVATION AT NEW PIN ASSEMBLY FOR INTERIOR BEAMS

APRIL 29.

ELEVATION AT NEW PIN ASSEMBLY FOR EXTERIOR BEAMS

# MAXIMUM REACTIONS AT PIN

_			··· · · · ·	<u> </u>
1	R₽	(K)	22.0	1
	RŁ.	(K)	<i>31.9</i>	1
	Imp.	(K)	9.6	1
	R (Total)	(K)	63.4	1



NUT DETAIL

(24 Required)

Existing welds shall be inspected for cracks using liquid dye penetrant or magnetic particle testing. Any cracks that are found shall be identified and reported to the Bureau of Bridges and Structures for further disposition. Clean and paint before installing new link plates.

Note B:

Bore diameter for bushing in link plate, existing webs and web reinforcement plates shall correspond to bushing manufacturer's allowable tolerances for proper functioning. Hole diameter may be adjusted to allow use of stock bushings.

Inside face of new link plates shall receive first field coat in shop. The primer shall pass the M.E.K. Rub Test before the first field coat is applied.

Actual bushing thickness per manufacturer's specifications, wound epoxy matrix backed Duralon Bearing, metal backed Fiber Glide Bearing or equivalent. No primer or grease shall be allowed on bushings. Bushings shall be suitable for dynamic loads of 20,000 psi.

Tighten inside nuts to bring all bushings into firm contact, then back off 4 turn and tighten outer nuts.

Note F:

Apply 3g" bead to face of the web reinforcing plates approximately '2" from bushing immediately before installing new link plates. Place sealant around nuts after installation. Sealant shall be suitable for prolonged exterior exposure without losing flexibility or adhesion to painted steel surfaces. Proposed products shall be subject to Department's acceptance based on documented testing or other evidence.

# GENERAL NOTES

All new structual steel shall conform to AASHTO Classification M-270 Gr. 36. unless otherwise noted.

All new fasteners shall be high strength bolts. Holes shall be subpunched or subdrilled  $^{ij}_{i5}$ " $\phi$  and reamed in the field to  $^{i3}_{i6}$ " $\phi$  for  $^{3}_{4}$ " $\phi$  high strength bolts unless otherwise noted after structural steel sections are properly fitted into position.

The Contractor shall provide support and/or shoring systems for the beam in the area of existing pin and link plate replacement. See Special Provisions for "Temporary Support System."

The inorganic zinc rich primer/acrylic/acrylic paint system shall be used for shop and field painting of new structural steel except where otherwise noted. The color of the acrylic finish coat shall be Interstate Green, Munsell No. 7.5G 4/8. See Special Provisions "Cleaning and Painting New Metal Structures". Cost shall be included in the cost of "Pin and Link Plate Replacement".

Existing Structural steel shall be cleaned and painted as required by the Special Provision "Cleaning and Painting Adjacent Areas of Existing Steel Structures". Cost shall be included in the cost of "Pin and Link Plate Replacement."

All existing steel surfaces behind link plates shall be cleaned and primed before installation of new link plates. Cost shall be included in the cost of "Pin and Link Plate Replacement."

Plan dimensions and details relative to existing structure have been taken from existing plans and are subject to nominal construction variations. It shall be the Contractor's responsibility to verify such dimensions and details in the field, except the pin diameters, and make necessary approved adjustments prior to construction or ordering of materials. Such variations shall not be cause for additional compensation for a change in the scope of the work, however, the Contractor will be paid for the quantity actually furnished at the unit price bid for the work.

The Pins and Link Plates shall conform to the minimum Charpy V-Notch Toughness of 25 ft.-ibs. at 40° F.

The pins, link plates, fill plates, bushings, nuts, silicone sealant and high strength bolts are the items included in "Pin and Link Plate Replacement".

## BILL OF MATERIAL

ITEM	UNIT	<b>QUANTITY</b>
Temporary Support System	Each	12
Pin and Link Plate Replacement	Each	12

PIN AND LINK PLATE REPLACEMENT F.A.I. RT. 80 SEC. 06-2HB-1 BUREAU COUNTY STA, 475+09.54 STR. No. 006-0089

006-0089

EXAMINED

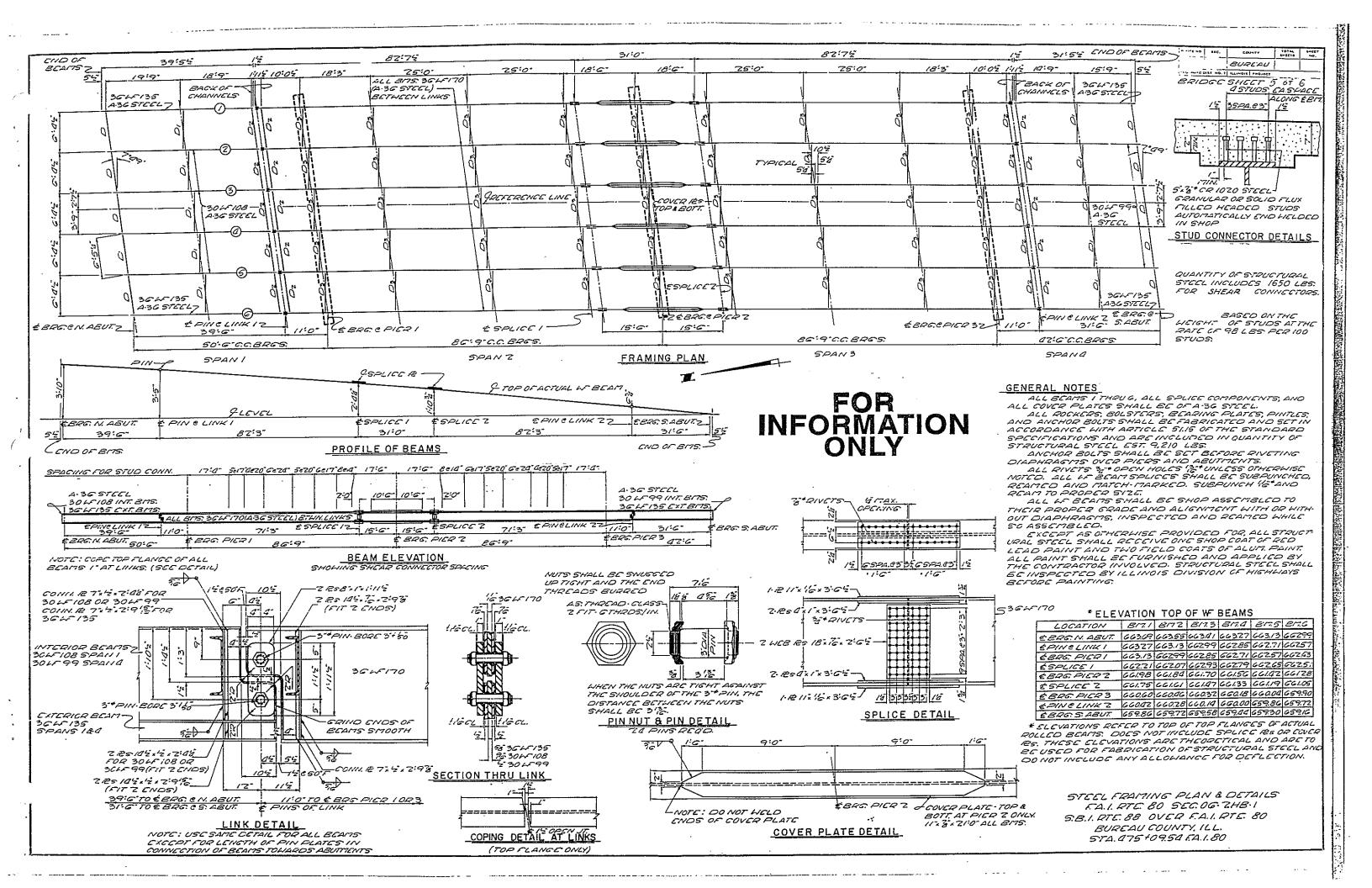
PASSED

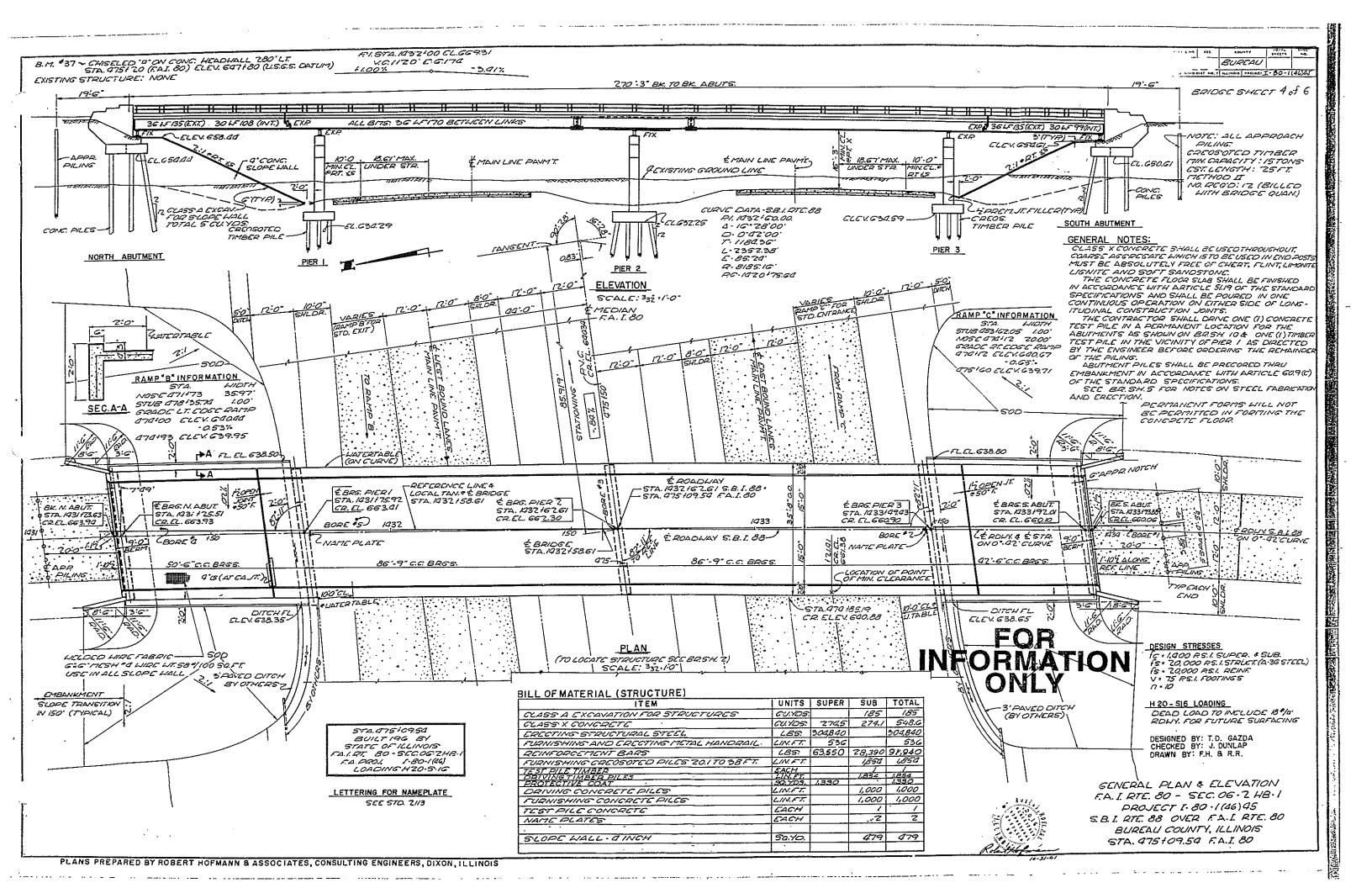
DESIGNED KPS

DRAWN Paul Summer

CHECKED KPS NJS

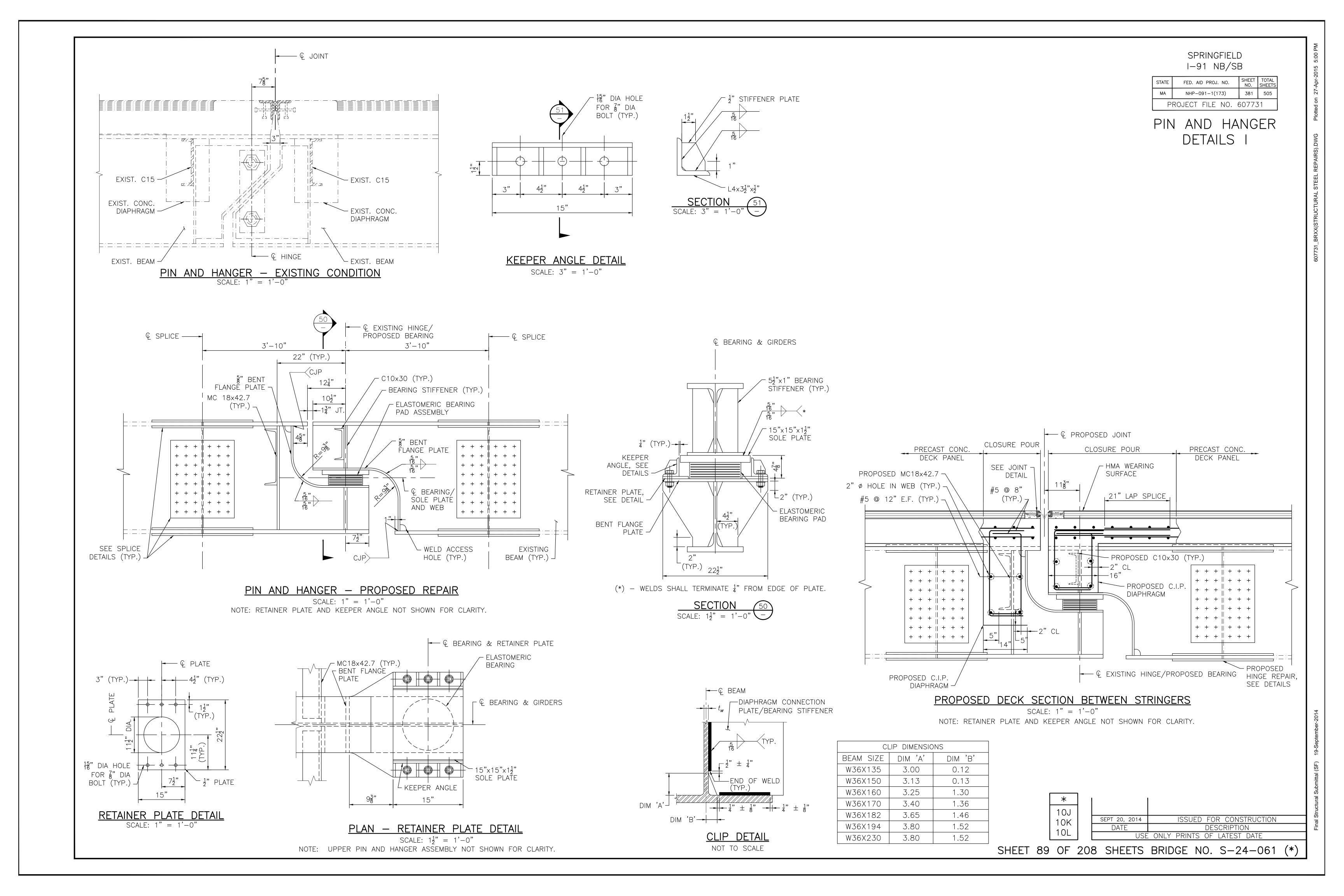
NJS





# Massachusetts Department of Transportation

Design drawings – ship lap joint assembly.







# Michigan Department of Transportation

Design drawings - Pin and hanger assembly replacement.

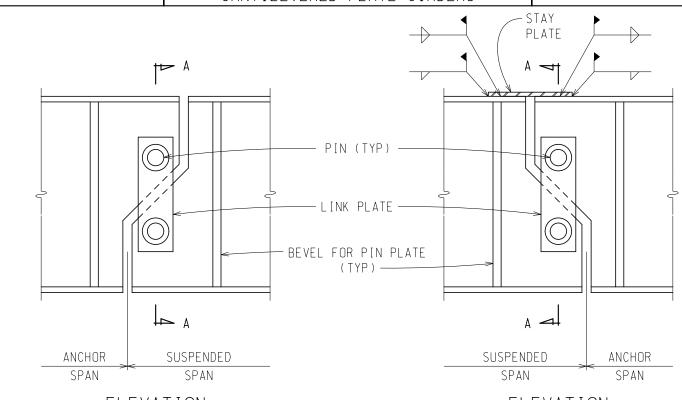
DRAWN BY: BLT CHECKED BY: VZ

APPROVED BY: DAJ

MICHIGAN DEPARTMENT OF TRANSPORTATION BUREAU OF HIGHWAY DEVELOPMENT

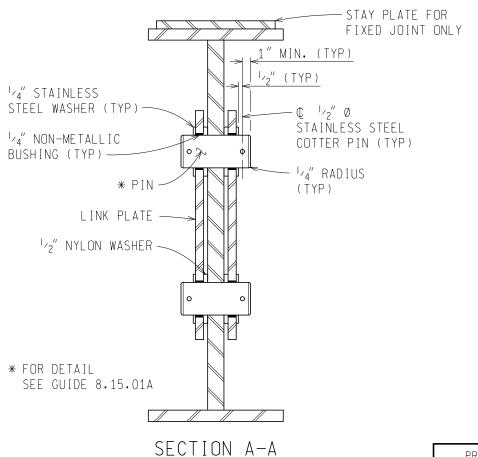
SUSPENDER DETAILS FOR CANTILEVERED PLATE GIRDERS

ISSUED: 06/25/12 SUPERSEDES:05/04/06



ELEVATION EXPANSION JOINT

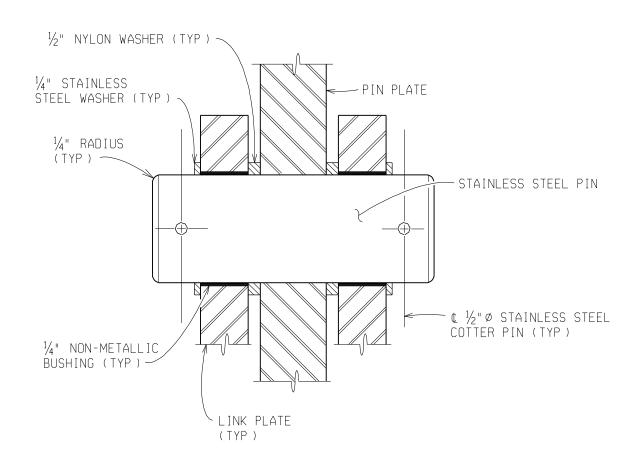
ELEVATION FIXED JOINT



PREPARED BY DESIGN DIVISION

8.15.01

DRAWN BY:	BLT	MICHIGAN DEPARTMENT OF TRANSPORTATION BUREAU OF HIGHWAY DEVELOPMENT	ISSUED:	05/04/06
CHECKED BY:	٧Z		SUPERSEDES:	:11/27/01
APPROVED BY:	1	PIN DETAIL		



# PIN DETAIL

NOTF:

SEE GUIDE 8.16.02 FOR WASHER DETAILS.

DRAWN BY: BLT CHECKED BY: VZ

APPROVED BY:

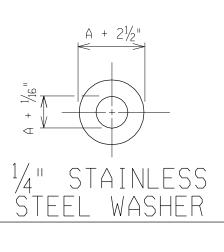
MICHIGAN DEPARTMENT OF TRANSPORTATION BUREAU OF HIGHWAY DEVELOPMENT

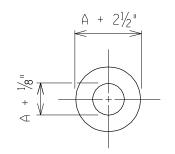
> SUSPENDER DETAILS FOR ROLLED BEAMS

ISSUED:

05/04/06

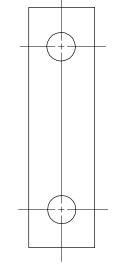
SUPERSEDES: 11/27/01

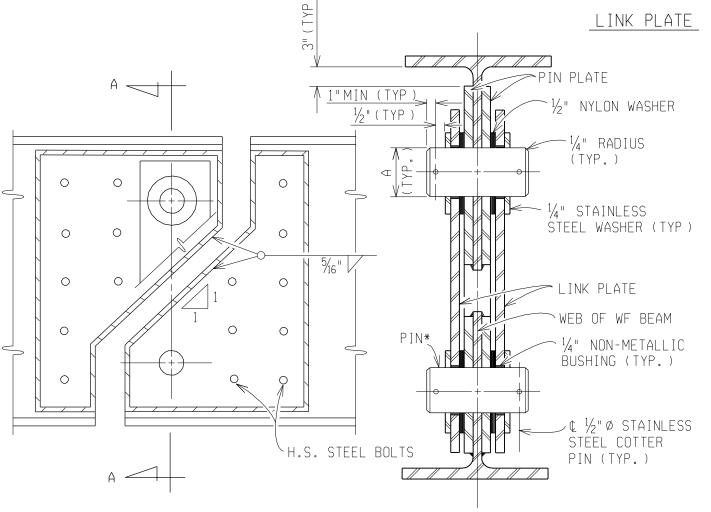




# 1/2" NYLON WASHER

INCLUDED IN THE BID ITEM "STRUCTURAL STEEL, \_\_\_\_, FURN AND FAB."





WELDED PIN PLATES

SECTION A-A \*FOR DETAIL SEE 8.15.01A

NOTE:

SPACING OF THE H.S. STEEL BOLTS SHALL BE ACCORDING TO THE CURRENT AASHTO SPECIFICATIONS.

PREPARED BY
DESIGN SUPPORT AREA

8.16.02

# Oklahoma Department of Transportation

Design drawings - catcher beam system.

DESIGN DATA

ADT 198 ADT 200 DHV

SCALES

D -T(% OF ADT) -V -

PLAN I' PROFILE HOR. I' VER. I' LAYOUT MAP I' -

CONVENTIONAL SYMBOLS

RAILROADS ---- RANGE & TOWNSHIP ---- SECTION LINES ----- QUARTER SECTION LINES

FENCES
GROUND LINE ===== EXISTING ROADS BASE LINE GRADE LINES

POWER LINES

OII WELLS

RIGHT-OF-WAY FENCE

BUILDINGS TET DRAINAGE STRUCTURES-IN PLACE DRAINAGE STRUCTURES-NEW PRES. R/W2 RIGHT-OF-WAY LINES-EXISTING R/W RIGHT-OF-WAY LINES-NEW

◑

PROPOSED ROADS

TELEPHONE & TELEGRAPH

RIGHT-OF-WAY MARKERS-IN PLACE RIGHT-OF-WAY MARKERS-REMOVE & RESET

1988 OKLAHOMA STANDARD SPECIFICATIONS FOR HIGHWAY CONSTRUCTION GOVERN APPROVED BY THE DEPARTMENT OF TRANSPORTATION, FEDERAL HIGHWAY ADMINISTRATION JANUARY 3, 1989.
SPECIAL PROVISIONS GOVERN OVER STANDARD SPECIFICATIONS.

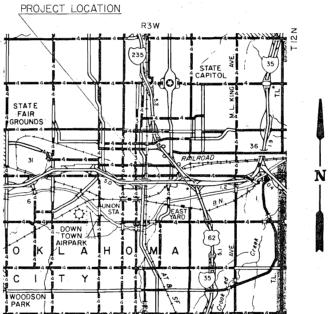
RIGHT-OF-WAY MARKERS-NEW

STATE OF OKLAHOMA DEPARTMENT OF TRANSPORTATION

STATE AID PROJECT NO. E-SAP-55(595)

STATE JOB NO. 11246 (05) CONTROL SECTION NO. 55-69

# OKLAHOMA COUNTY



# REPAIR & MODIFY EXPANSION

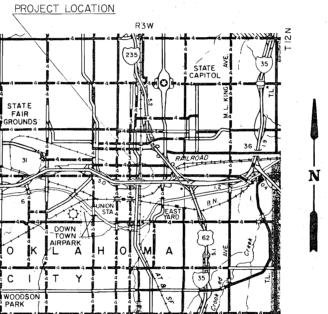
EXCEPTIONS: NONE

PLAN OF PROPOSED

# STATE HIGHWAY

FEDERAL HIGHWAY NO. I-40

NBIS 550690805



# **PIERS**

ROADWAY LENGTH BRIDGE LENGTH PROJECT LENGTH_	0.000	FT.	
EQUATIONS: NONE			

DESCRIPTION RE
ADDED SHEETS DATE 11-16-89 ADDED SHEET 1-29-90

## INDEX OF SHEETS

- 1. TITLE SHEET
- 2. GENERAL NOTES
- 3. SUMMARY OF PAY DUANTITIES (BRIDGE & TRAFFIC) AND GENERAL NOTES (TRAFFIC)
- 4. JACKING LOCATIONS AND FALSEWORK
- 5. DETAILS OF BRIDGE REPAIRS 6. BEARING REPLACEMENT AT
- PIERS 78, 81, & 8 RAMP 22
- 7. COLUMN REPAIR DETAILS
- 8. COLUMN CAP DETAILS 9. PIER MODIFICATION
- 10-11. DETAIL OF BEARING SUPPORT BRACKET
- 12. MISCELLANEOUS DETAIL 13. DETAILS OF CROSSFRAME AND
- HANGER CONNECTION 13-A DETAILS OF CROSSFRAME AND
- HANGER CONNECTION 14. LOCATION OF CONSTRUCTION
- AND GENERAL NOTES 15. DETAILS OF FALSEWORK AND JACKING LOCATIONS

### THE FOLLOWING STANDARDS ARE REQUIRED FOR THIS PROJECT

	OKLAHOMA OF TRANSPORTATION		IT OF TRANSPORTATION IGHWAY ADMINISTRATION
DATE APPRO	VED	DATE AF	PPROVED
ВҮ	,	BY	
	CHIEF ENGINEER	· ·	DIVISION ADMINISTRATOR
C W O	DRAIFAT NA	CCID FF/FOFT	CUEET NO I

### GENERAL NOTES

### SPECIFICATIONS

All construction and materials shall be in accordance with the 1988 Oklahoma Standard Specifications for Highway Construction and Special Provisions. (See Proposal for Special Provisions).

AMCHOR BOLTS:

a) Material: Anchor bolts shall be either hot rolled continuously threaded bars conforming to AISI 4140 or deformed reinforcing bars of sufficient size to produce threads of the UNC series for bolt size called for on the Plans. Minimum sizes of reinforcing bars, if used, shall be as follows: 1" Bolt - #9 Bar, 1 1/4" Bolt - #11 Bar, 1 1/2" Bolt - #14 Bar

Small be ds follows: I bolt - F9 bar, 11/4 bolt - F11 bar, 11/2 Bolt - F14 Bar. All anchor bolts, nuts, and washers shall be galvanized in accordance with AASHTO M232.

accordance with AASHIO M232.
b) Installation:
Anchor bolts may be preset at the time the concrete is poured.
If the Contractor elects to place the anchor bolts after the concrete is poured, the setting of the anchor bolts shall be in accordance with the following procedure:
Holes of sufficient depth shall be preset at all anchor bolt locations. The material used to form holes shall not be oiled or greased and must be removed before the placing of the anchor bolts. Diameter of holes shall be 11/2 larger than the anchor bolts. Anchor bolts shall be set in melted sulphur or an approved pourable embedding material before bearing assemblies are set in place. The use of non-shrink grout for embedding anchor bolts will not be permitted. permitted.

permitted.

c) Sizing: The minimum requirement for anchor bolt size and length (Fixed or Expansion Bearing) is:

Spans 50 feet in length and less: 1" dia. bolt - set 10" into

concrete.

Spans over 50 feet to 100 feet in length: 1 1/4" dia. bolt - set 12" minimum into concrete.

Spans over 100 feet to 150 feet in length: 1 1/2" dia. bolt - set 15" minimum into concrete.

Anchor Bolt holes shall be drilled with a rotary type drill. Care shall be taken to avoid cutting existing reinforcing steel.

### CLASS AA CONCRETE

A high range water reducer shall be used in all "Class AA Concrete" required for this project in accordance with Section 701.03 of the Specifications.

VERIFICATION OF EXISTING CONDITIONS:

All dimensions of the existing bridge components shown on the Plans are approximate. The Contractor shall verify all dimensions necessary to connect the new material and shall be solely responsible for the accuracy thereof.

accuracy thereof.

Bidders will fully inform themselves of the nature of the work and condition under which it will be performed. The Contractor shall adopt methods consistent with good construction practice and shall take all necessary preautions to prevent damage to the existing bridge or attachments. Any damage to the existing bridge structure or roadway due to the Contractor's negligence shall be repaired at the Contractor's expense, to the satisfaction of the Engineer.

LP/EPOXY CONCRETE ADHESIVES FOR CONSTRUCTION JOINTS:

a) Purpose: LP/Epoxy Concrete Adhesives shall be used in the construction joint to bond the new Portland Cement Concrete to the old

a) Purpose: LP/LPDX Concrete Agnesives Snail we used in the construction joint to bond the new Portland Cement Concrete to the old concrete in place.

b) Surface Preparation: Surface preparation for Portland Cement Concrete: Remove all loose and unsound material from the surface prior to application of LP/Epoxy Concrete Adhesive. If the concrete is unsound, use a jackhammer or pick to uncover sound concrete. Small pieces of concrete and dust shall be removed with air, water, or broom.

c) Installation: LP/Epoxy Concrete Adhesive may be applied by brush, roller, spray, or broom. An even 5-10 mil film thickness shall be applied for optimum adhesion between surfaces.

d) Precautions: Porous concrete absorbs adhesive and leaves a dry surface. Application shall be made immediately before concrete is poured. Do not apply wet concrete over dry areas. Reapply adhesives to dry areas. Surface must show wet adhesive to be effective.

e) Method of Payment: All costs of LP/Epoxy Concrete Adhesives shall be included in the price bid for other items of work.

a) All permanent structural steel shall be A-36 except new stainless steel pins.

stainless steel pins.

b) Shop Drawings: The "Bearing Support Bracket" is detailed and dimensioned from calculated slopes. No accounting has been made in the details for actual conditions. Shop drawings will include such adjustments as are necessary to provide a level surface and the proper

adjustments as are necessary to provide a level surface and the proper height to place the bearing assembly.

c) Construction: After the "Bearing Support Bracket" has been placed, the contractor shall verify that the bearing arm of the bracket is level. Maximum tolerance shall be 1%. If the arm slope is greater than 1% from absolute level and or the vertical dimension at centerline of bearing is not within 4 "of the plan dimension (10%"), the "Bearing Support Bracket" shall be refabricated such that it falls within the allowable tolerance. REFER TO ADJUSTABLE HEIGHT BEARING ASSEMBLY NOTE FOR MORE INFORMATION.

d) High Strength Bolts: High strength A-125 steel bolts shall be

d) High Strength Bolts: High strength A-325 steel bolts shall be used for all field and shop connections. Unless otherwise noted or

shown

High strength bolts shall be tightened by using "Turn-of-Nut" method or by means of "Direct Load Indicators". The "Calibrated Wrench" method shall not be used. Tightening by means of "Direct Load Indicators" will be permitted, provided an accurate direct measurement procedure confirms that the bolts have been tightened to attain the

Refer to Special Provision 724-1 for additional requirements for high strength bolting.

e) Welding: All welding for structural steel shall conform to the BRIDGE WELDING CODE ANSI/AASHTO/AWS DI.5.

No field or shop welding will be allowed except as shown on the

payment.

f) Inspection Requirements: Radiographic and Ultrasonic, or Magnetic Particle Inspections will be required as appropriate.
g) Painting: All disturbed existing structural steel and all new structural steel shall be painted with a "Red Lead Ready-Mixed Three (3) Coat System" or an approved method. All painting shall be in accordance with the 1988 Standard Specifications. All cost of painting shall be included in the price bid per lb. of structural steel. Temporary steel used in Falsework shall not be nainted

used in Falsework shall not be painted.
h) Inspection Requirements: Radiographic and Ultrasonic, or Magnetic Particle Inspections will be required as appropriate.

PINS AND RECESSED NUTS: (PIERS 77, 82, and 7 Ramp 22)

All hanger pins at Piers 77, 82 and 7 Ramp 22 shall be removed intact without burning. The contractor shall mark the pins removed such that they can be identified by span, location, girder, and upper or lower pin. The Engineer shall examine the pins for defects. If any defective pins are discovered, those pins shall be returned to the Bridge Division and remain the property of the State. All remaining pins shall become the property of the contractor and shall be disposed of in an approved manner.

The pins shall be replaced with new 3"- minimum diameter stainless steel pins using M169 steel at all locations that are not directly over the new concrete pedestal. Replacing the pins at the concrete column locations are optional and are not included in the estimated quantity for "Structural Steel". The new pins shall be insulated with rubber hose or the void filled with silicone or other approved method. The new pins shall be installed after the bearing arm brackets are in place. All cost of removing existing pins, new stainless steel pins, installing new pin, necessary hardware and incidentals shall be included in the unit price bid for "Structural Steel". unit price bid for "Structural Steel".

### ADJUSTABLE HEIGHT BEARING ASSEMBLY (PIERS 77 and 82 and PIER 7 RAMP 22)

- (1) Block existing hanger pins with oak blocks to insure that no movement is possible.
- (2) Field drill bolt holes through the Support Bracket and existing girder as shown on the plans. Bolt the Support Bracket to the existing girder with 1 1/4" bolts.
- (3) Cope the diaphragm and remove the lower part of the bolted connection as shown on the plans. Install filler plates as required. Tack weld the prepunched 1/2" plate to the existing web plates as shown on the plans. Field drill the bolt holes through the filler plates and the existing web. Install the double angles with 1" bolts through the web. Bolt the Hanger Bars to the extended stiffener plates on the Bearing Pad Support Bracket using 7/8" bolts. Field drill the bolt holes through the double angles for connection to the prepunched Hanger Bars. Bolt the Hanger Bars to the double angles using 7/8" bolts.
- (4) Slide the bearing assembly into place.
- (5) Begin jacking until the jacks are in bearing. <u>DO NOT RAISE THE</u> GIRDERS, more than 1/8".
- (6) Adjust the vertical height on the bearing assembly. The 2" plate under the elastomeric bearing pad must be perfectly level. The dimension from the bottom of the girder to base of the bearing assembly must be exactly 94" at the centerline of bearing. After the height has been adjusted, holes shall be drilled in the double angles and bolted to hold the correct position.
- (7) Fill the void between the bearing plate and the Bearing Support Bracket using the Epoxy Resin Injection System to transfer full bearing onto the Bearing Pad Support Bracket in accordance with special provision "Structural Concrete Repair by Sealing and Injection". All cost shall be included in the unit price bid per gallon of "Epoxy Resin, Above Water".
- (8) Field weld the bearing assembly to the bottom flange of the existing girder as shown on the plans.
- Remove and reinstall the pins in accordance with the PINS AND RECESSED NUTS note and remove the jacks, placing bearing on the Bearing Support Bracket.

## (10) Install the crossframe angles as shown on the plans.

# BEARING PADS AT HANGER BRACKETS All bearing pads shall be included in the price bid for "Structural

THREE UNIT CONCRETE ANCHOR EXPANSION BOLTS:
All costs of materials, tools, labor, and incidentals necessary to place three unit concrete anchor expansion bolts shall be included in the price bid for other items of work.

FALSEWORK AND JACKING:

Pay Item "Falsework and Jacking" shall include all excavation and backfilling the excavated void when falsework is removed, metal strapping, drilled holes in pier cap, structural steel, jacks, welds, labor, materials, cleaning the pier cap and section of angle to be placed on the west side of the pier cap, and incidentals necessary to place a total of ninternen (19) girders at Pier 78 and Pier 8 ramp 22 on temporary supports.

The jacking sequence shall be in the numerical sequence indicated on the plans. All jackings with the same number may be jacked in any sequence, but all jackings with the same number shall be completed before beginning the next jacking number. All girders shall be jacked simultaneously at Pier 7 Ramp 22. Additional jacking may be required.

Jacking shall compensate for any settlement which has occurred on the west side of Pier 78 and Pier 8 ramp 22. The contractor shall obtain profile data in the vicinity of the expansion joint. If necessary, the beams shall be raised to produce an even grade across the joint. Profile adjustment and jacking cost shall be included in the price bid for Falsework and Jacking.

The contractor shall have the option of using used steel provided the sections meet or exceed the member sizes shown on the plans. For the crossbeams the Contractor may use the crossbeams from Pier 81 as described in "ITEMS OF WORK CARRIED OVER FROM E-SAP-55(578)" or shall use used beams from the Norman 1-35 Maintenance Yard. Beams will require some modification to meet the span requirements needed for the crossbeams. The Contractor may need to remove some of the shear connectors. The Bridge Division will determine which sections will be used. If in the opinion of the Engineer the Contractor damages one of these beams while they are in his possession, the Contractor shall provide full compensation to the County for the damaged beam. -Price bid for Falsework and Jacking shall include cost of modifying and transporting these beams to the project site and removing and transporting them back to the Norman Yard.

BEARINGS ON FOOTINGS (PIERS 78 and PIER 8 RAMP 22):

After the contractor has excavated to expose the top of the footing, the area where the sole plate is to be placed shall be sandblasted and ground with a carbbrundum brick before placement of the piling sole plates. If leveling is necessary, this shall be achieved with shim plates (plywood may be used as directed by the Engineer). Leveling shall be done before metal straps are wrapped at the third point of the columns. All cost of bearing shall be included in the price bid for "Falsework and Jacking".

### ANGLE FOR CONCRETE FORMWORK (PIER 78 and PIER 8 RAMP 22)

The contractor shall place a 6x8xi angle and 3-unit concrete anchors across the west side of the pier cap as shown on the plans before the crossbeam is placed. All cost of Angle for Concrete Formwork shall be included in the price bid for Falsework and Jacking.

Metal Strapping or and approved alternate shall be wrapped around the column and piling a minimum of three (3) double wraps as approved by the Engineer. The minimum size of metal strap shall be two (2) inches. All cost of Metal Strapping shall be included in the price bid for

JACKING EXTERIOR GIRDERS (PIERS 78, 81 and PIERS 7 and 8 RAMP 22) When jacking the exterior girders at Piers 78 and 81 the lane above the girder shall be closed to traffic. When jacking the girders at Piers 7 and 8 Ramp 22 the ramp shall be closed to traffic.

### BEARING PADS:

All bearing pads shall be placed when the temperature is between  $50^\circ F$  and  $70^\circ F$  .

PIER COLUMN REPAIR: (PIERS 77, 82, and 7 RAMP 22)
The Pier Columns at Piers 77 and 82 shall be encased with a nine (9) inch reinforced collar and a five (5) foot cap extension. A concrete pedestal shall be formed on the cap extension to provide bearing for the sixty (60) foot girders. Pier 7 Ramp 22 shall have a pedestal formed as shown on the plans.

shown on the plans.

All loose concrete shall be removed and the existing columns shall be sandblasted to ensure a clean bonding surface.

Bearing shall not be placed on the new pedestals until the concrete has been in place 10 days and meets the strength requirement of subsection 701.01(d) of the Standard Specifications. All cost of repairing pier columns shall be included in the unit price bid per each "Repair Concrete Pier". Individual quantities are shown on the Pier sheet for estimating purposes only.

CLEANING PIER CAPS:

After all the beams on the west side of Pier 78 and Pier 8 ramp 22 have been placed on temporary supports, the contractor shall remove all of the broken concrete and debris from the west side of the pier cap and pedestals. All cost of cleaning pier caps shall be included in the price bid for "Repair Concrete Pier".

REPAIR CONCRETE PIER
Pay item "Repair Concrete Pier" includes the following 8 Piers: 77
left, 77 right, 7 Ramp 22, 78 left, 78 right, 8 Ramp 22, 82 left and 82

REPAIR CONCRETE PIER (PIER 78 Right and Left)

Item "Repair Concrete Pier" consists of removing the elevated section of the pier cap to twelve (12) inches above the lower section of Pier 78 right and left. A new epoxy coated reinforced pier cap section shall be formed using "Class A Concrete" as shown on the plans. All cost of Class A Concrete, Epoxy Coated Reinforcing Steel repairing the cracks and spalls in the cap and columns as directed by the Engineer, materials, labor, and incidentals necessary to restore the pier cap shall be included in the price bid for "Repair Concrete Pier".

Estimated quantities for this item as follows;

Class AA Concrete

C.Y. 34.7

Epoxy Coated Reinforcing Steel

IB. 3530.0

Three Unit Concrete Pier" shall be completed and the concrete shall obtain a minimum strength of 3000 psi prior to any jacking of bearing placed on the pier cap.

CONSTRUCTION SEQUENCE (PIER NO. 78 and PIER 8 RAMP 22)

The contractor shall replace the existing bearing shoes on the east side of Pier 78 and Pier 8 Ramp 22 as shown on the plans before "Repair Concrete Pier" begins. See "FIXED BEARING ASSEMBLY (PIER NO. 78 and Pier 8 RAMP 22)" note.

FIXED BEARING ASSEMBLY (PIER NO. 78 and PIER NO. 8 RAMP 22)

Item "fixed Bearing Assembly" shall consist of removing and replacing the existing bearing assemblies on the west side of Pier 78 and Pier 8 Ramp 22 in accordance with the Standard Specifications and as shown on the plans. All cost of elastomeric bearing pads, bearing plates, anchor bolts, nuts, materials, labor, and incidentals necessary to replace the existing bearings shall be included in the unit price bid ner each "Fixed Rearino Assembly". per each "Fixed Bearing Assembly".

SHIM PLATE MELDS UNDER BEAMS (PIER 70, AND PIER 8 RAMP 22):
In order to allow for future grade adjustments and for the placement of the new bearing assembly under the girders, additional jacking may be required. Crossbeams placed directly under bridge girders shall not be welded to the shim plates. All shim plates shall be welded to each other and to the vertical supporting member in place to provide stability. All cost of shim plate welds shall be included in the price bid for "Falsework and Jacking".

CONSTRUCTION SEQUENCE (PIER 81)

The contractor shall replace the existing bearing shoes on the west side of Pier 81 with new elastomeric bearing assemblies as shown on the plans. All cost of replacing the expansion bearing shoes shall be included in the price bid per each "Expansion Bearing Assembly".

EXPANSION JOINTS:

The finger Expansion Joints (left side of 1-40) at all Expansion Piers of this project have had plates welded to one side of the device during a previous overlay project. It shall be necessary to torch cut the finger extrusion on the free side of the device to allow for jacking as approved by the Engineer. All cost of torch cutting shall be included in the price bid for "Falsework and Jacking".

All debris shall be removed from the expansion devices at Piers 77, 78, 81, 82 and Piers 7 and 8 Ramp 22 while traffic control is in place on 1-40. The contractor shall also check the driving surface at these locations. If the driving surface is not even, adjustments shall be necessary on bearing arm brackets. All cost of removing debris and evening the driving surface shall be included in other items of work.

PIER DRAIM PIERS:
Six (6) and eight (8) inch drain pipes are anchored to the Pier Cap
and Columns. The drains shall be temporarily disconnected from the
scuppers and moved to allow for Falsework and or Construction. The
Drain Pipes shall be reconnected after the construction is completed.
All cost of moving and resetting Drain Pipes shall be included in other

REMOVE AND RESET GUARDRAIL, LIGHT POLES, AND CHAIN-LINK FENCE:
The guardrail, light poles, and chain-link fence shall be temporarily removed to allow for construction and equipment in the area of Piers 77 and 78. When construction is completed, these items shall be returned to their original position and condition. The contractor shall contact Steve Klika with COTPA, 300 East California, Oklahoma City, Oklahoma, 73104 before removal is begun. All cost of removaling and resetting shall be included in other items of work.

### PENETRATING WATER REPELLENT SURFACE TREATMENT

PHILLIAGING MAIER REPELLENT SURFACE TREATMENT
A Penetrating Nater Repellent Surface Treatment shall be applied to
the top, side, and end surfaces of Piers 78 and 81 and Piers 7 and 8
Ramp 22 and the top; and end surfaces of the 5'-0" cap extensions on the
columns of Piers 77 and 82. All cost of treatment shall be included in
the unit price bid per S.Y. of "Penetrating Nater Repellent Surface
Treatment", Estimated quantities are as follows:

Pier	77		95.0	S.Y.
Pier	7 Ramp 3	22	20.0	S.Y.
Pier	78		360.0	S.Y.
Pier	8 Ramp	22	60.0	S.Y.
Pier			435.0	S.Y.
Pier	82		95.0	S.Y.

VALUE ENGINEERING:
Alternate designs made by Professional, Registered Engineer, registered in the State of Oklahoma will be considered, but must be approved by the Oklahoma Department of Transportation, Bridge Division.

# REVISIONS

ITEMS OF MORK CARRIED OVER FROM E-SAP-55(578)

The falsework located at Pier 81 must remain in place until bearing assemblies have been replaced on the west side of Pier 81 shown on the plans. Due to the location of the falsework at Pier 81 following items shall be placed on this project. Costs shall included in other items of pay.

- 1) Remove falsework at Pier 81 after the bearing assemblies have been installed on the west side of Pier 81. The crossbeam of the falsework shall be inspected by the Engineer for yielding, web buckling, or cracks. If in the opinion of the Engineer, the contractor damages the crossbeam while in his possession, the contractor shall provide full compensation to the County for damages. If the crossbeam is approved by the Engineer the contractor may reuse if for the falsework at Pier 78. If the contractor elects to reuse the crossbeam it shall be subjected to the same inspection and conditions as when it was removed at Pier 81 after construction is completed at Pier 78. If the crossbeam is approved by the Engineer, the contractor shall deliver the crossbeam to the Norman Maintenance Yard and the remaining members of falsework removed from Pier 81 shall be returned to Jensen Construction Company, P.O. Box 9919, Iulsa Oklahoma 74157. All cost of removing falsework members and returning them to their respective locations shall be included in the price bid for "Falsework and Jacking". After the falsework has been removed from Pier 81 the existing structural Steel members shall be filled, ground smooth, and painted in accordance with the Standard Specifications. The new stiffeners shall also be painted. All cost of repairing and painting structural steel at Pier 81 shall be included in other items of work
- (2) Remove any remaining forms from the pier cap and pedestals. Repair concrete spalls and cracks on the pier cap, pedestals and columns of Pier 81. Falsework bolts and sleeves shall also be removed from the pier cap and the spalls and holes shall be filled and repaired as directed by the Engineer. All cost of repairing Pier 81 shall be included in other items of work.
- (3) Apply "Penetrating Water Repellent Surface Treatment" to the top, side, and ends of Pier 81 pier cap. All cost of treatment shall be included in the unit price bid per S.Y. of "Penetrating Water Repellent Surface Treatment". The estimated quantity for this item is 435.0 S.Y..
- (4) The 6x8xi angle on Pier 81 shall be ground to remove all traces of clip angles used to support the formwork. The angles shall have all excess overhangs cut off and returned to Jensen Construction Company. The angles shall remain in place and shall be painted in accordance with the Standard Specification.
- (5) The contractor shall backfill the excavated void to the footings of Pier 81. All cost backfilling shall be included in other items of
- (6) The contractor shall reinstall the conduit and wire for lighting at Pier 81. All cost of reinstalling shall be included in other items of work.
- (7)The contractor shall repair the diaphragm between girder 14 and 15 on the east side of Pier 81 as approved by the Engineer. All cost of removing and replacing damaged portion of diaphragm shall be included in other items of work.
- (8)Bearing Pads shall be installed on the east side of Pier 81. The pads are fabricated and in the possession of the Engineer. All cost of installing bearing pads shall be included in other items of work.

I-40 CROSSTOWN Design Detail LKB 8/8 Check GENERAL NOTES Smuad: McGUIRF

OKLAHOMA COUNTY

STATE OF DEPARTMENT OF TRANSPORTATION OKLAHOWA PROJ. NO. E-SAP-55(595)

### TRAFFIC OPERATIONS PAY QUANTITY NOTES

- (TO-19) THIS ITEM INCLUDES AN ESTIMATED 500 L.F. 4" WHITE AND 500 L.F.
  4" YELLOW STRIPE. THE CONTRACTOR SHALL PROVIDE AND INSTALL "3M CORP. DETOUR GRADE REMOVABLE TAPE" OR "CATAPHOTE CORP. DETOUR GRADE REMOVABLE TAPE" OR AN APPROVED EQUAL.
- (TO-70) THIS ITEM IS AN ESTIMATED QUANTITY TO BE USED AS DEEMED NECESSARY BY THE ENGINEER.

### TRAFFIC OPERATIONS GENERAL CONSTRUCTION NOTES

DUE TO THE TEMPORARY NATURE OF CONSTRUCTION SIGNING, FOOTINGS WILL HAVE NO REINFORCING STEEL.

ALL SIGNS SHALL BE CONSTRUCTED TO MEET THE CURRENT OKLAHOMA DEPARTMENT OF TRANSPORTATION STANDARD SPECIFICATIONS.

ONE (1) WING BARRICADE SHALL BE SET ON EACH SIDE OF THE ROADWAY 250° IN ADVANCE OF THE FIRST ADVANCE WARNING SIGN IN EACH ADVANCE WARNING SERIES.

THIS PROJECT SHALL BE CONSTRUCTED WITHOUT CLOSING TRAFFIC ON CROSS STREETS. A MINIMUM OF ONE LANE IN EACH DIRECTION SHALL BE MAINTAINED AT ALL TIMES.

THE CONTRACTOR SHALL REPAIR OR REPLACE ANY NEW OR EXISTING SIGNS WHICH ARE DAMAGED DUE TO HIS NEGLIGENCE OR CARELESS HANDLING DURING THE CONSTRUCTION OF THIS PROJECT. THIS SHALL BE DONE AT THE CONTRACTORS EXPENSE.

TRAFFIC CONDITIONS MAY NECESSITATE CHANGES IN THE USE AND/OR QUANTITIES OF THE TRAFFIC CONTROL DEVICES AS SHOWN IN THE PLANS OR IN THE STANDARDS. ANY SUCH CHANGES ARE SUBJECT TO THE APPROVAL OF THE ENGINEER.

ANY SIGNS AND/OR DELINEATORS WHICH ARE TO BE REMOVED DURING THIS PROJECT WILL BE STORED IN A PROTECTED AREA DESIGNATED BY THE RESIDENT ENGINEER, UNTIL SUCH A TIME THAT THEY ARE TO BE RESET BY THE CONTRACTOR. COST OF THIS WORK TO BE INCLUDED IN OTHER ITEMS OF WORK.

ANY EXISTING SIGNING CURRENTLY IN PLACE WHICH IS IN CONFLICT WITH THE INDICATED CONSTRUCTION SIGNING AS SHOWN THE PLANS, OR ON THE T.C.D. STANDARD DRAWINGS, SHALL BE EITHER COVERED OR REMOVED AND STORED FOR THE DURATION OF THE PROJECT. THESE SIGNS SHALL BE EITHER UNCOVERED OR RE-INSTALLED, BY THE CONTRACTOR, UPON COMPLETION OF THE PROJECT. COST OF THIS WORK TO BE INCLUDED IN OTHER ITEMS OF WORK.

ALL CHANNELIZING DEVICES INITIALLY PROVIDED ON THIS PROJECT SHALL BE EITHER NEW OR IN LIKE NEW CONDITION AND SHALL BE APPROVED FOR USE ON THIS PROJECT BY THE ENGINEER.

ALL WORK ON I-40 MAINLINE OR OFF RAMPS WHICH WILL REQUIRE THE REDIRECTING OF TRAFFIC SHALL BE LIMITED TO THE HOURS BETWEEN 9 A.M. AND 3 P.M. MONDAY THRU FRIDAY AND ANYTIME ON SATURDAY OR SUNDAY. IF WORK IN THIS AREA IS PERFORMED ON SATURDAY OR SUNDAY IT WILL BE DONE ONLY DURING THE HOURS DEEMED TO BE SAFE BY THE ENGINEER.

REGULATORY SPEED LIMIT SIGNS SHALL BE USED TO SLOW TRAFFIC ENTERING LANE TAPERS ON I-40. THESE SPEED LIMITS SHALL BE REDUCED A MINIMUM OF 10 M.P.H. BUT MAY BE FURTHER REDUCED AT THE DISCRETION OF THE ENGINEER.

KEPAIK	EXP. HANGERS		
ITEM	DESCRIPTION	UNIT	QUANTITY
506 (A)	STRUCTURAL STEEL	LB.	77,180.00
515	PENETRAT WATER REPELL SURF.TR.	S.Y.	1,060.00
520(C)SP	EPOXY RESIN ABOVE WATER	GAL.	17.50
640	FIELD OFFICE	EA.	1.00
641	MOBILIZATION	L.SUM	1.00
900.41SP	FIXED BEARING ASSEMBLY	EA.	19.00
900.42SP	EXPANSION BEARING ASSEMBLY	EA.	32.00
900.51SP	FALSEWORK AND JACKING	L.SUM	1.00
900.73SP	REPAIR CONCRETE PIER	EA.	8.00

	PAY QUANTITIES		
IC CON	TROL I-40 & E.K. GAYLORD		
ITEM	DESCRIPTION	UNIT	QUANTITY
856(B)	REMOVABLE PAVEMENT MARKING TAPE (4"WIDE) (TO-19)(TO70)	L.F.	1,000.00
880(C)	ADVANCE WARNING DEVICE(TYPE C)	S.D.	30.00
880(D)	SIGNS 0 TO 6.25 SF	S.D.	Í,575.00
880(E)	SIGNS 6.26 TO 15.99 SF	S.D.	300.00
880(F)	SIGNS 16.0 SF TO 32.99 S.F.	S.D.	870.00
880(H)	BARRICADES(TYPE 1)	S.D.	30.00
880(1)	BARRICADES(TYPE II)	S.D.	30.00
880(J)	BARRICADES(TYPE III)	S.D.	270.00
880(K)	WING BARRICADES	S.D.	270.00
880(H)	TYPE A LIGHT	S.D.	750.00
880(0)	TYPE C LIGHT	S.D.	3,150.00
880(P)	DRUMS	S.D.	3,150.00

SUMMARY OF PAY QUANTITIES (BRIDGE AND TRAFFIC) GENERAL NOTES (TRAFFIC)

Detail LKB 8/8 Check Squad: Mc GUIRE Engr.: PETERS

STATE OF DEPARTMENT OF TRANSPORTATION
OKLAHOMA PROLNG E-SAP-55 (595) SHEET NO. 3

DESIGN DATA

LOAD FACTOR DESIGN: CONCRETE CLASS AA f'c = 3,500 psi REINFORCING STEEL (GRADE 60) fy = 60,000 psi

ALLOWABLE STRESS DESIGN:
STRUCTURAL STEEL (A36) fs = 20,000 psi

LOADING: HS-20 or STD. OKLAHOMA O'LOAD TRUCK

DESIGN: AASHTO SPECIFICATIONS 1989 EDITION AND AWS SPECIFICATIONS

REACTIONS FOR JACKING PURPOSES:
PIERS 77, 82, and 7 RAMP 22

RDL = 20 TONS RLL+I = 26 TONS

RTOTAL = 46 TONS/GIRDER

PIERS 78 (WEST), 81(EAST), AND 8 RAMP 22 (WEST)

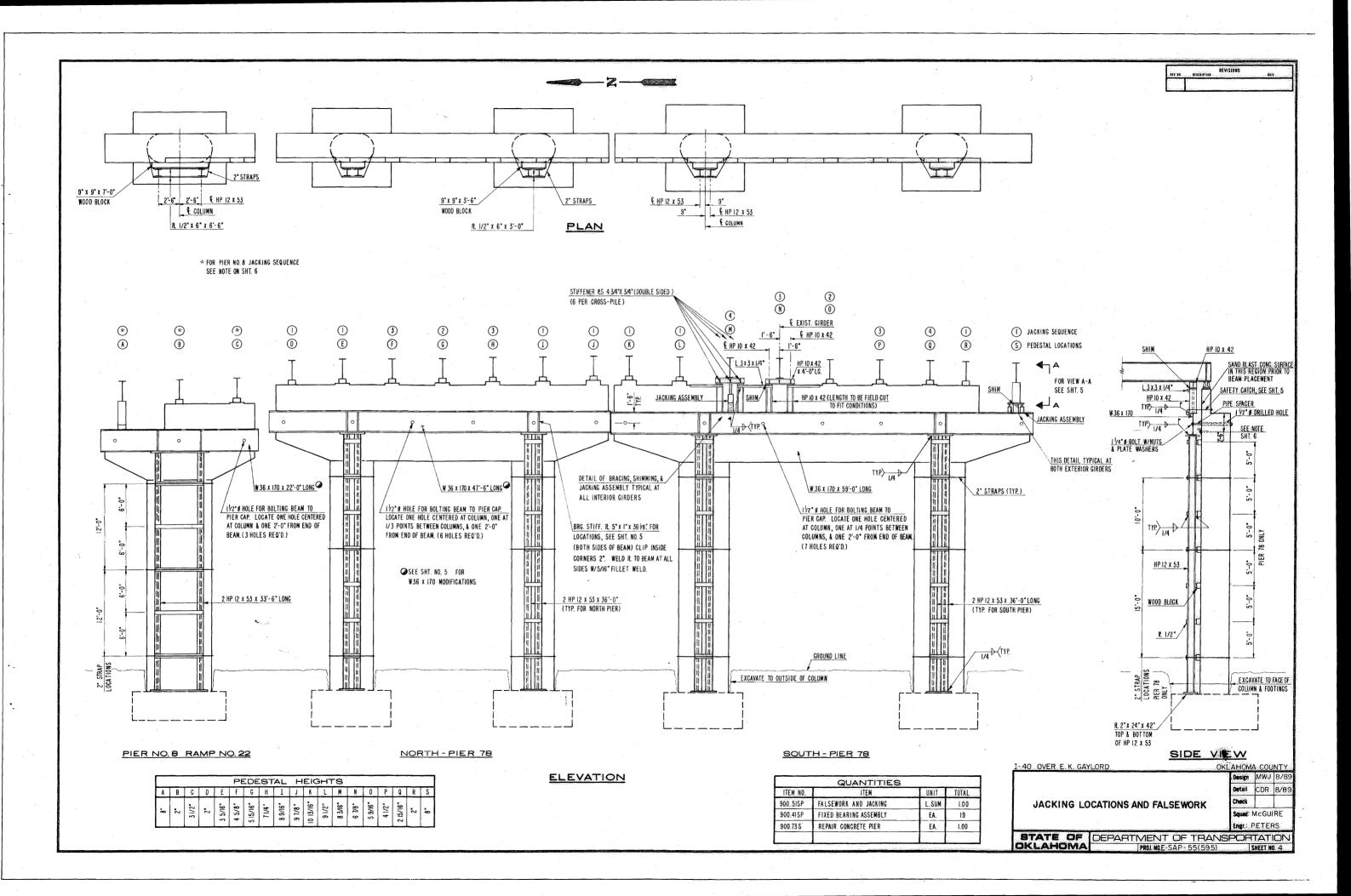
RDL = 20 TONS RLL+I = 26 TONS

RTOTAL = 46 TONS/GIRDER

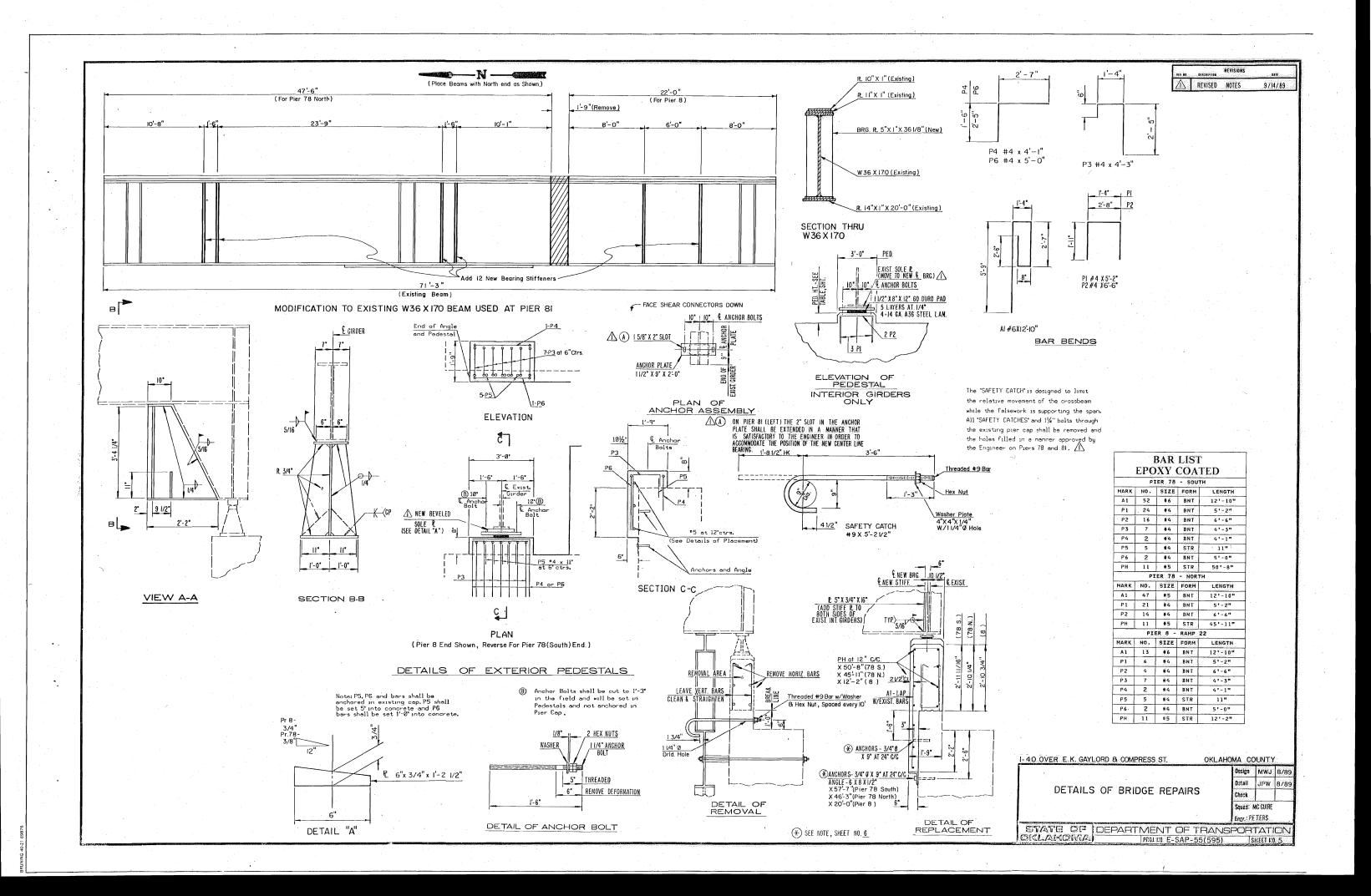
PIERS 78(EAST), 81(WEST), AND 8 RAMP 22(WEST)

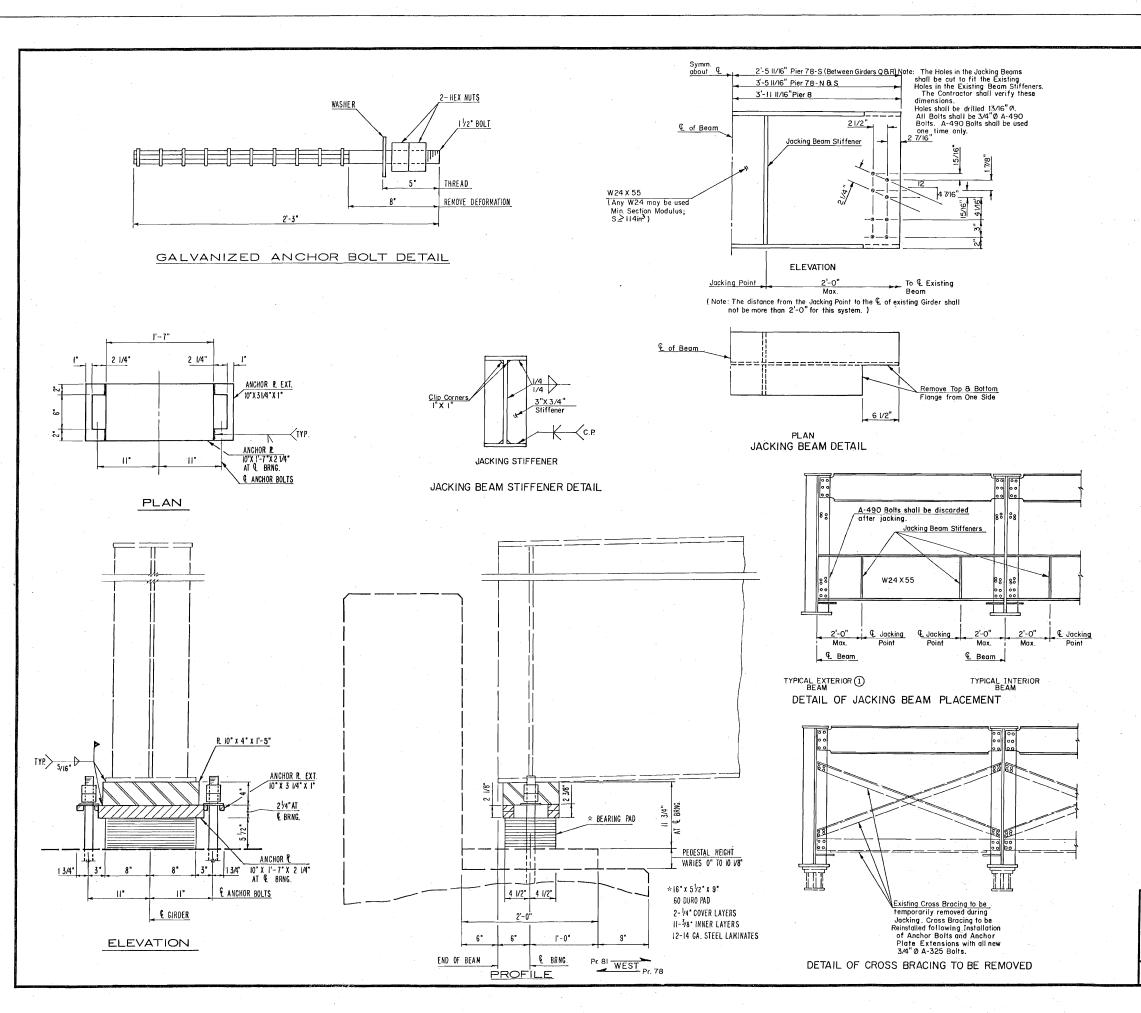
RDL = 28 TONS RLL+I = 38 TONS

RTOTAL = 66 TONS/GIRDER



40-21 69876





REVISIONS

Pay Item Expansion Bearing Assembly shall consist of removing and replacing the existing bearing assembly in accordance with these plans and the Standard Specifications. This item shall include jacking, cleaning, elastomeric bearing pads, bearing plates, anchor bolts, W 24 X 55 Beams, materials, labor and incidentals required to replace the existing bearing assembly on the west side of Pier 81 and the east side of Pier 78. The Contractor shall follow the following construction sequence:

- (1) Jacking shall be done when the temperature is between 50°F. and 70°F. Jacking shall be restricted to off-peak traffic hours, such as Sunday mornings.
  (2) The Contractor shall temporarily remove the existing crossframes except for the top member.
  (3) The Contractor shall bolt the jacking heam to the 72" plate girder as shown on the plans using the bolt holes from the crossframes and all new A-490 bolts and jack the girder as shown on the plans to take the load off the existing expansion assembly. On the ramp, all three (3) girders shall be jacked simultaneously. The reaction is approximately 70 tons per girder.
- assembly. On the ramp, all three (3) girders shall be jacked simultaneously. The reaction is approximately 70 tons per girder.

  (4) It is recommended that the Contractor torch the sole plate on all four sides and remove the existing bearing assembly. It may be necessary to torch the pintle. The anchor bolts should be cut off flush with the top of the pier cap.

  (5) The Contractor shall clean the top of the pedestal as directed by the Engineer. Sandblasting may be required. Concrete surfaces in the bearing area shall be ground with a carborundum brick. In the bearing area, the bottom of the steel girder shall be ground smooth.

  (6) The Contractor shall slide in the new bearing assembly, release the jacks, remove the jacking assembly, drill 3" holes for the 1-1/2" anchor bolts, and drop in the new anchor bolts. The anchor plate extensions shall be welded to the anchor plate.

  (7) The anchor bolts shall be grouted in accordance with the standard anchor bolt note shown on Sheet 2. The anchor plates shall be welded to the girder and the crossframes restored in accordance with the plans using new A-325 bolts.

  (8) The anchor plates, anchor plate extensions, 3/4" dia A325 bolts & nuts, shall be painted in accordance with the Standard Specifications.

\*If it is necessary to jack more than one (1) inch, the Contractor shall be required to jack the girders on both sides of the pier. The jacking sequence for this operation shall be obtained from the Bridge Division. If jacking is required on both sides, the elevated pier cap repair shall be completed and have obtained a minimum strength of 3,000 p.s.i. prior to jacking both sides as a safety precaution for the falsework.

The existing bearing assembly shall become the property of the Contractor and shall be removed from the project site in accordance with the Standard Specifications.

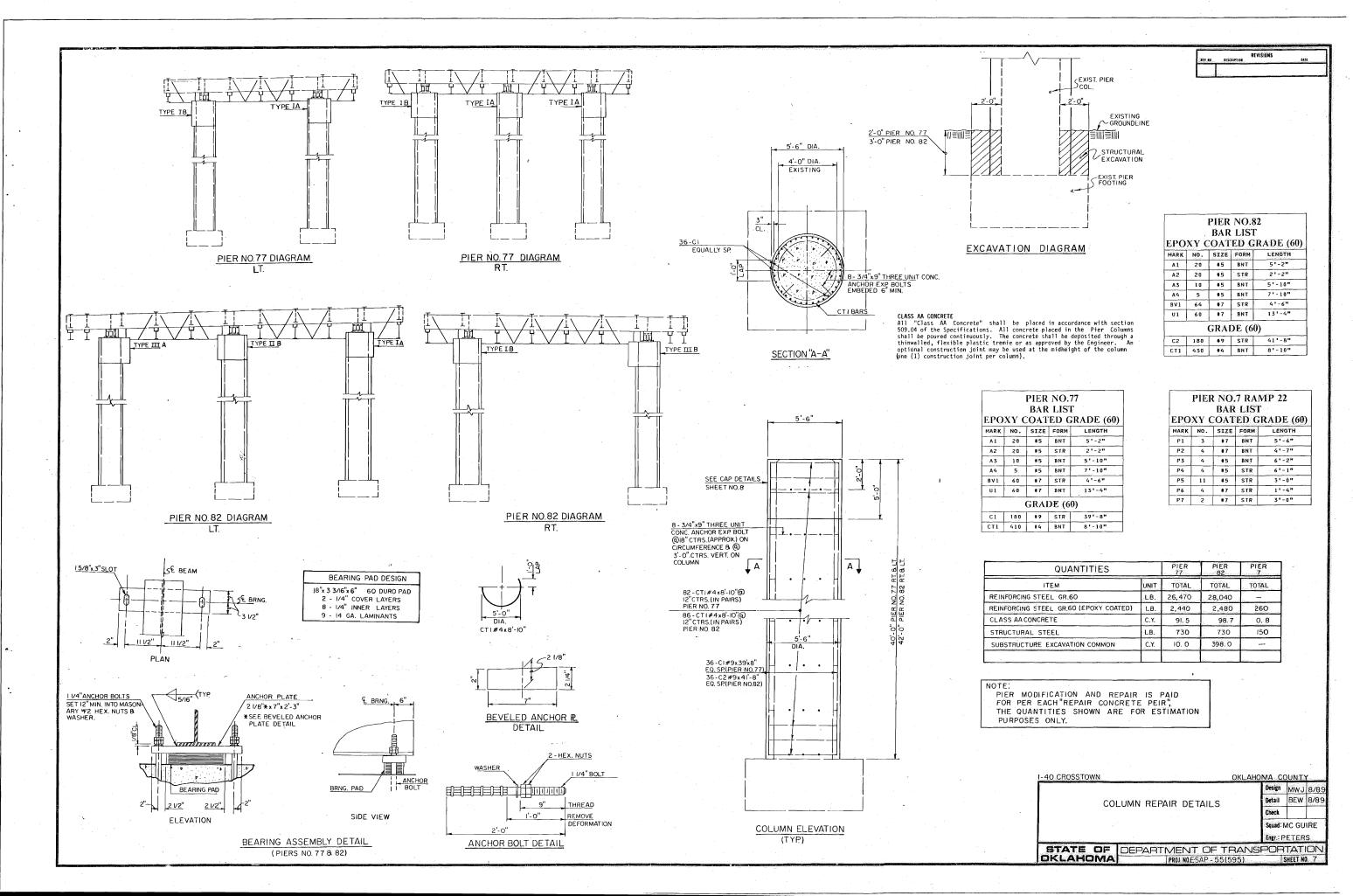
All structural steel shall be A-36. Used steel shall not be allowed except for the jacking beam.

	QUANTITIES		
I TEM NO.	ITEM	UNIT	TOTAL
900.42 SP 6165	EXPANSION BEARING ASSEMBLY	EA.	32

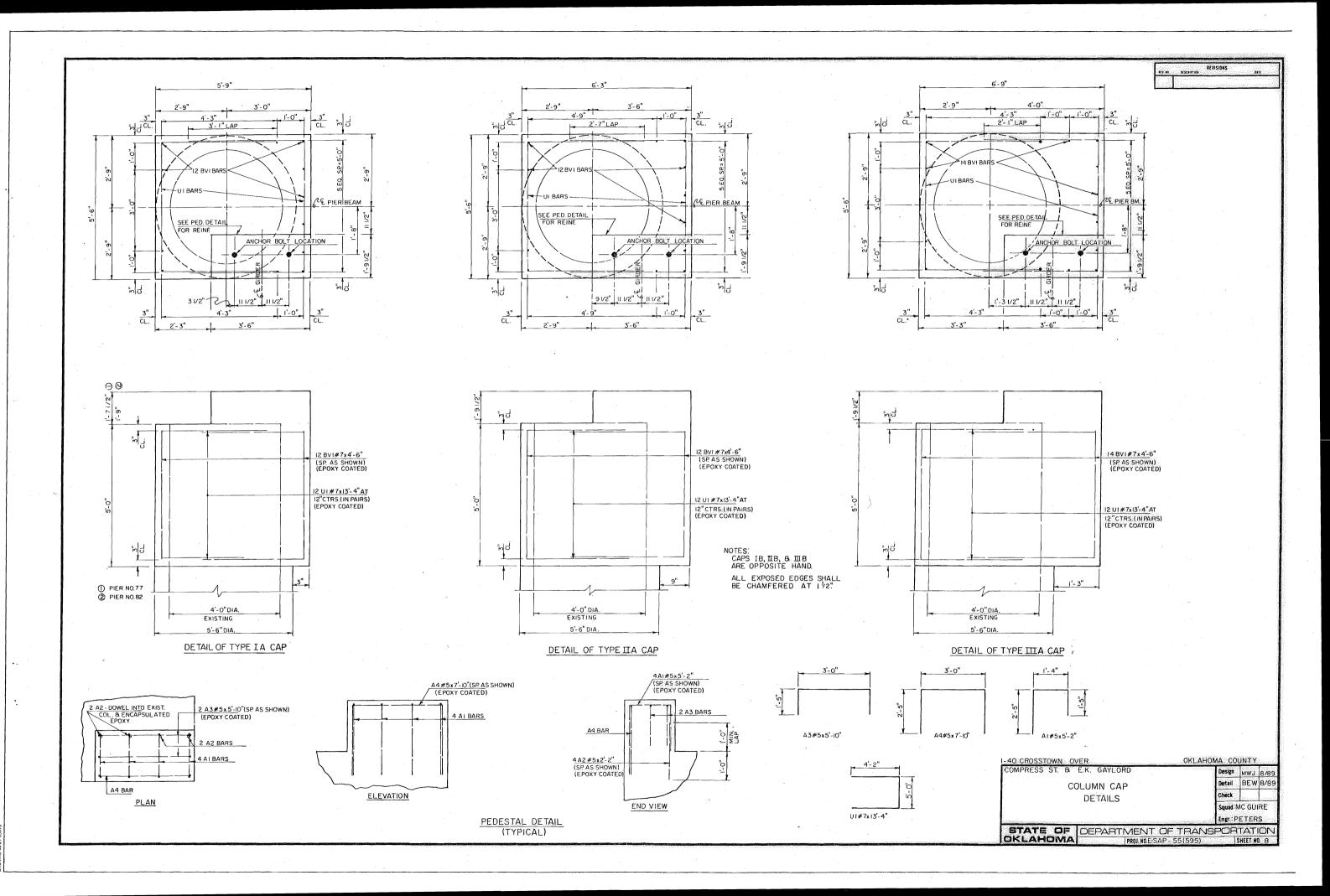
1) The jacking of the exterior girders shall be done from the inside only and shall be jacked only under dead load. In order to accomplish this traffic will have to be removed from the exterior lanes during the jacking. For further details see traffic notes on Sheet No. 3

NOTE: For Construction Sequence at Pier 78 refer to Sheet No. 2

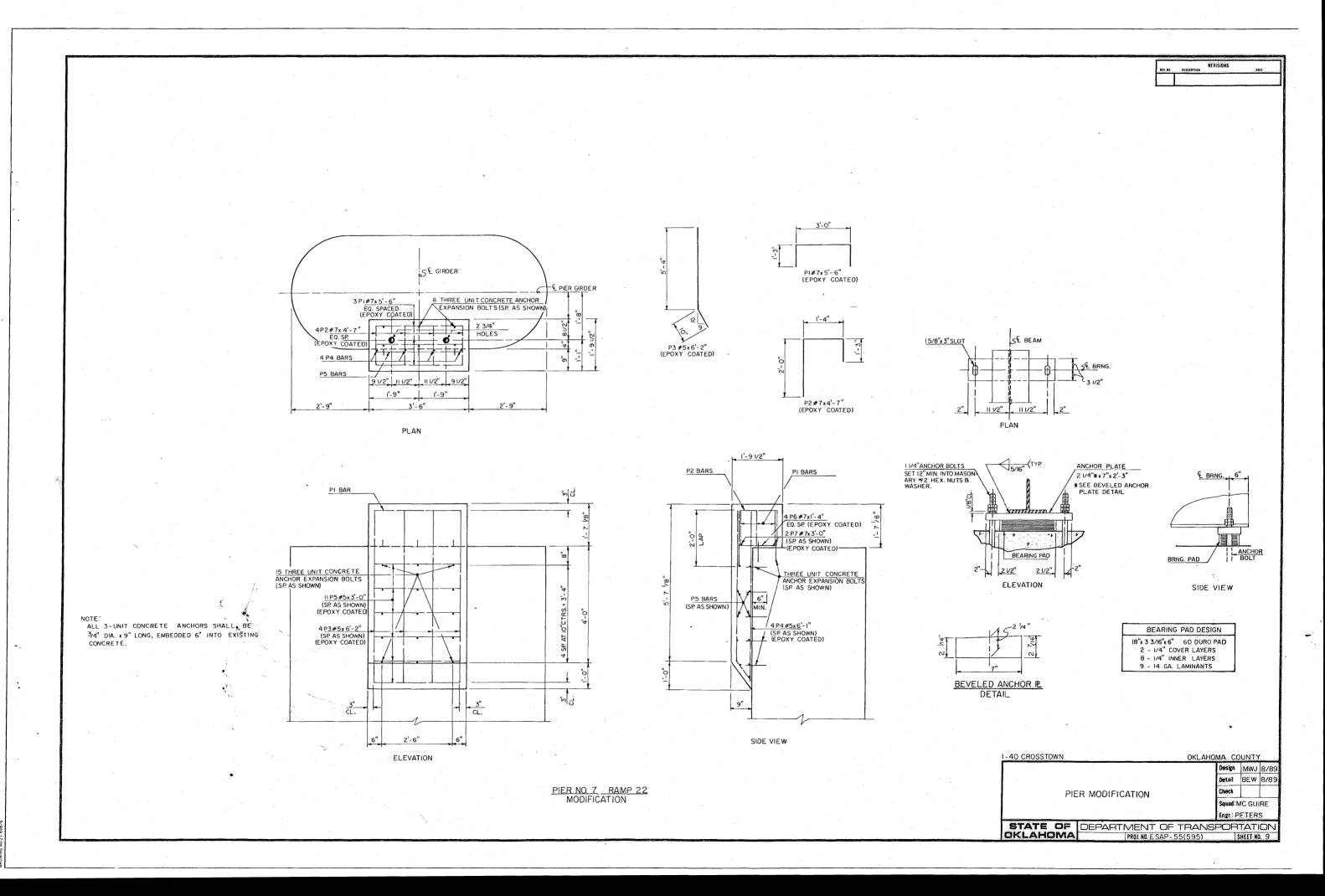
1-40 OVER E.K. GAYLORD & COMPRESS ST. OKLAHOMA COUNTY Design 200a 9/8 Detail JPW 9/89 BEARING REPLACEMENT Check AT PIER 78, PIER 81 Squad: MCGUIRE AND PIER 8 RAMP 22 STATE OF DEPARTMENT OF TRANSPORTATION OKLAHOMA | PROJ. NO. E-SAP-55(595) | SHEET NO. 6

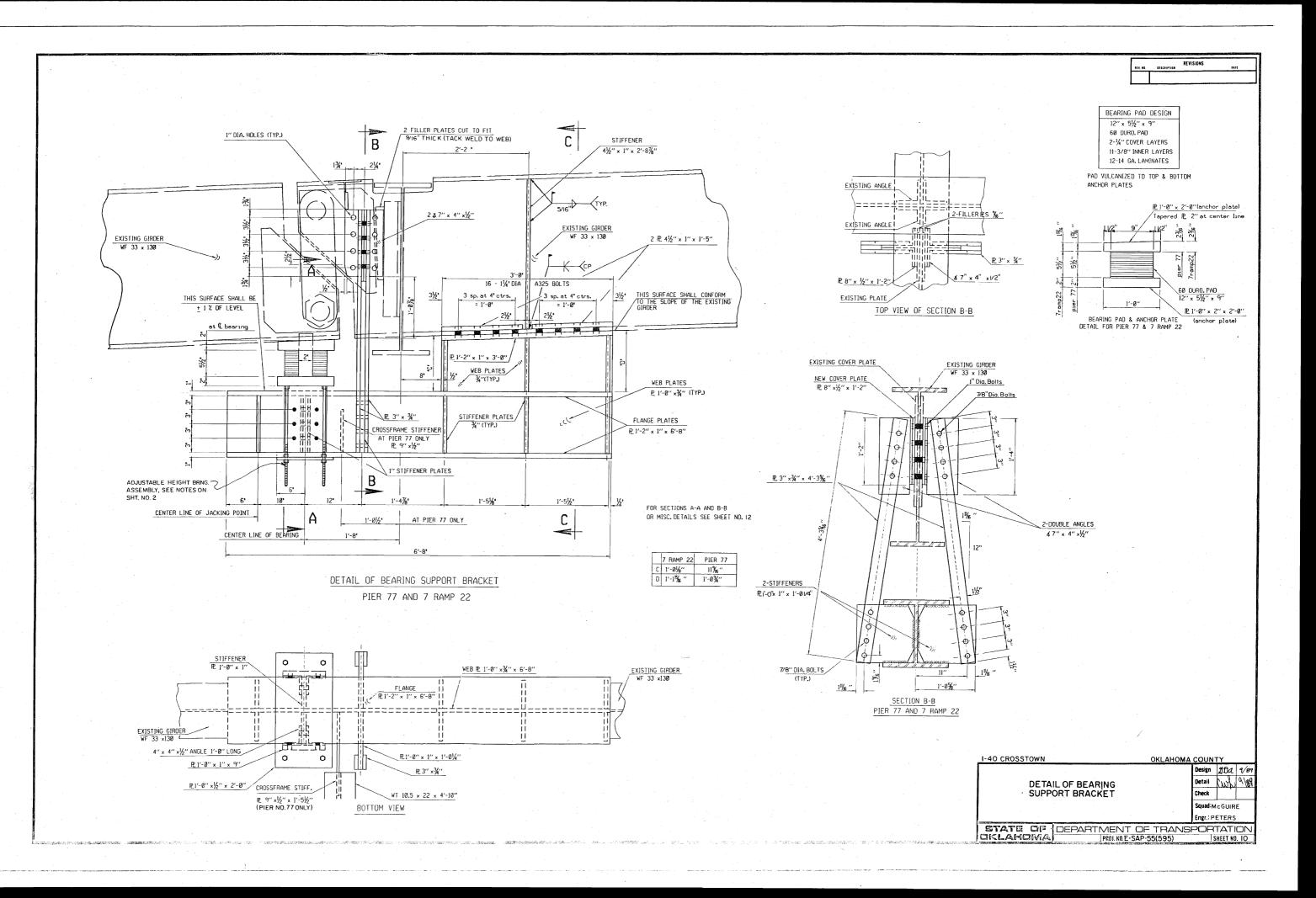


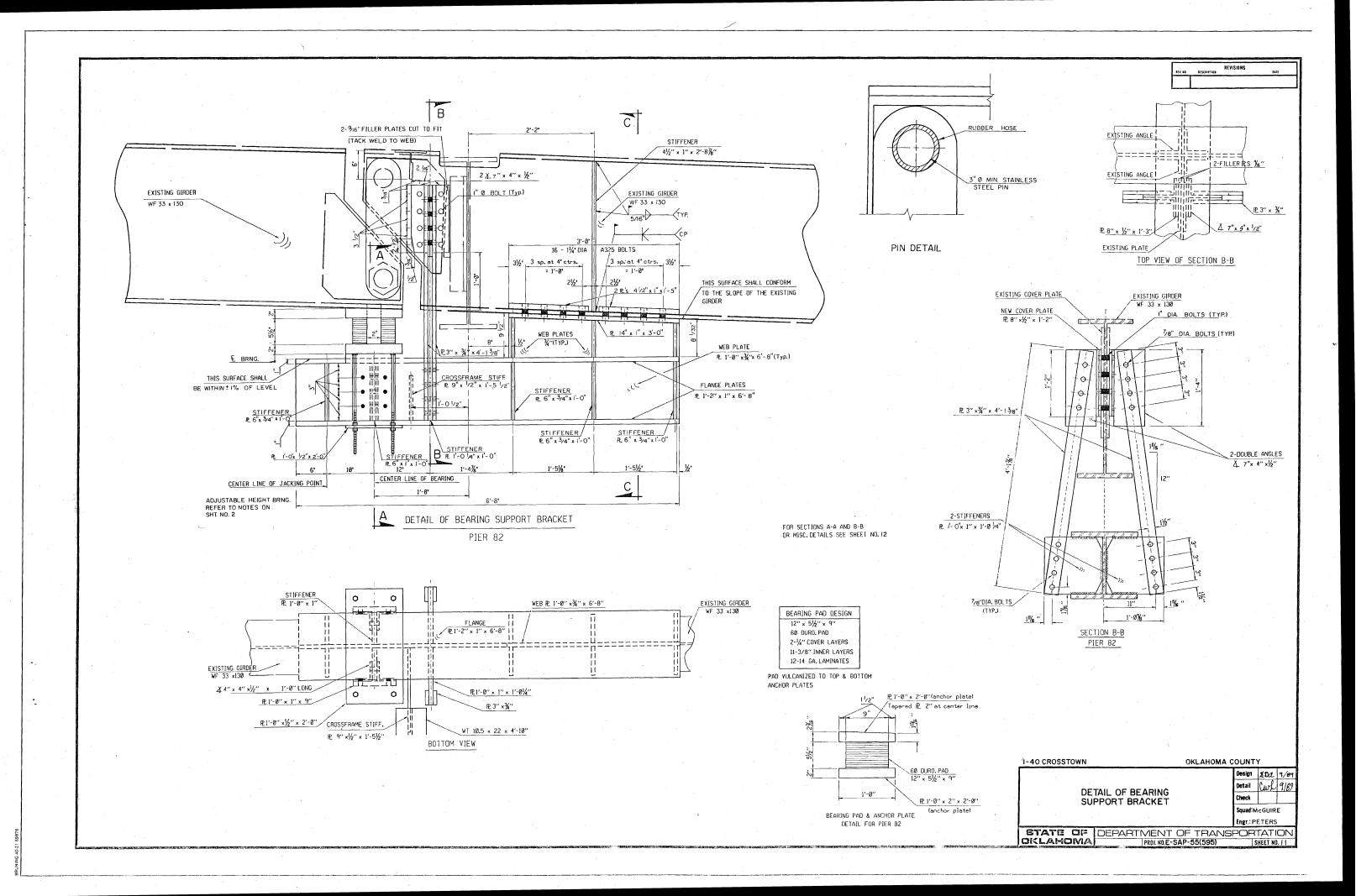
15 40-21 69876

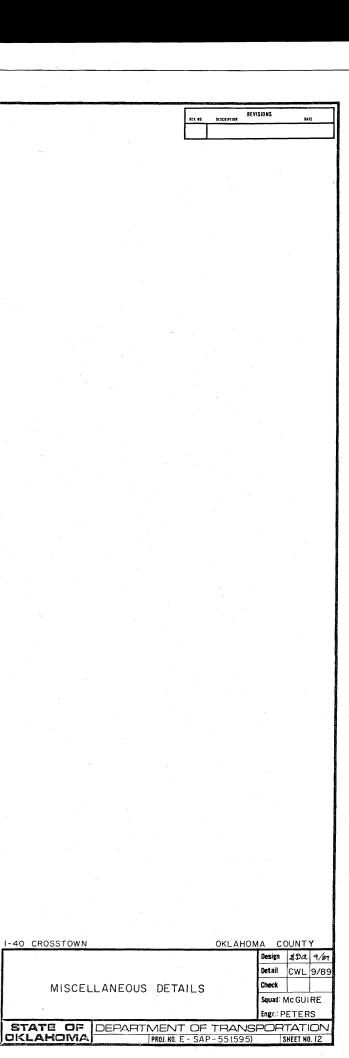


NING 40.21 60876

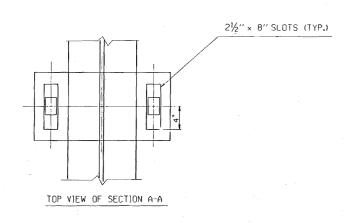


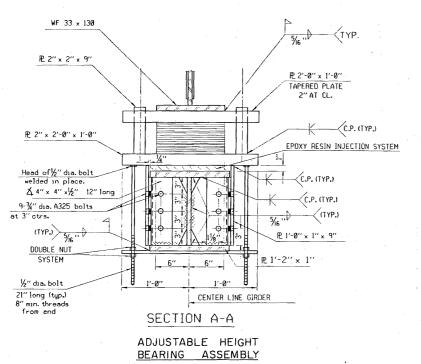


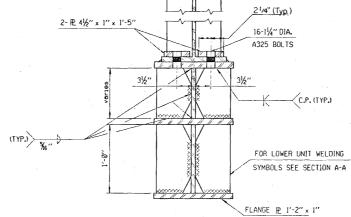




I-40 CROSSTOWN

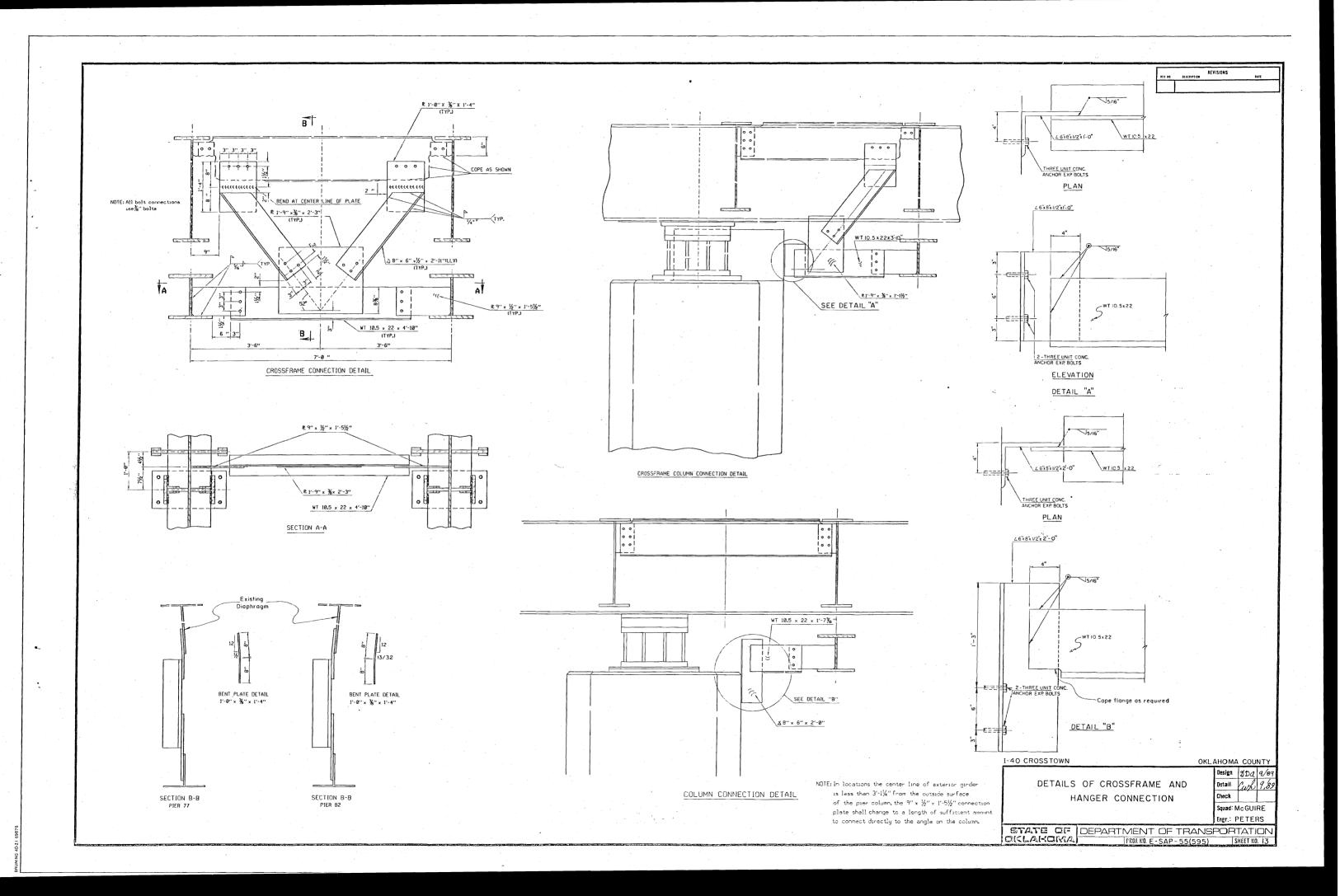


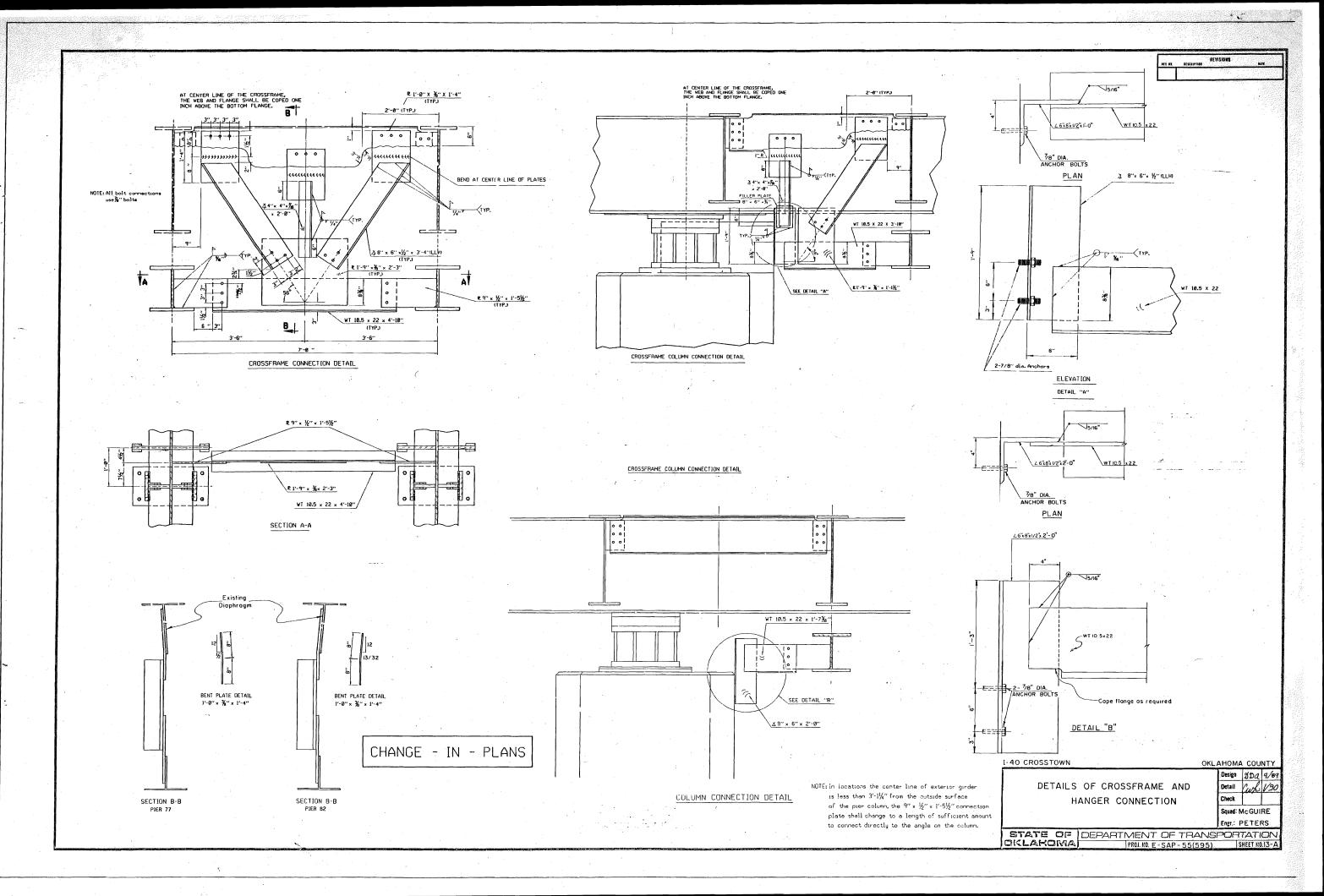




SECTION C-C

STIFFENER PLATE
PL 5" x 1"





NG 40-21 69876

ELEVATION

#### TRAFFIC OPERATIONS GENERAL CONSTRUCTION NOTES

DUE TO THE TEMPORARY NATURE OF CONSTRUCTION SIGNING, FOOTINGS WILL HAVE NO REINFORCING STEEL.

ALL SIGNS SHALL BE CONSTRUCTED TO MEET THE CURRENT OKLAHOMA DEPARTMENT OF TRANSPORTATION STANDARD SPECIFICATIONS.

ONE (1) WING BARRICADE SHALL BE SET ON EACH SIDE OF THE ROADWAY 250° IN ADVANCE OF THE FIRST ADVANCE WARNING SIGN IN EACH ADVANCE WARNING SERIES.

THE CONTRACTOR SHALL REPAIR OR REPLACE ANY NEW OR EXISTING SIGNS WHICH ARE DAMAGED DUE TO HIS NEGLIGENCE OR CARELESS HANDLING DURING THE CONSTRUCTION OF THIS PROJECT. THIS SHALL BE DONE AT THE CONTRACTORS EXPENSE.

ANY EXISTING SIGNING CURRENTLY IN PLACE WHICH IS IN CONFLICT
WITH THE INDICATED CONSTRUCTION SIGNING AS SHOWN THE PLANS, OR
ON THE T.C.D. STANDARD DRAWINGS, SHALL BE EITHER COVERED OR
REMOVED AND STORED FOR THE DURATION OF THE PROJECT. THESE SIGNS
SHALL BE EITHER UNCOVERED OR RE-INSTALLED, BY THE CONTRACTOR, UPON
COMPLETION OF THE PROJECT. COST OF THIS WORK TO BE INCLUDED IN
OTHER ITEMS OF WORK.

ALL CHANNELIZING DEVICES INITIALLY PROVIDED ON THIS PROJECT SHALL BE EITHER NEW OR IN LIKE NEW CONDITION AND SHALL BE APPROVED FOR USE ON THIS PROJECT BY THE ENGINEER.

THIS PROJECT SHALL BE CONSTRUCTED WITHOUT CLOSING TRAFFIC ON CROSS STREETS. A MINIMUM OF ONE LANE IN EACH DIRECTION SHALL BE MAINTAINED AT ALL TIMES.

EXISTING ROADWAY SHALL REMAIN OPEN DURING CONSTRUCTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROPER BARRICADES, LIGHTS, AND SIGNING WITHIN THE LIMITS OF CONSTRUCTION. ALL CONSTRUCTION SIGNING WILL BE DONE ACCORDING TO STANDARDS SET FORTH IN THE "MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES, 1987 EDITION", AND AS SHOWN ON TCD STANDARD DRAWINGS.

IN THE CLOSURE OF THE RIGHT EASTBOUND LANE, CARE WILL BE TAKEN NOT TO RESTRICT TRAFFIC ON ANY CROSS STREETS.

#### TRAFFIC OPERATIONS PAY QUANTITY NOTES

All traffic quantities shall be included in the Lump Sum price bid for "Beam Repair".

The 200' of Concrete Median Barrier will be supplied by the Division. The Contractor shall unload, set remove, and reload the Concrete Median barriers and the cost shall be included in the price bid for "Beam Repair".

During the repair work, the right lane of eastbound I-40 shall be closed to traffic.

VERIFICATION OF EXISTING CONDITIONS:

All dimensions of the existing bridge components shown on the Plans are approximate. The Contractor shall verify all dimensions necessary to connect the new material and shall be solely responsible for the

to connect the new material and shall be solely responsible for the accuracy thereof.

Bidders will fully inform themselves of the nature of the work and condition under which it will be performed. The Contractor shall adopt methods consistent with good construction practice and shall take all necessary precautions to prevent damage to the existing bridge or attachments. Any damage to the existing bridge structure or roadway due to the Contractor's negligence shall be repaired at the Contractor's expense, to the satisfaction of the Engineer.

See Title Sheet for required Traffic std's.

TRAFFIC - QUANTITIES				
ITEM NO.	ITEM	UNIT	TOTAL	
880 (C)	Advanced Warning Device (Type C)	S.D.	30	
880 (D)	Signs 0 to 6.25 S.F.	5.D.	300	
880(E)	Signs 6.25 to 15.99 SF	5. D.	240	
880 (F)	Signs 16.0 to 32.99 SF	S.D.	300	
880 (H)	Barricades (Type I)	5.D.	60	
		S.D.	60	
880(J)	Barricades (Type III)	5.D.	180	
880 (K)	Wing Barricades	S.D.	120	
880(M)	Type A Light	5.D.	180	
880(0)	Type C Light	S.D.	750	
880 (P)	Drums	5.D.	750	

#### SPECIFICATIONS:

All construction and materials shall be in accordance with the 1988 Oklahoma Standard Specifications for Highway Construction and Special Provisions. (See Proposal for Special Provisions).

"falsework and Jacking" shall include all excavation, backfilling of excavated void, metal strapping, structural steel, timber, jacks, welds, labor, materials and incidentals necessary to complete beam repair. All "Falsework and Jacking" shall be included in the price bid for "Beam Repair".

The Contractor shall have the option of using used steel provided the sections meet or exceed member sizes shown on the plans.

The materials used for the Falsework shall remain the property of the Contractor after the repair is completed.  $\label{eq:contractor} % \left( \frac{1}{2} \right) = \frac{1}{2} \left( \frac{1}{2} \right) \left( \frac{1}$ 

Structural Steel requirements shall be waived for the falsework assemblies.  $\ \ \,$ 

Careful attention shall be taken to insure that the column  $\,$  sections of the falsework assemblies are vertical.

The location of the Pier crossbeam stiffener plates shall be determined after the column sections of the falsework assemblies are erected.

Metal strapping or approved alternate shall be wrapped around the column a minimum of three (3) double wraps as approved by the Engineer. The minimum size of metal straps shall be two (2) inches.

Care shall be taken to avoid overtensioning the straps at the column falsework assembly. Small timber spacers may be used, if necessary.

After the Contractor has excavated to expose the top of the footing, the area where the sole plate is to be placed shall be sandblasted and ground with carborundum brick before placement of the piling sole plates. If leveling is necessary, this shall be achieved with shim plates (plywood may be used as directed by the Engineer). Leveling shall be done before metal straps are wrapped at the third point of the columns. All cost of bearing shims shall be included in "Falsework and Jacking".

The jacks shall be placed directly under the web of the crossbeam.

Jacking shall be done concurrently at both falsework assemblies. Jacking shall stop when the crossbeam has been lifted approximately  $1/8^{\prime\prime}$  off of the existing shoe.

Total required jacking force is approximately 200 tons. The contractor shall saw off (Do Not Torch Cut) a  $2\,Vz'''$  x  $2\,Vz'''$  {min.} piece of the Top Flange at the end of the damaged pier beam. The sample is needed by the Department for a charpy V-notch test. See sheet no. 15 for detail.

Pay Item "Beam Repair" shall include all costs of preheating, removing cracked metal, welding flange, spot painting of the affected area and additional stiffener plates, and labor, materials, and incidentals necessary to complete crack repair and "Falsework and lackiem"

Painting and preparation shall be done in accordance with Sections 506.04(d) and 730.04(c) of the 1988 Oklahoma Standard Specifications for

Primers meeting SSPC specifications for paint #11 may be substituted for red lead and basic lead silico chromate primers.

The beam shall be sufficiently heated before welding repair shall begin. All cracked metal shall be removed thoroughly. The removal of crack shall extend the entire width of the flange to insure complete removal of insufficient metal. All heating of beam, removal of unsound metal and welding shall conform to the Bridge Welding Code AMSI/AASHIO/AWS D1.5 (including current revisions). Also, welding shall conform to the 1988 Oklahoma Standard Specifications for Mighway Construction except that the references to AWS D1.1 will be replaced by ANSI/AASHIO/AWS D1.5.

## INSPECTION REQUIREMENTS:

Radiographic and Ultrasonic or Magnetic Particle Inspection will be required for the repair weld on the beam.

	QUANTITIE	S	
ITEM NO.	ITEM	UNIT	TOTAL
<b>9</b> 00.39 Sp.	Beam Repair	L,5um	J.
			14 C.

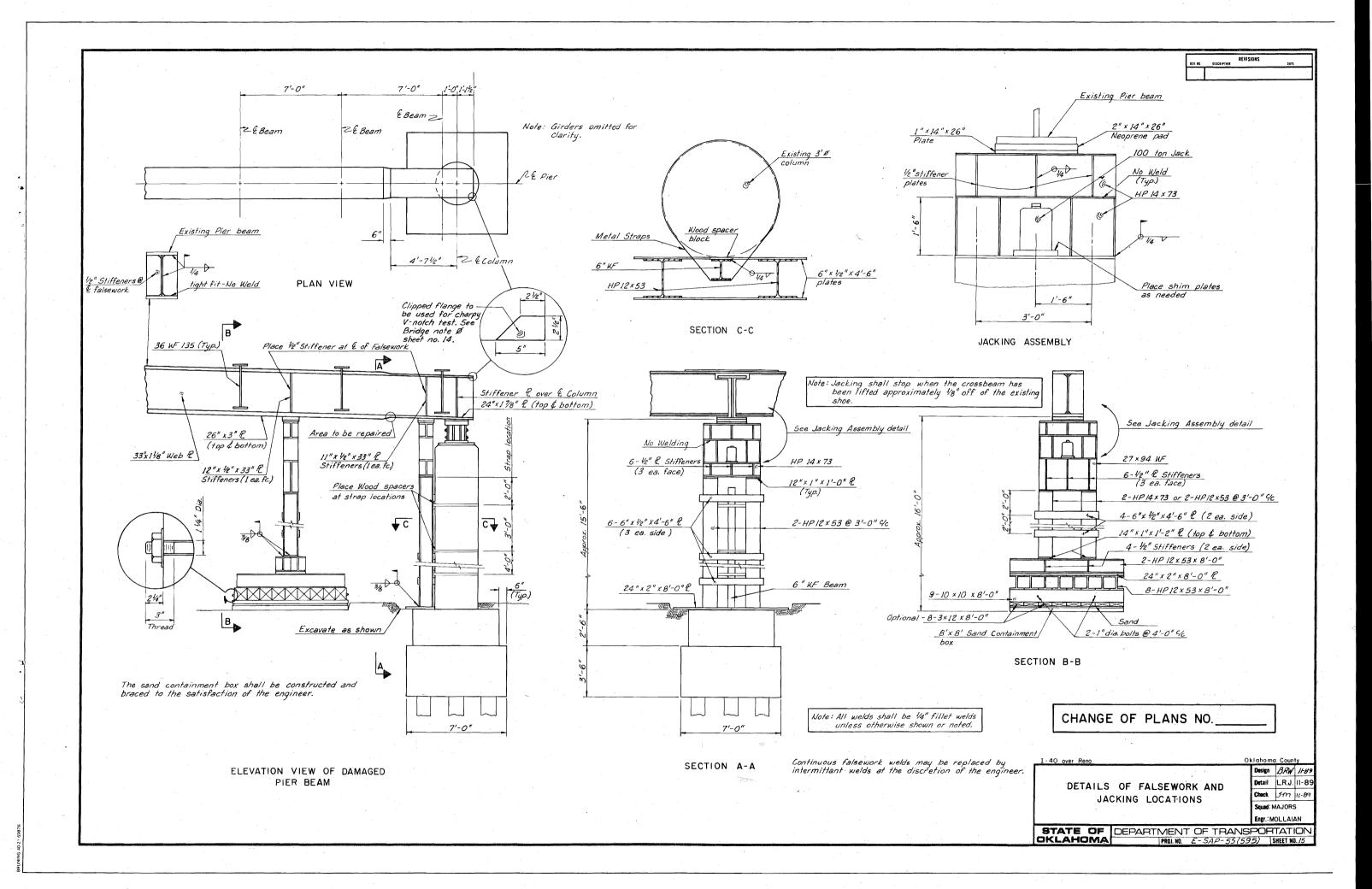
CHANGE OF PLANS NO.

I-40 over Reno

LOCATION OF CONSTRUCTION AND GENERAL NOTES

Design はパル //-Detail K.W. 11-89 Check Jm 11-89 Squad: MAJORS

STATE OF DEPARTMENT OF TRANSPORTATION OKLAHOMA PROJ. NO. E-SAP-55(595) SHEET NO. /4



# Pennsylvania Department of Transportation

Design drawings – catcher beam system.

### GENERAL NOTES

THE WORK OF THIS CONTRACT INCLUDES INSTALLATION OF AUXILIARY SUPPORT BEAMS LOCATED BENEATH THE GIRDERS AT THE HINGE LOCATIONS IN SPANS 3 AND 5 OF THE WESTBOUND STRUCTURE AND SPANS 3 AND 5 OF THE

DETAILS AND DIMENSIONS SHOWN ON THESE DRAWINGS TO DESCRIBE THE EXISTING STRUCTURE WERE TAKEN FROM THE DRAWINGS FROM WHICH THE STRUCTURE WAS ORIGINALLY BUILT AND MAY NOT REFLECT PRESENT CONDITIONS. VERIFY ALL DIMENSIONS AND GEOMETRY OF THE EXISTING STRUCTURE IN THE FIELD, AS NECESSARY, FOR PROPER FIT OF THE PROPOSED CONSTRUCTION.

CONTRACT PLANS AND SHOP DRAWINGS FOR THE EXISTING BRIDGE ARE AVAILABLE FROM THE PENNSYLVANIA DEPARTMENT OF TRANSPORTATION, AT A NOMINAL REPRODUCTION COST. CONTACT DISTRICT BRIDGE ENGINEER TO MAKE ARRANGEMENTS FOR ORDERING A SET OF CONTRACT PLANS AND FOR SELECTING THOSE SHOP DRAWINGS REQUIRED. DO NOT ASSUME THAT ALL THE SHOP DRAWINGS RELATING TO THE PROPOSED NEW WORK ARE AVAILABLE. DO NOT CONSIDER ANY OF THE DATA ON THE EXISTING STRUCTURE SUPPLIED IN THE ORIGINAL DESIGN DRAWINGS OR MADE AVAILABLE BY THE DEPARTMENT OR ITS AUTHORIZED AGENTS, AS POSITIVE REPRESENTATIONS OF ANY OF THE CONDITIONS THAT WILL BE ENCOUNTERED IN THE FIELD. THIS INFORMATION IS NOT PART OF THE PLANS, PROPOSAL, OR CONTRACT, AND IS NOT TO BE CONSIDERED A BASIS FOR COMPUTATION OF THE UNIT PRICES USED FOR BIDDING PURPOSES. THERE IS NO EXPRESSED OR IMPLIED AGREEMENT THAT INFORMATION IS CORRECTLY SHOWN. ASSUME THE POSSIBILITY THAT CONDITIONS AFFECTING THE COST AND/OR QUANTITIES OF WORK TO BE PERFORMED MAY DIFFER FROM THOSE INDICATED.

PROVIDE ALL MATERIALS AND WORKMANSHIP IN ACCORDANCE WITH PENNSYLVANIA DEPARTMENT OF TRANSPORTATION SPECIFICATIONS PUBLICATION 40B/87, CURRENT SUPPLEMENTS, AASHTO/AWS BRIDGE WELDING CODE D1.5-88 AND CONTRACT SPECIAL PROVISIONS.

PROVIDE STRUCTURAL STEEL CONFORMING TO ASTM A633, GRADE E, 60 KSI Y.P., EXCEPT WHERE NOTED OTHERWISE. PROVIDE STRUCTURAL STEEL CONFORMING TO ASTM A36 FOR STEEL DENOTED A36, AND CONFORMING TO ASTM A572 WHERE STEEL IS DENOTED A572.

FABRICATE AUXILIARY SUPPORT BEAM FLANGE PLATES, WEB PLATES AND STIFFENERS AND BEARING PLATE ASSEMBLIES USING ASTM A633 STRUCTURAL STEEL TO CONFORM TO THE REQUIREMENTS OF AASHTO GUIDE SPECIFICATIONS FOR FRACTURE-CRITICAL NON-REDUNDANT STEEL BRIDGE MEMBERS. PROVIDE MATERIAL CONFORMING TO THE BASE METAL CHARPY V-NOTCH REQUIREMENTS LISTED IN THE SPECIAL PROVISIONS.

FABRICATE ALL FRACTURE CRITICAL COMPONENTS AT AN AISC CATEGORY III FABRICATION SHOP WITH FRACTURE CRITICAL CERTIFICATION.

DESIGN SPECIFICATIONS ARE DIVISION I OF 1983 AASHTO STANDARD SPECIFICATIONS FOR HIGHWAY BRIDGES 'INCLUDING INTERIMS THROUGH THE 1986 INTERIM SPECIFICATIONS AND AS SUPPLEMENTED BY THE PENNSYLVANIA DEPARTMENT OF TRANSPORTATION DESIGN MANUAL, PART 4 (INCLUDING CURRENT REVISIONS.)

LIVE LOAD DISTRIBUTION TO GIRDERS IS BASED UPON THE AASHTO METHOD.

DEAD LOAD INCLUDES THE ORIGINAL WEIGHT OF THE STRUCTURE AND 30 POUNDS PER SQUARE FOOT FOR FUTURE WEARING SURFACE ON THE DECK SLAB.

LIVE LOAD IS HS25 APPLIED BY THE LOAD FACTOR METHOD. A LIVE LOAD OF THE PENNSYLVANIA PERMIT LOAD P-82 AND 125 PERCENT OF THE ALTERNATE MILITARY LOADING ARE ALSO APPLIED BY THE LOAD FACTOR METHOD.

IN ADDITION TO THE NORMAL REQUIREMENTS OF PENNDOT AND AASHTO, THE DESIGN OF PORTIONS OF THE PROPOSED CONSTRUCTION IS CONTROLLED BY THE STRESSES OCCURRING AT THE INSTANT THE AUXILIARY SUPPORT SYSTEM BECOMES ACTIVE (WHEN A PORTION OF THE STRUCTURE WILL DROP A SHORT DISTANCE). FOR THIS CASE, A DYNAMIC IMPACT FACTOR IS APPLIED TO ALL LOADS AND THE FOLLOWING LOAD COMBINATIONS ARE USED.

00 TE

HS20 LOADING: 1.30 (D + L + I) (DYNAMIC FACTOR)\*
HS25 LOADING: 1.20 (D + L + I) (DYNAMIC FACTOR)\*
P-82 PLU5 HS25: 1.05 (D + L + I) (DYNAMIC FACTOR)\*
MEMBERS SUBJECT TO THESE LOADINGS ARE EVALUATED AT LOAD FACTOR OPERATING
RATING STRESS LEVELS. THE "STRENGTH-IN-EXCESS-OF-FIRST-YIELD" CAPACITY
IS NOT USED. THE OVERLOAD PROVISIONS OF AASHTO DO NOT APPLY.

FATIGUE DESIGN IS BASED ON AN ADTT OF 6000 WITH 2,000,000 CYCLES OF AASHTO HS25 TRUCK LOADING.

ALL DIMENSIONS SHOWN ARE PARALLEL AND NORMAL TO THE AXIS OF THE MAIN GIRDERS, EXCEPT AS NOTED.

DIMENSIONS SHOWN FOR NEW STEEL ARE FOR A NORMAL TEMPERATURE OF 68 DEGREES F.

FIELD SPLICES OF NEW AUXILIARY SUPPORT BEAM ARE NOT PERMITTED.

ALL NEW FASTENERS ARE ASTM-A325 HIGH-STRENGTH BOLTS, UNLESS NOTED AS ASTM-A490 HIGH STRENGTH BOLTS.

 $\,$  FILL ANY BOLT HOLES NOT USED AS PART OF THE FINAL CONSTRUCTION WITH HIGH-STRENGTH BOLTS.

PAINT NEW STRUCTURAL STEEL IN ACCORDANCE WITH PUBLICATION 408/87, SECTION 1060. PAINT EXISTING STRUCTURAL STEEL IN ACCORDANCE WITH SECTION 1070.

FIELD-WELDING ON ANY PART OF THE EXISTING BRIDGE IS NOT PERMITTED WITHOUT PRIOR APPROVAL OF THE ENGINEER.

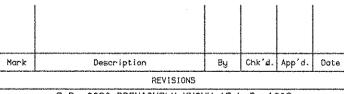
THE MINIMUM RADIUS FOR RE-ENTRANT CUTS IS 2".

IN PERFORMANCE OF WORK OPERATIONS, EXERCISE CARE TO PREVENT DAMAGE TO THOSE PORTIONS OF THE STRUCTURE WHICH WILL REMAIN IN PLACE. REPAIR OR REPLACE ANY PORTION OF THE STRUCTURE DAMAGED BY CONSTRUCTION OPERATIONS, AT THE DISCRETION OF THE ENGINEER, AND AT NO ADDITIONAL COST TO THE DEPARTMENT. PERFORM THIS WORK TO THE SATISFACTION OF THE ENGINEER.

\* SEE DESIGN LOAD TABLE, SHEET 4, FOR DYNAMIC FACTOR.

# SYMBOLS FOR FASTENERS (ALL FASTENERS 7/8' Ø UNLESS NOTED)

- . NEW FIELD-INSTALLED HIGH-STRENGTH BOLT IN NEW HOLE.
- O EXISTING BOLT TO REMAIN.
- O NEW FIELD-INSTALLED HIGH-STRENGTH BOLT IN NEW HOLE, HIDDEN.



S.R. 0080 PREVIOUSLY KNOWN AS L.R. 1009

## Commonwealth of Pennsylvania

DEPARTMENT OF TRANSPORTATION

CLEARFIELD-CENTRE COUNTIES
S.R. 0080 SECTION B13
SEGMENT 1382 OFFSET 000
S.R. 0080-000 STA. 0+00
OVER MOSHANNON CREEK
MULTIPLE SPAN WELDED PLATE GIRDER BRIDGES
GENERAL NOTES

NOV 14 1989

RECOMMENDED

S-18043

SHEET 2. OF 7

DES: CWH DR: CWH CK: NEK

4 - 11011132"