NDOT – Drainage Design and Erosion Control Manual Appendix K: Equations for Drainage Design

Equa. No.	Description	Equation	Page No.
1.1	Peak Runoff (Rational Method)	Q = CiA	1-13
1.2	Time of Concentration (Kirpich Equation)	$T_c = 0.0078 L^{0.77} S^{-0.385} C_F$	1-21
1.3	Critical Depth in Open Channel Flow	$A^{3}/T = Q^{2}/g$	1-31
1.4	Froude Number	$Fr = V/(gD)^{0.5}$	1-32
1.5	Manning's Equation for evaluating uniform flow in open channels	$V = \frac{1.486}{n} R^{2/3} S^{1/2}$	1-33
1.6	Compound Bend Angle	$\gamma = 180^{\circ} - \cos^{-1}(-\cos(\alpha) x)$ $\cos(\beta)$	1-54
1.7a	Modified Manning's Equation for evaluating gutter flow hydraulics (depth known)	$\frac{\cos(\beta))}{Q = 0.56(z/n) S^{1/2} d^{8/3}}$	1-66
1.7b	Modified Manning's Equation for evaluating gutter flow hydraulics (spread known)	Q = $(0.56/n) S_x^{5/3} S^{1/2} T^{8/3}$	1-66
1.8	Determine pavement cross slope for a V-shaped gutter	$S_X = S_{X1}S_{X2} / (S_{X1} + S_{X2})$	1-66
1.9	Length of inlet required to intercept 100% of gutter flow	$L_a = Q_a / (Q_a / L_a)$	1-72
1.10	Ratio of frontal flow to total gutter flow for grate inlets	$E_o = Q_w/Q = 1 - (1 - W/T)^{2.7}$	1-74
1.11	Ratio of side flow to total gutter flow for grate inlets	$Q_{s}/Q = 1 - Q_{w}/Q = 1 - E_{o}$	1-74
1.12	Ratio of frontal flow intercepted to total frontal flow for grate inlets	$R_f = 1 - 0.09 (V - V_o)$	1-74
1.13	Ratio of side flow intercepted to total side flow for grate inlets	$R_s = 1 / [1 + (0.15V^{1.8}/S_xL^{2.3})]$	1-74
1.14	Efficiency of a grate	$E = R_f E_o + R_s (1-E_o)$	1-75
1.15	Interception capacity of a grate on grade	$Q_i = EQ = Q[R_fE_o + R_s(1-E_o)]$	1-75
1.16	Capacity for a grate inlet in a low point or sump, inlet acting as a weir	$Q_i = CPd^{1.5}$	1-76
1.17	Capacity for a grate inlet in a low point or sump, inlet operating as an orifice	$Q_i = CA(2gd)^{0.5}$	1-76
1.18	Length of slotted pipe inlet required to intercept 100% of gutter flow on continuous grade	$L_T = 0.6Q^{0.42}S^{0.3}(1/nS_x)^{0.6}$	1-77
1.19	Interception efficiency of a slotted pipe inlet shorter than the length required for total interception of gutter flow on continuous grade	E = 1 - (1 - L/L <sub>T</sub> ) <sup>1.8</sup>	1-77
1.20	Actual gutter flow intercepted by a slotted pipe inlet on a continuous grade	Q <sub>i</sub> = EQ	1-77
1.21	Capacity for a slotted pipe inlet in a low point or sump, inlet operating as an orifice	$Q_i = 0.8LW(2gd)^{0.5}$	1-78
1.22	Capacity for a slotted pipe inlet (with a slot width of 1.75 in) in a low point or sump, inlet operating as an orifice	$Q_i = 0.94 Ld^{0.5}$	1-78
1.23	Capacity of a slotted vane drain	$Q = Kd^{5/3}$	1-78

Equa. No.	Description	Equation	Page No.
1.24	Discharge rate of flow of a storm sewer	Q = $\frac{1.486}{n}$ A R <sup>2/3</sup> S <sup>1/2</sup>	1-81
1.25	Velocity of flow in a storm sewer flowing full	$V_{\text{full}} = \frac{0.590}{N} D^{2/3} S^{1/2}$ $Q_{\text{full}} = 0.463 D^{8/3} S^{1/2}$	1-81
1.26	Discharge rate of flow in a storm sewer flowing full	n	1-81
1.27	Energy losses from pipe friction in storm sewers	$S_f = [Qn/1.486 AR^{2/3}]^2$	1-82
1.28	Head losses due to friction in storm sewers	$H_f = S_f L$	1-82
1.29	Velocity head losses in storm sewers	$H = K(V^2)/2g$	1-83
1.30	Terminal losses in storm sewers	$H = K(V^2)/2g$ H <sub>tm</sub> = (V <sup>2</sup> )/2g	1-83
1.31	Entrance losses in storm sewers	$H_e = K(V^2)/2g$	1-83
1.32	Head loss at a storm sewer junction	$H_{j1} = (V^2) (outflow)/2g$	1-83
1.33	Energy loss in a storm sewer junction due to a change in direction of flow	$H_b = K(V^2) \text{ (outlet)/2g}$	1-84
1.34	Energy loss in a storm sewer junction with several entering flows	$H_{j2} = [(Q_4V_4^2) - (Q_1V_1^2) - (Q_2V_2^2) + (KQ_1V_1^2)]/(2gQ_4)$	1-85
2.1	Shear stress on a channel	$\tau = \gamma RS$	2-27
2.2	Permissible shear stress for non-cohesive soils	$\tau = \gamma RS$ $\tau_p = (4.0 \text{ lbs/cu ft}) \times (D_{50} \div SF)$	2-28
2.3	Channel bend shear stress	$\tau_{\rm h} = (K_{\rm h}) \times (\tau_{\rm max})$	2-30
2.4	Distance increased shear stress travels down a channel from a bend	$\tau_{b} = (K_{b}) \times (\tau_{max})$ $L_{p} = (0.604) \times (R^{7/6} \div n_{b})$	2-30
2.5	Brink depth at a pipe culvert outlet	$Y_0 = (A \div 2)^{0.5}$	2-55
2.6	Froude Number	$\frac{Y_{e} = (A \div 2)^{0.5}}{V_{0} \div (g Y_{e})^{0.5}}$	2-55
2.7a - 2.7f	Variable used in calculating riprap basin depression	F ÷ Y <sub>e</sub> = (variable x Fr) – variable	2-55
2.8	Riprap basin depression	$F = (F \div Y_e) \times Y_e$	2-55
I.1	Earth loads on trench conduits	$W_c = C_d w B_d^2$	I-3
1.2	Earth loads on positive projecting embankment conduits	$W_{c} = C_{c} W B_{c}^{2}$	I-3
1.3	Earth loads on negative projecting embankment conduits	$W_c = C_n w B_d B'_d$	I-4
1.4	Earth loads on induced trench embankment conduits	$W_c = C_n w B_c^2$	I-5
1.5	Live loads on buried conduits	W <sub>L</sub> = πW L (2P <sub>1</sub> + P <sub>2</sub> )/ L + 24	I-6
1.6	Pipe strength	D-Load = TEB / D	I-10
1.7	Pipe design strength	<u>(D-Load x D) x L</u> f FS	I-10
1.8	Pipe stiffness	PS = F/ $\Delta$ Y ≥ EI / 0.149r <sup>3</sup> = 0.559 E (t/r) <sup>3</sup>	I-11
1.9	Theoretical pipe stiffness	PS = 4.47 [E/(DR-1) <sup>3</sup> ]	I-12
I.10	Earth loads on flexible culverts (lbs/lin ft)	$W_c = HwB_c$	I-14

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Equa. No.	Description	Equation	Page No.
I.11	Earth loads on flexible culverts (psi)	P = wH / 144	I-14
I.12	Deflection of buried flexible conduits	$\Delta X = D_L \frac{Kw_c r^3}{EI + 0.061 E' r^3}$	I-15
I.13	Relationship between the horizontal and vertical deflection of buried flexible conduits	$\Delta X$ = 0.913 $\Delta Y$	I-15
1.14	Percent of deflection of buried flexible conduits, ( $\Delta X = \Delta Y$ )	$\% \frac{\Delta Y}{D} = \frac{D_{L}KP (100)}{0.149 F} + 0.061E'$	I-15
I.15	Percent of deflection of buried flexible conduits, ( $\Delta X = \Delta Y$ )	$\% \underline{\Delta Y} = \underline{D_{L}KP (100)}{D [2E/3(DR-1)^{3}] + 0.061E^{2}}$	I-15
I.16	Percent of deflection of buried flexible conduits with live loads considered, $(\Delta X = \Delta Y)$	$\frac{\Delta Y}{D} = \frac{(D_{L}KP + K W')}{(100)}$ D [2E/3(DR-1) <sup>3</sup> ]+0.061E'	I-16